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TESIS CON FALLA DE ORIGEN

INFLUENCIA DEL ANGULO DEL AGITADOR Y DEL FONDO DE UN
 TANQUE CONTINUO DE MEZCLA COMPLETA EN LA
 DISTRIBUCION DE TIEMPOS DE RESIDENCIA DE
 UN SOLIDO PARTÉ I: SIN DEFLECTORES

TESIS PROFESIONAL

QUE PARA OBTENER EL TITULO DE:

INGENIERO QUIMICO

P R E S E N T A

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INTRODUCCIÓN

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Esta investigación tiene como objetivo determinar la influencia de la geometría del fondo del tanque y la posición del agitador, variando la salida del alimento, en la distribución de tiempos de residencia de un sólido, en un tanque continuo de mezcla completa.

Para determinar la influencia de estos parámetros se utilizó la prueba estadística de Kolmogorov-Smirnov, para funciones de distribución de frecuencias comparando los resultados experimentales y teóricos.

El trazador sólido a usar, correspondió a arena sílica de una malla determinada conteniendo la característica de ser un sólido no reactivo y será el vehículo para el conocimiento de la distribución de tiempos de residencia.

Las pruebas experimentales se hicieron a cabo combinando las dos geometrías de fondo del tanque, las dos posiciones del agitador y las dos posiciones de salida del alimento, completando así dieciséis pruebas, pues cada prueba se hizo por duplicado. Además, cada una de las pruebas fue comparada con el modelo ideal de mezcla completa.

S I M B O L O G I A

S I M B O L O G Í A

A= Constante de Orificio

A° MAX= Diferencia máxima entre las frecuencias teórica y experimental para cada prueba.

A1= Posición de agitación número uno (A1).

A2= Posición de agitación número dos (A2).

A° 1= Diferencia entre frecuencias teóricas y experimentales, dada por la ec. IV-B3.

A° 2= Diferencia entre frecuencias teóricas y experimentales, dada por la ec. IV-B4.

B= Constante de orificio.

C= Concentración promedio de trazador en el tanque, dada por la ec. IV-A1.

C_r= Concentración de trazador para cada tubo muestreador, dada por la ec. IV-A2.

D= Valor máximo permisible en la prueba estadística.

DIF-A= Diferencia entre frecuencias teóricas y experimentales, dadas por las ecs. IV-B1 y IV-B2.

E= Esperanza matemática.

E_o= Esperanza matemática experimental a un valor dado de teta.

E_o Teor= Esperanza matemática de teta teórica, dada por la ec. IV-A6.

F= Distribución de frecuencias.

F_o= Frecuencia acumulada experimental a un valor dado de teta.

F_e PROM= Valor promedio entre frecuencias de la prueba y su réplica.

F_o R1= Valor de frecuencias de la réplica número uno.

F_e R2= Valor de frecuencias de la réplica número dos.

F_e Teor= Frecuencia acumulada teórica dada por la ec.

IV-A7.

F_e teor1= Frecuencia teórica acumulada igual a F_e Teor.

F_e teor2= Frecuencia teórica de valores discretos, dada por la ec. IV-AB.

h_o = Hipótesis de nulidad.

Q = Caudal del fluido.

R_1 = Réplica número uno.

R_2 = Réplica número dos.

Re_1 = Tanque con geometría de fondo plano.

Re_2 = Tanque con geometría de fondo de cono y filete.

S_1 = Posición de salida del fluido número uno.

S_2 = Posición de salida del fluido número dos.

t = Tiempo, en minutos.

V = Volumen de operación en el tanque.

V_o = Caudal de entrada al tanque (constante).

W Seco= Peso del tubo muestreador antes de la prueba.

W Total= Peso del tubo muestreador después de la prueba.

α = Nivel de significancia para el tratamiento estadístico.

h = Diferencia de presión en el medidor de flujo.

Θ = Teta, tiempo adimensional (t/τ).

τ = Tiempo espacial, en minutos (V/V_o).

CAPÍTULO 1

FUNDAMENTOS TEÓRICOS

FUNDAMENTOS TEÓRICOS

A.- Distribución de Tiempos de Residencia en Reactores de Mezcla Completa. (1,7)

Cuando una corriente de fluido entra en un reactor con agitación, el flujo sigue diferentes caminos a lo largo del mismo, por lo que los tiempos de residencia de las diferentes partículas serán distintos.

Para la determinación del tiempo de residencia en este estudio, se utiliza el método estímulo-respuesta, que consiste en estimular al sistema mediante una perturbación y analizar las respuestas a este estímulo. Con esto obtenemos el comportamiento del sistema a las condiciones dadas. La perturbación antes mencionada se logra con la adición de un trazador, en nuestro caso sólido, directamente al reactor. La concentración de dicho trazador, que será proporcional al peso de éste, en un volumen dado de muestra, es medida a la salida del reactor y es la que nos dará a conocer la respuesta.

La distribución de tiempos de residencia de la corriente de salida del reactor recibe el nombre de la distribución de la edad a la salida, E.

La esperanza matemática de que una partícula de trazador permanezca en el reactor un tiempo t , está representada por la concentración promedio en la corriente de salida del reactor en dicho tiempo t .

$$\text{Ec. 1.1} \quad \int_{t=0}^{t=\infty} E * dt = 1$$

Dado un tiempo adimensional, midiendo el tiempo en función del tiempo espacial, tenemos que:

$$\text{Ec. 1.2} \quad \theta = \frac{t}{\tau}$$

Se denomina curva F a la curva presentada por la concentración a la salida del reactor contra el tiempo, cuando a la corriente del fluido que entra al recipiente y no lleva consigo ningún trazador, se le impone, en $t=0$, una señal escalón, de concentración C_0 en la corriente de entrada al reactor. Esta curva es ascendente desde cero hasta uno.

Si se considera un fluido sin trazador que circula en flujo estacionario a través del reactor, y en el instante $t=0$ se introduce una señal escalonada de concentración C_0 , se puede llegar a relacionar la esperanza matemática E con la frecuencia F.

Si tomamos en consideración que, para cualquier instante $t > 0$, la señal de la salida tiene una edad menor a t , se tiene que:

$$\text{Ec. 1.3} \quad \left[\begin{array}{l} \text{FRACCIÓN DE LA SEÑAL} \\ \text{EN LA CORRIENTE DE} \\ \text{SALIDA} \end{array} \right] = \left[\begin{array}{l} \text{FRACCIÓN DE LA CORRIENTE} \\ \text{DE SALIDA CON EDAD} \\ \text{MENOR A } t \end{array} \right]$$

donde el término de la izquierda corresponde al valor de F , por lo que:

$$\text{Ec. 1.4} \quad F = \int_0^t E * dt$$

haciendo la aproximación a límites finitos, tenemos que:

$$\text{Ec. 1.5} \quad F = \sum_{t=0}^{t+\Delta t} E * \Delta t$$

\bar{E} = Interpretación de la Información dada por un Trazador. (1,7)

En la generalidad de los casos, el comportamiento real de un reactor nunca presenta una idealidad, ya que existen diferentes factores para que esto suceda. Dichos factores pueden ser, la recirculación del fluido, la formación de pozos o zonas muertas en el reactor y la formación de canalizaciones de flujo, por ejemplo.

Otro factor importante es el cambio de escalas en el sistema, pues el comportamiento de un reactor piloto puede variar considerablemente con respecto al comportamiento presentado por un reactor a nivel planta industrial. Esta variación depende, en gran parte, al control que se tenga sobre las variables del proceso en cuestión. A continuación se explican algunos de los factores ya mencionados, que contribuyen al comportamiento real de un reactor los cuales se relacionan íntimamente con la curva obtenida de la

información proporcionada por un trazador:

1) Recirculación del fluido (By-Pass): Este fenómeno se origina debido a que en el reactor, la entrada y salida del fluido están muy cercanas entre sí, por lo que el tiempo de residencia de una cierta cantidad de trazador en el reactor es muy corto. La figura 1.1 representa la curva de E_0 contra θ , en donde el primer pico es el que indica la salida inmediata de una fracción del trazador.

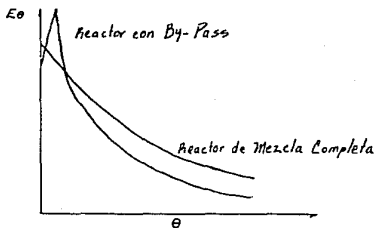


figura 1.1

2) Zonas muertas: Este fenómeno se presenta cuando hay un estancamiento del fluido en el reactor en las esquinas del mismo. Como podemos observar en la figura 1.2, hay una señal que se adelanta debido a zonas muertas, por lo que el trazador se distribuye en un volumen menor lo que origina que el tiempo de residencia de éste dentro del reactor, disminuya.

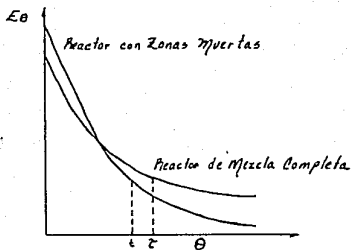


figura 1.2

C.-Mezcla y Agitación. (2.4.6.10)

La suspensión de sólidos en una fase líquida depende, en gran parte, del mezclado y agitación que a estos sólidos les son impuestos. El proceso de mezcla es mover el material para que éste logre un estado homogéneo, provocando que las partículas de materia se entremezclen en diferentes direcciones. Cuando existe una fuerza externa, como la de un impulsor, el líquido se mezcla, creando una turbulencia y moviendo éste a la región turbulenta.

El elemento usado para la mezcla de líquidos y que origina turbulencia y corriente, es el impulsor giratorio, el cual puede tener la forma de turbina, paleta plana o en forma de hélice del tipo marino. Aunque hay muchas variaciones en cuanto al diseño de los impulsores, éste no es el único parámetro que influye

directamente en el tipo de corriente y turbulencia que se puede presentar dentro de un sistema de mezclado.

Hay tres factores que determinan y regulan el movimiento del fluido en un sistema de mezclado y éstos son: la geometría del recipiente, el impulsor y el líquido. El impulsor, por sí sólo, produce el movimiento del fluido, y, conjuntamente con la geometría de las paredes del recipiente, genera las líneas principales de flujo a través del líquido.

Cuando un tanque no presenta deflectores en sus paredes, el resultado de la agitación es la formación de un vórtice, (fig. 1.3) lo que origina que la corriente no presente movimiento vertical y sólo sea un movimiento circular. El uso de deflectores en la geometría de las paredes del mezclador, influye grandemente en la suspensión de sólidos en una fase líquida, pero es necesario aportar más energía para lograr una corriente y una turbulencia homogéneas en todas las zonas del tanque. Aunque la suspensión de sólidos es usualmente desarrollada en tanque con fondo plano con deflectores, esta geometría tiene características que tienden a alejar marcadamente el comportamiento del fluido de la idealidad (fig. 1.4).

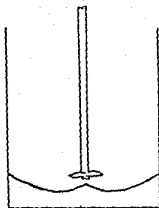


figura 1.5

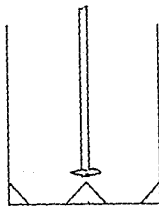


figura 1.6

La principal virtud de esta geometría es que puede lograrse modificando un tanque de fondo plano convencional, a un costo muy bajo, logrando un modelo apropiado para sólidos que son difíciles de suspender.

CAPÍTULO 2

EXPERIMENTACIÓN

E X P E R I M E N T A C I Ó N

A.- Desarrollo Experimental.

Para llevar a cabo este estudio, primeramente se hizo una revisión bibliográfica acerca de los parámetros que pueden llegar a influir en la suspensión de sólidos en un líquido, además de consultar diferentes trabajos de tesis relacionados con nuestro tema en cuestión.

Se vio que la geometría del fondo juega un papel importante en el comportamiento de la corriente del fluido y que la comparación de diferentes tipos de geometrías proporcionaría información interesante. Al efectuar las pruebas preliminares en los dos tipos de geometría de fondo escogidas se vio que, al cambiar el ángulo de agitación en el sistema, la señal de respuesta del trazador variaba considerablemente lo cual hace pensar en otra variable más: el ángulo de agitación.

Después de varias pruebas, se eligió como trazador sólido una arena sílica de un tipo de malla apropiado, de tal manera que no se presentará un asentamiento marcado de ésta.

Se llevaron a cabo ocho pruebas, cada una con su réplica, en donde los parámetros constantes fueron los siguientes:

1. Caudal del fluido (l/min).....0.830
2. Volumen del tanque (l).....12.70
3. Velocidad de agitación (rpm).....296-306

4. Tipo de agitador.....Turbina de hoja sumergida
 5. Diámetro de la partícula del trazador (mm)....0.1140
 6. Cantidad de trazador (g).....100.0
 7. Entrada del Alimento
 con respecto al fondo del tanque (cm).....22
 8. Posición de entrada del trazador...Junto al agitador

Las variables a tratar en esta investigación fueron las siguientes (ver figuras 2.1 y 2.2):

1. Geometría del Fondo del Tanque.-

- Fondo Plano. (Re1)
- Fondo de Cono y Filete. (Re2)

2. Posición del Agitador.-

- Vertical. (A1)
- Angular. (A2)

3. Salida del Fluido.-

- 22 cm del Fondo del Tanque. (S1)
- 10 cm del Fondo del Tanque. (S2)

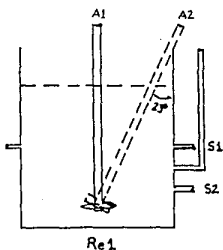


figura 2.1

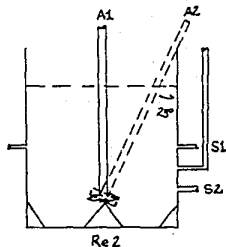


figura 2.2

B.- Esquema del Equipo.

El equipo empleado se armó siguiendo el modelo de flujo de mezcla completa, el cual se describió en el capítulo 1.

La figura 2.3 muestra el sistema utilizado en la investigación. Para mayor información consultar el apéndice II.

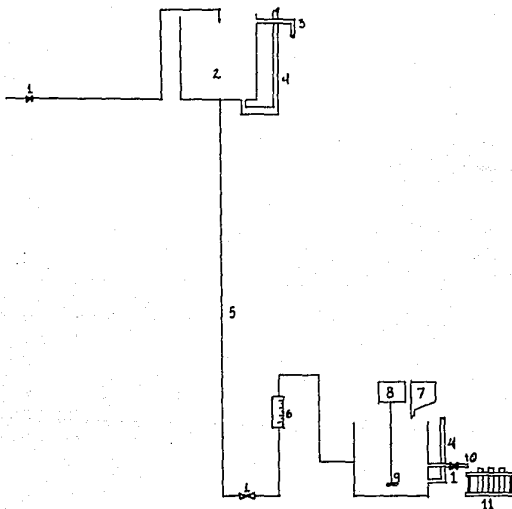


figura 2.3

Descripción de la figura 2.3:

1. Llaves de paso
2. Tanque de alimentación
3. Rebosadero
4. Medidores de nivel
5. Corriente de alimentación
6. Rotámetro
7. Tolva de alimentación de trazador
8. Agitador
9. Tanque
10. Corriente de salida del sistema
11. Tubos muestradores

C.- Metodología.

Cada corrida consistió en combinar una posición del agitador con una salida del fluido. Esta posición se mantuvo fija para probar la segunda salida del fluido. Después, se cambió la posición del agitador para ser combinada con las dos diferentes salidas del fluido.

Posteriormente, se cambió el tanque con la otra geometría de fondo para realizar las combinaciones pertinentes.

El procedimiento a seguir para cada corrida está descrito a continuación:

1. Pasos Preliminares.
 - 1.1. Calibración del rotámetro (ver apéndice III).
 - 1.2. Armado del equipo de acuerdo con la figura 2.3.

1.3. Determinación de la concentración promedio en el tanque.

2. Rutina de Trabajo.

2.1. Se pesan los tubos de ensayo previamente lavados y secos.

2.2. Se escogen las condiciones de operación: Salida del fluido, ángulo de agitación y fondo del tanque.

2.3. Se llena el tanque hasta su nivel de operación al igual que el tanque alimentador, regulando el flujo del caudal previamente establecido.

2.4. Se logra un estado estacionario en el reactor mediante una llave de paso a la salida de éste.

2.5. Se pone en marcha el agitador durante cinco minutos y después se apaga asegurándose que el nivel de operación no varíe.

2.6. Se pesan cien gramos de arena sílica previamente lavada y seca. Se preparan los tubos muestreadores.

2.7. Se inicia la agitación v. a un tiempo cero tomado con un cronómetro, se agrega la arena por el centro del tanque, lo más rápido posible.

2.8. Cada corrida tuvo una duración de 37.5 minutos, tiempo que fue distribuido en los siguientes intervalos:

| No. de Muestra | Intervalo de Tiempo |
|----------------|---------------------|
| 1 | tiempo cero |
| 2-31 | 10 segundos |
| 32-46 | 30 segundos |
| 47-71 | 60 segundos |

2.9. Al terminar el tiempo de corrida, se dejan reposar los

tubos por algunos minutos. para después decantar cada uno de éstos, eliminando la mayor cantidad de agua.

2.10. Se introducen los tubos a un secador, a una temperatura de 200°C durante una hora, se dejan enfriar y, se pesan.

CAPÍTULO 3

RESULTADOS OBTENIDOS

R E S U L T A D O S O B T E N I D O S

Los resultados que se obtuvieron en las diferentes pruebas y los cálculos correspondientes se presentan en tablas que incluyen las siguientes columnas:

Número = Número de muestra.

Tiempo = Tiempo al que fue tomada la muestra después de agregado el trazador, segundos.

Teta = Valor adimensional del tiempo, $e=t/\tau$.

W Total = Peso del tubo muestreador con la arena recolectada y seca, gramos.

W Seco = Peso del tubo muestreador vacío, gramos.

Ea = Valor de la esperanza matemática de teta, para un tiempo determinado.

Fe = Valor de frecuencia acumulada correspondiente a cada tiempo.

Ea Teor = Valor de Ea teórico calculado para el sistema.

Fe Teor = Valor de Fe teórico calculado a partir de Ea Teor.

En este capítulo sólo se dará un ejemplo de los cálculos realizados (tabla 3.1) y las tablas con los datos de las otras corridas se encuentran en el apéndice V.

La tabla 3.1 corresponde a la corrida realizada utilizando el tanque de fondo plano (Re1), la posición del agitador número uno (vertical) (A1) y la salida del fluido número uno (22 cm del fondo del tanque) (S1).

Las figuras mostradas en este capítulo corresponden a cada una de las tablas de las corridas realizadas y van numeradas de manera ascendente, presentándose en el siguiente orden para cada prueba:

1. Esperanza de teta: E_t teórica y experimental vs e .
2. Frecuencia de teta: F_t teórica y experimental vs e .

TABLA 3.1
Número

| | tiempo | total | W Total | Relación W Secu | Ea | Ea Teor | Fe | Fe Teor |
|---------|--------|--------|---------|--------------------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.0292 | 21.0292 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.0397 | 21.0160 | 0.9617 | 0.9892 | 0.0052 | 0.0109 |
| 2 | 20 | 0.0218 | 21.0420 | 21.1733 | 0.9503 | 0.9785 | 0.0157 | 0.0215 |
| 3 | 30 | 0.0327 | 21.0751 | 21.6220 | 0.9594 | 0.9679 | 0.0261 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6213 | 21.3641 | 0.9750 | 0.9574 | 0.0366 | 0.0426 |
| 5 | 50 | 0.0545 | 22.0227 | 21.9825 | 0.9165 | 0.9470 | 0.0469 | 0.0530 |
| 6 | 60 | 0.0654 | 21.3976 | 21.1575 | 0.9102 | 0.9367 | 0.0568 | 0.0633 |
| 7 | 70 | 0.0762 | 22.0038 | 21.8450 | 0.9052 | 0.9266 | 0.0667 | 0.0724 |
| 8 | 80 | 0.0871 | 20.7960 | 20.5534 | 0.9196 | 0.9165 | 0.0766 | 0.0835 |
| 9 | 90 | 0.0980 | 22.0620 | 21.8285 | 0.8851 | 0.9066 | 0.0864 | 0.0934 |
| 10 | 100 | 0.1089 | 21.4012 | 21.1730 | 0.8650 | 0.8968 | 0.0960 | 0.1032 |
| 11 | 110 | 0.1198 | 21.5669 | 21.3403 | 0.8590 | 0.8871 | 0.1053 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6267 | 21.4048 | 0.8487 | 0.8775 | 0.1146 | 0.1225 |
| 13 | 130 | 0.1416 | 21.0292 | 20.8010 | 0.8650 | 0.8680 | 0.1240 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2729 | 21.0020 | 0.8753 | 0.8506 | 0.1335 | 0.1414 |
| 15 | 150 | 0.1634 | 20.5055 | 20.3558 | 0.8700 | 0.8493 | 0.1430 | 0.1507 |
| 16 | 160 | 0.1743 | 21.2215 | 20.9972 | 0.8503 | 0.8401 | 0.1523 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4192 | 21.2030 | 0.8196 | 0.8310 | 0.1614 | 0.1690 |
| 18 | 180 | 0.1961 | 21.1222 | 20.9006 | 0.8400 | 0.8220 | 0.1705 | 0.1780 |
| 19 | 190 | 0.2070 | 21.2064 | 20.9942 | 0.8044 | 0.8131 | 0.1794 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0342 | 20.8270 | 0.7854 | 0.8042 | 0.1881 | 0.1958 |
| 21 | 210 | 0.2287 | 21.5917 | 21.3978 | 0.7350 | 0.7955 | 0.1964 | 0.2045 |
| 22 | 220 | 0.2396 | 21.2535 | 21.0555 | 0.7506 | 0.7869 | 0.2045 | 0.2131 |
| 23 | 230 | 0.2505 | 21.2070 | 21.0053 | 0.7646 | 0.7784 | 0.2127 | 0.2216 |
| 24 | 240 | 0.2614 | 21.4043 | 21.2029 | 0.7635 | 0.7700 | 0.2210 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2357 | 21.0408 | 0.7388 | 0.7616 | 0.2292 | 0.2384 |
| 26 | 260 | 0.2832 | 22.1072 | 21.9149 | 0.7290 | 0.7534 | 0.2372 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7812 | 21.5932 | 0.7127 | 0.7452 | 0.2451 | 0.2548 |
| 28 | 280 | 0.3050 | 21.4830 | 21.2856 | 0.6914 | 0.7371 | 0.2527 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5256 | 21.3406 | 0.7013 | 0.7291 | 0.2603 | 0.2709 |
| 30 | 300 | 0.3268 | 21.5946 | 21.4234 | 0.6490 | 0.7212 | 0.2676 | 0.2788 |
| 31 | 310 | 0.3377 | 21.4308 | 21.2621 | 0.6698 | 0.6981 | 0.2892 | 0.3019 |
| 32 | 320 | 0.3486 | 21.0889 | 20.9035 | 0.6952 | 0.6756 | 0.3115 | 0.3244 |
| 33 | 330 | 0.4248 | 20.8267 | 20.6459 | 0.6854 | 0.6539 | 0.3340 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4558 | 21.2910 | 0.6247 | 0.6329 | 0.3555 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1557 | 21.0006 | 0.6251 | 0.6125 | 0.3759 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3419 | 21.1733 | 0.6391 | 0.5928 | 0.3965 | 0.4072 |

TABLA 3.1
Número

| | tiempo | continuación... | | ReAISIRI | | Ee | Ee teor | Fe | Fe Teor |
|----|--------|-----------------|---------|----------|--------|--------|---------|--------|---------|
| | | leta | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.3887 | 21.2265 | 0.6149 | 0.5738 | 0.4170 | 0.4262 | |
| 38 | 540 | 0.5602 | 21.3685 | 21.2122 | 0.5849 | 0.5553 | 0.4366 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3807 | 21.2352 | 0.5516 | 0.5375 | 0.4552 | 0.4625 | |
| 40 | 600 | 0.6525 | 21.4625 | 21.3239 | 0.5254 | 0.5202 | 0.4728 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.7046 | 21.5677 | 0.5190 | 0.5035 | 0.4898 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.6867 | 20.9535 | 0.5049 | 0.4873 | 0.5066 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1993 | 21.0720 | 0.4826 | 0.4716 | 0.5227 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.8680 | 21.7414 | 0.4799 | 0.4565 | 0.5384 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2640 | 21.1387 | 0.4750 | 0.4418 | 0.5540 | 0.5582 | |
| 46 | 810 | 0.8623 | 21.2002 | 21.0860 | 0.4253 | 0.4138 | 0.5835 | 0.5862 | |
| 47 | 870 | 0.9476 | 20.6724 | 20.5723 | 0.3795 | 0.3877 | 0.6098 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5223 | 21.4273 | 0.3601 | 0.3631 | 0.6339 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7529 | 20.6665 | 0.3275 | 0.3402 | 0.6564 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3814 | 21.3022 | 0.3002 | 0.3166 | 0.6769 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4574 | 21.3826 | 0.2835 | 0.2985 | 0.6960 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.0915 | 21.0200 | 0.2710 | 0.2796 | 0.7141 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7612 | 20.6912 | 0.2654 | 0.2619 | 0.7316 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9204 | 20.0560 | 0.2441 | 0.2453 | 0.7483 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1718 | 21.1110 | 0.2305 | 0.2298 | 0.7638 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1598 | 21.1062 | 0.2032 | 0.2153 | 0.7780 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2185 | 21.1645 | 0.2047 | 0.2017 | 0.7913 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0143 | 20.9858 | 0.1839 | 0.1889 | 0.8040 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8251 | 20.7804 | 0.1694 | 0.1769 | 0.8155 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9547 | 20.9112 | 0.1649 | 0.1658 | 0.8265 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.3014 | 21.2579 | 0.1649 | 0.1553 | 0.8372 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7135 | 20.6759 | 0.1501 | 0.1454 | 0.8475 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2652 | 21.2269 | 0.1452 | 0.1362 | 0.8572 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.2648 | 21.1705 | 0.1300 | 0.1276 | 0.8662 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6925 | 21.6530 | 0.1497 | 0.1196 | 0.8753 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9962 | 20.9606 | 0.1350 | 0.1120 | 0.8846 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7621 | 20.7360 | 0.0914 | 0.1049 | 0.8920 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4231 | 21.4069 | 0.0842 | 0.0983 | 0.8977 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1177 | 21.0902 | 0.1042 | 0.0920 | 0.9039 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9534 | 20.9533 | 0.0004 | 0.0862 | 0.9073 | 0.9138 | |

FIG. 3.1
RelAISIR1

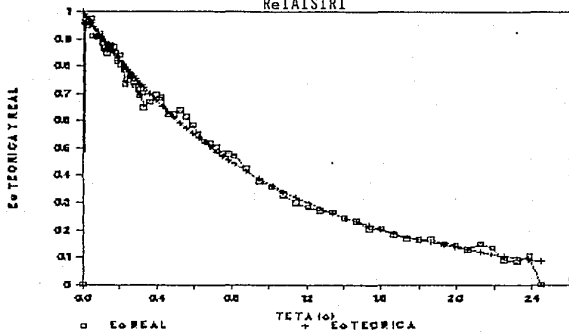


FIG. 3.2
RelAISIR1

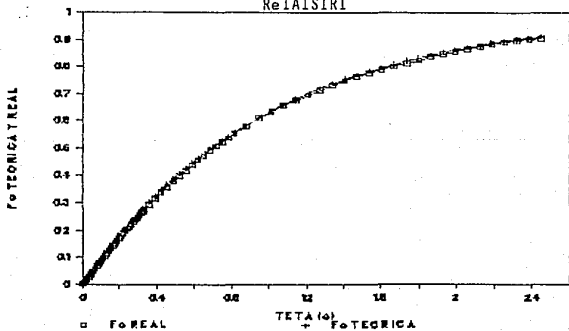


FIG. 3.3

ReIA1S1R2

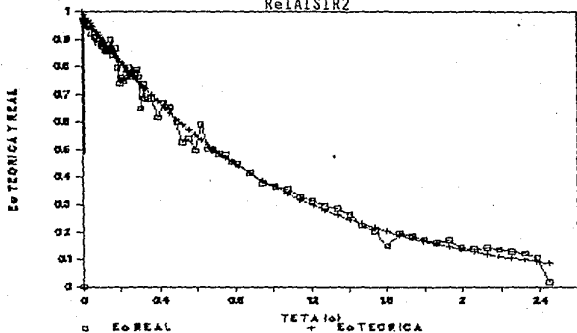


FIG. 3.4

ReIA1S1R2

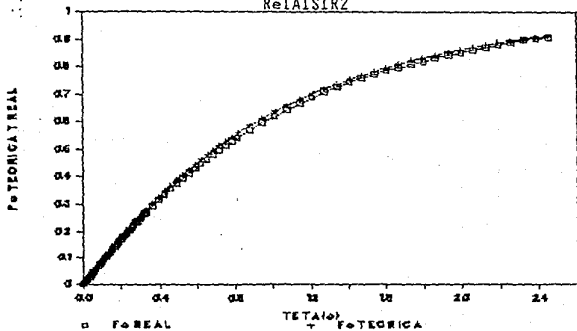


FIG. 3.5

Re1A1S2R1

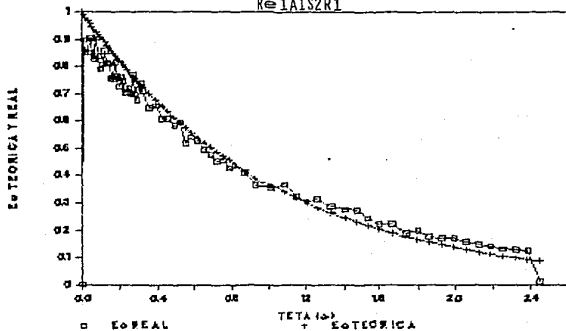


FIG. 3.6

Re1A1S2R1

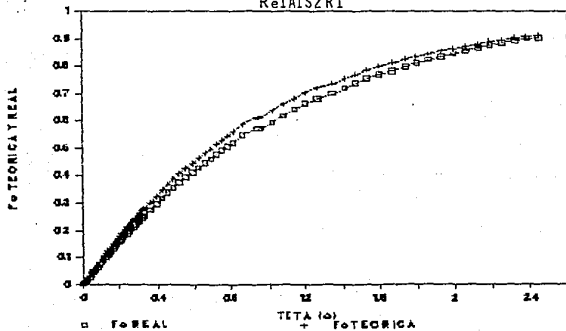


FIG. 3.7
Re1A1S2R2

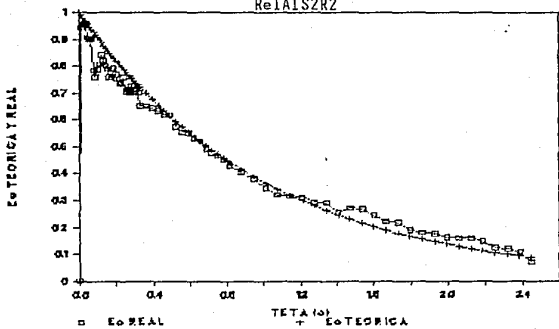


FIG. 3.8
Re1A1S2R2

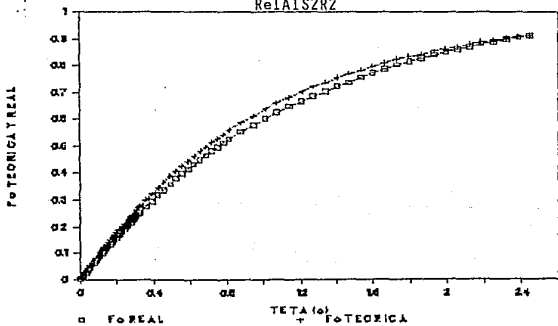


FIG. 3.9
RelA2S1R1

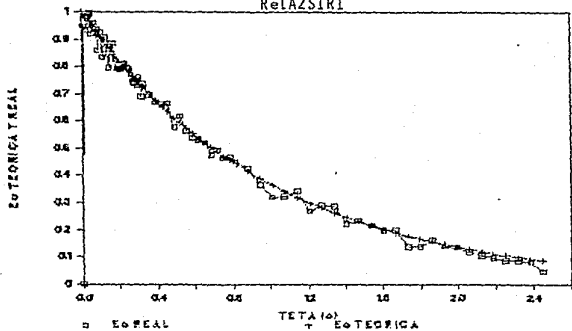


FIG. 3.10
RelA2S1R1

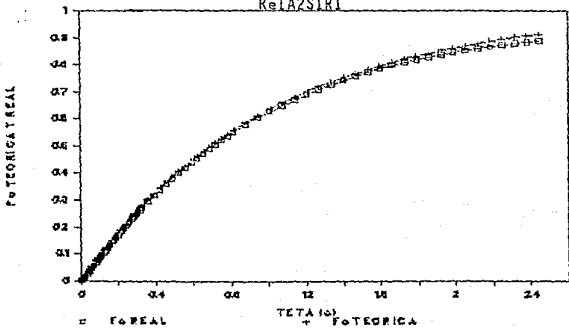


FIG. 3.11
Re1A2S1R2

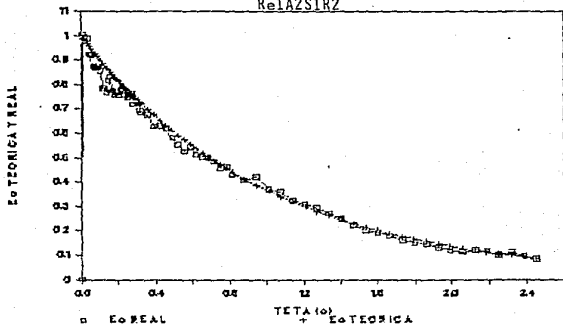


FIG. 3.12
Re1A2S1R2

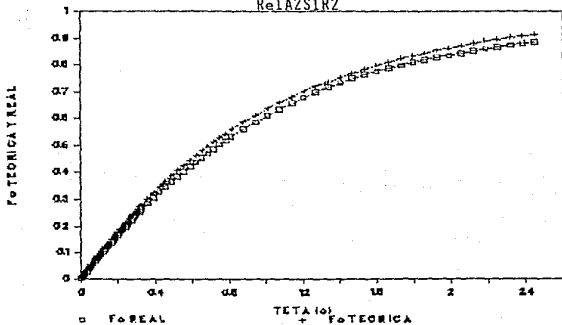


FIG. 3.13
Re1A2S2R1

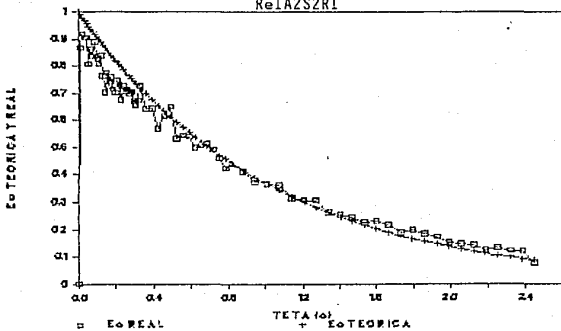


FIG. 3.14
Re1A2S2R1

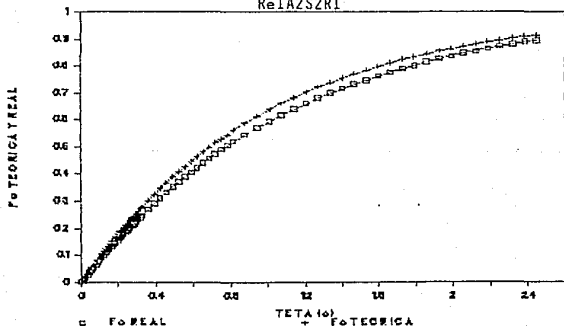


FIG. 3.15
Re1A2S2R2

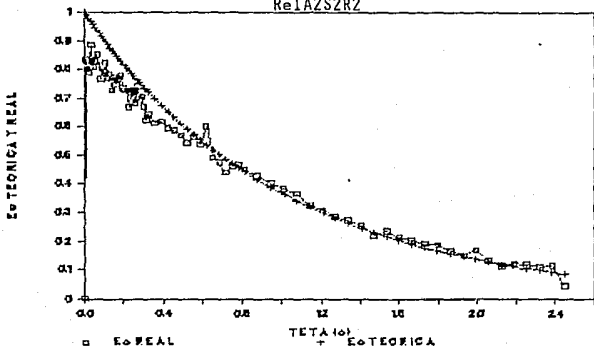


FIG. 3.16
Re1A2S2R2

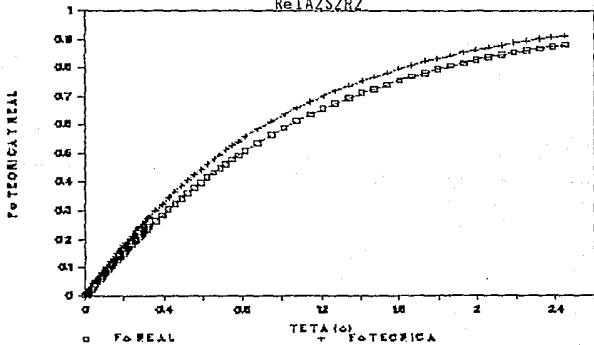


FIG. 3.17
Re2A1S1R1

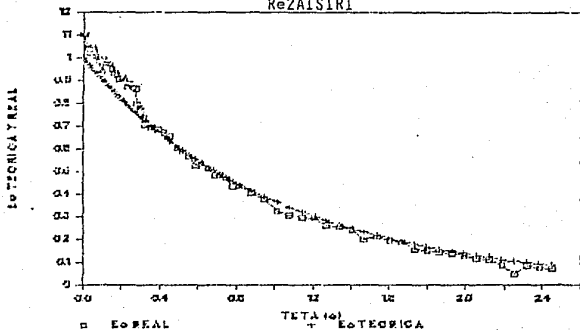


FIG. 3.18
Re2A1S1R1

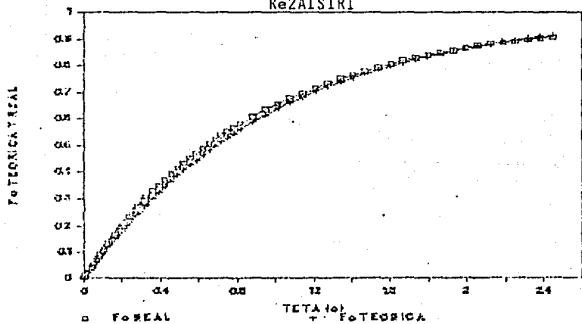


FIG. 3.19
Re2A1S1R2

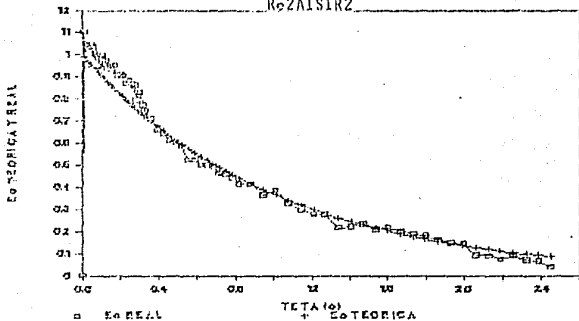


FIG. 3.20
Re2A1S1R2

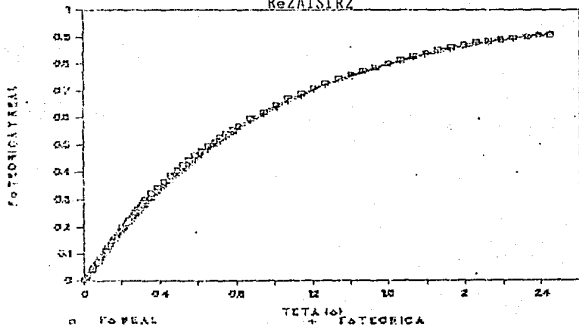


FIG. 3.21
Re2A1S2R1

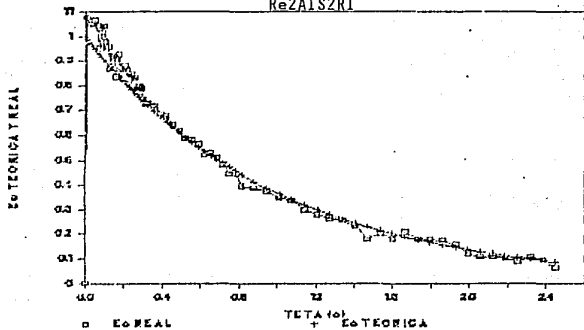


FIG. 3.22
Re2A1S2R1

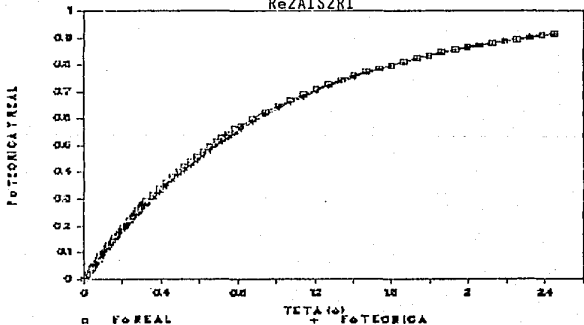


FIG. 3.23
Re2A1S2R2

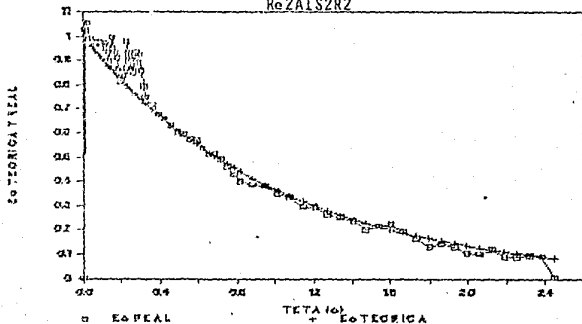


FIG. 3.24
Re2A1S2R2

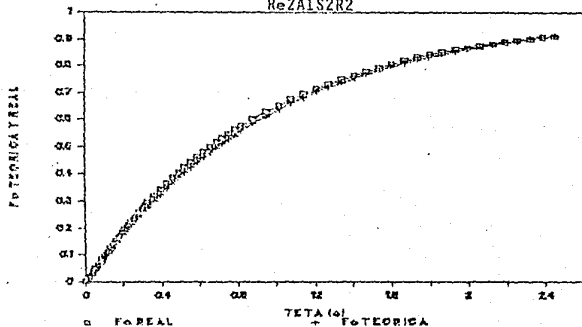


FIG. 3.25
Re2A2S1R1

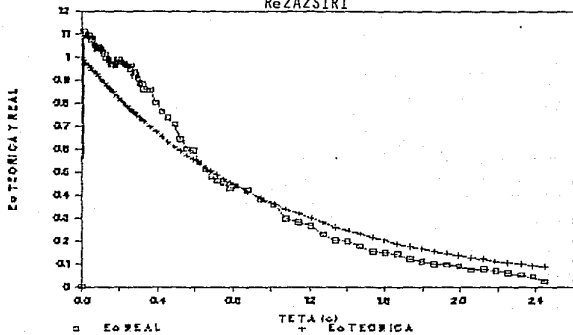


FIG. 3.26
Re2A2S1R1

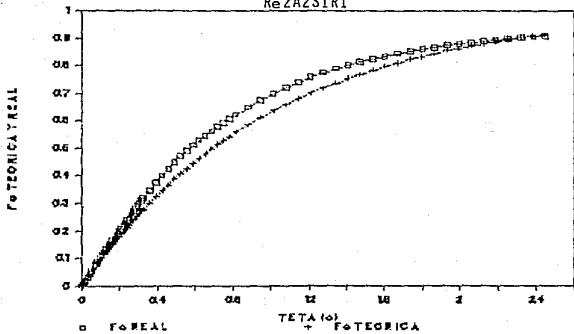


FIG. 3.27
Re 2A2S1R2

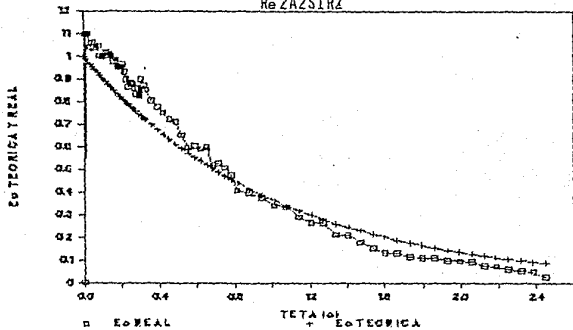


FIG. 3.28
Re 2A2S1R2

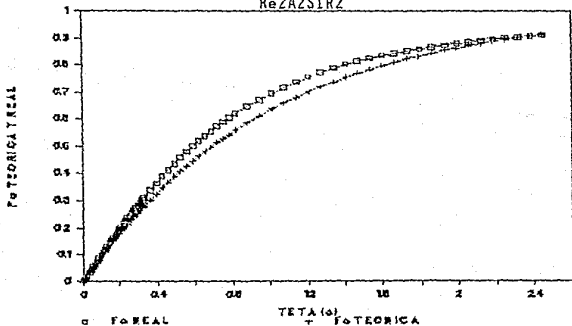


FIG. 3.29
ReZAZSR1

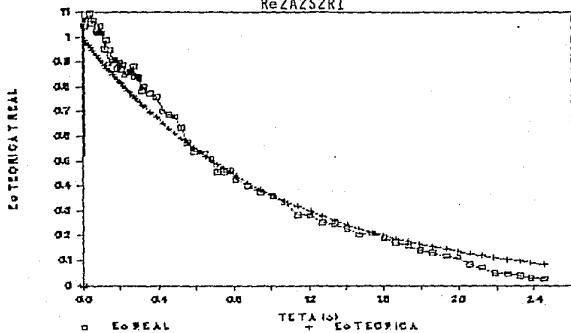


FIG. 3.30
ReZAZSR1

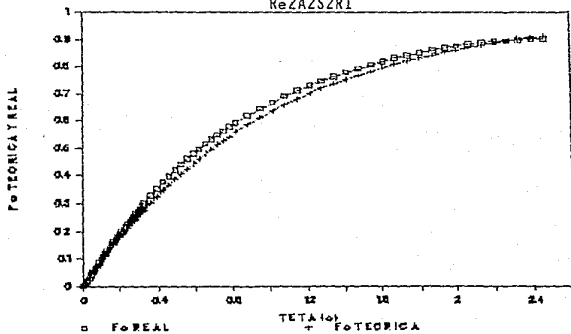


FIG. 3.31
Re2A2S2R2

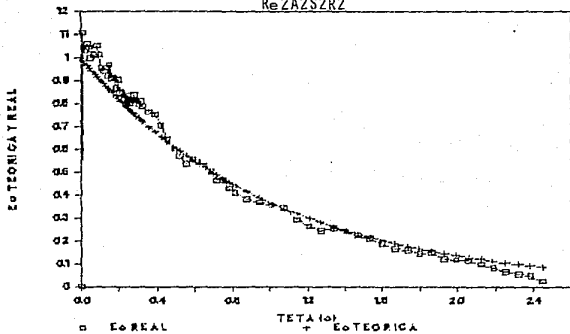
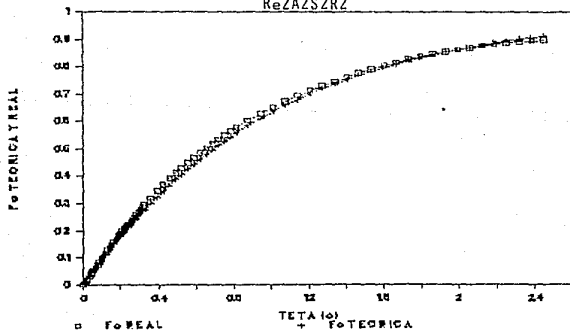


FIG. 3.32
Re2A2S2R2



CAPÍTULO 4

ANÁLISIS ESTADÍSTICO

ANÁLISIS ESTADÍSTICO

Para el análisis estadístico de los resultados obtenidos se aplicó la prueba de Kolmogorov-Smirnov para funciones de distribución de frecuencias.

Esta prueba fue aplicada a cada una de las corridas, comparándolas con el modelo ideal de mezcla completa usando el análisis unimuestral y además el bimuestral para la comparación entre dos muestras (corrida y réplica). Para calcular el valor de las frecuencias experimentales se utilizó la ecuación 1.6. Las tablas se muestran en el apéndice VI.

A continuación se da a conocer la información obtenida por el análisis estadístico.

La tabla 4.1 muestra los valores de D a distintos niveles de significancia, los cuales se utilizarán para ver si la diferencia máxima sobrepasa o no dichos valores, cuando se compara una distribución experimental con una teórica (tabla 4.2), o cuando se compara el promedio de dos distribuciones experimentales con la distribución teórica (tabla 4.3).

TABLA 4.1

N= 70 datos

| α | D |
|----------|--------|
| 1 % | 0.1948 |
| 5 % | 0.1626 |
| 10 % | 0.1458 |
| 15 % | 0.1363 |
| 20 % | 0.1279 |

En la tabla 4.2 se expone el análisis estadístico entre los datos experimentales para cada prueba y su réplica y los datos teóricos calculados a partir de la ecuación 1.6.

TABLA 4.2

| No. | CORRIDA | DIF-A | No. | CORRIDA | DIF-A |
|-----|-----------|--------|-----|-----------|--------|
| 1 | Re1A1S1R1 | 0.0352 | 9 | Re2A1S1R1 | 0.0257 |
| 2 | Re1A1S1R2 | 0.0446 | 10 | Re2A1S1R2 | 0.0208 |
| 3 | Re1A1S2R1 | 0.0677 | 11 | Re2A1S2R1 | 0.0158 |
| 4 | Re1A1S2R2 | 0.0605 | 12 | Re2A1S2R2 | 0.0206 |
| 5 | Re1A2S1R1 | 0.0366 | 13 | Re2A2S1R1 | 0.0667 |
| 6 | Re1A2S1R2 | 0.0553 | 14 | Re2A2S1R2 | 0.0622 |
| 7 | Re1A2S2R1 | 0.0706 | 15 | Re2A2S2R1 | 0.0357 |
| 8 | Re1A2S2R2 | 0.0778 | 16 | Re2A2S2R2 | 0.0244 |

ho: Los datos experimentales y teóricos siguen la misma distribución.

Para $DIF-A \text{ MAX} > D$, se rechaza ho.

En ninguno de los casos se rechaza ho.

La tabla 4.3 nos muestra el análisis estadístico aplicado al promedio de frecuencias entre la corrida y su réplica y el valor de frecuencias teóricas calculado por la ecuación 1.5.

TABLA 4.3

| PRUEBA | A*MAX |
|-------------|--------|
| Re1A1S1R1R2 | 0.0383 |
| Re1A1S2R1R2 | 0.0641 |
| Re1A2S1R1R2 | 0.0459 |
| Re1A2S2R1R2 | 0.0742 |
| Re2A1S1R1R2 | 0.0227 |
| Re2A1S2R1R2 | 0.0182 |
| Re2A2S1R1R2 | 0.0630 |
| Re2A2S1R1R2 | 0.0293 |

ho: Los datos experimentales y teóricos de la frecuencia acumulada siguen la misma distribución.

Para $A^* \text{ MAX} > D$ se rechaza ho.

En ninguno de los casos se rechaza ho.

La tabla 4.4 muestra los valores críticos de D a distintos niveles de significancia cuando se quieren comparar dos distribuciones experimentales (tabla 4.5), para decidir si se rechaza o no la hipótesis nula:

TABLA 4.4

n=m= 70 datos

| α | D |
|----------|--------|
| 0.1 % | 0.3296 |
| 0.5 % | 0.2924 |
| 1.0 % | 0.2755 |
| 2.5 % | 0.2501 |
| 5.0 % | 0.2299 |
| 10.0 % | 0.2062 |

La tabla 4.5 muestra los valores obtenidos del análisis estadístico entre réplicas.

TABLA 4.5

| PRUEBA | (FeR1-FeR2)MAX |
|---------|----------------|
| Re1A1S1 | 0.0141 |
| Re1A1S2 | 0.0071 |
| Re1A2S1 | 0.0199 |
| Re1A2S2 | 0.0131 |
| Re2A1S1 | 0.0102 |
| Re2A1S2 | 0.0111 |
| Re2A2S1 | 0.0126 |
| Re2A2S2 | 0.0170 |

ho: La prueba y su réplica siguen la misma distribución.
 Para $(FeR1-FeR2)MAX > D$, se rechaza ho.
 En ninguno de los casos anteriores se rechaza ho.

CAPÍTULO 5

DISCUSIÓN DE RESULTADOS

D I S C U S I Ó N D E R E S U L T A D O S

Los análisis estadísticos aplicados en este estudio nos dan la siguiente información:

1. En base a los datos estadísticos obtenidos aplicados entre la prueba y su réplica, vemos que éstas siguen la misma distribución, o sea, que no presentan diferencia significativa entre ellas.

2. El análisis estadístico aplicado a las pruebas que corresponden a la salida uno y dos (figs. 2.1 y 2.2), nos permite observar que no hay una diferencia notoria en la distribución de frecuencias, por lo que podemos decir que la Distribución de Tiempos de Residencia del solido no se ve afectada por este parámetro.

3. En las pruebas realizadas en el tanque con fondo de cono y filete, observamos cierta diferencia en la distribución de frecuencias, al comparar visualmente las dos posiciones del agitador (figs. 5.1 y 5.2). En la posición número uno podemos decir que hay una ligera tendencia al fenómeno de By-Pass (figs. 3.17 y 3.21) a diferencia de las pruebas realizadas en este mismo tanque, pero con la posición de agitación número dos que no presentan dicho fenómeno. Sin embargo, ninguna de las pruebas en particular sigue una distribución de frecuencias alejada de la idealidad, de acuerdo al criterio de Kolmogorov, pues en ninguno de los casos se rechaza la hipótesis nula correspondiente.

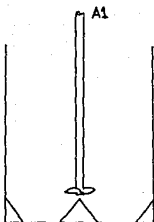


figura 5.1

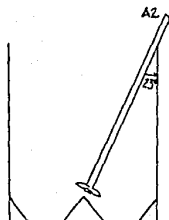


figura 5.2

Hay que hacer notar que la prueba estadística aplicada en este estudio no es lo suficientemente sensible para detectar desviaciones pequeñas, como en el caso anteriormente expuesto. A pesar de esto, al observar las gráficas de las pruebas correspondientes, se detecta la tendencia al fenómeno del By-Pass y podemos decir que esta tendencia no se presenta al azar porque hay repetibilidad de resultados.

Esta observación me hace pensar en el comportamiento que tendría esta prueba estadística ya a un nivel industrial, como en el caso de reacciones de polimerización. En este caso en particular, pienso que la distribución de pesos moleculares de un cierto polímero se vería afectada más notoriamente por el fenómeno del By-Pass.

Por otra parte, al terminar cada prueba se revisaba el tanque para ver si quedaba arena en el fondo de éste.

En ninguno de los casos se registró una cantidad considerable de trazador. Esto se logró haciendo un barrido de velocidades de agitación con diferentes tipos de propela. Llegando así, a una velocidad óptima con la propela adecuada. En estudios anteriores se han presentado problemas de asentamiento de trazador debido al tamaño de partícula de éste. El trazador utilizado en este estudio tiene un tamaño de partícula tal, que nos permite mantener una suspensión casi completa, logrando así que no tengamos cantidades considerables de trazador, en el fondo del tanque, al final de cada prueba. Otra opción para evitar este problema, sería creando corrientes verticales y laterales con el uso de deflectores en la pared del tanque, pero se necesitaría una potencia de agitación muy alta para evitar la formación de volúmenes muertos. Esta última opción corresponde a la parte II de este estudio (10).

RESUMEN

RESUMEN

Esta tesis tiene como objetivo determinar la influencia en la geometría del fondo de un reactor continuo de mezcla completa en combinación con dos diferentes posiciones del agitador y las salidas del fluido, en la distribución de tiempos de residencia de un sólido.

Las geometrías de fondo que se sometieron a comparación fueron: la convencional de fondo plano y la de cono y filete. Las posiciones del agitador empleadas fueron la posición vertical y la posición inclinada (25° con respecto a la pared del tanque), y las salidas del fluido se encuentran a 10 y 22 cm con respecto al fondo del tanque.

Las pruebas efectuadas nos proporcionan información mediante la cual podemos valorar la desviación que existe con respecto a los datos teóricos.

Para ello se recurre a un estudio estadístico que emplea la prueba de Kolmogorov-Smirnov, para funciones de distribución de frecuencias y al análisis visual de las gráficas, que nos ayudaran a apreciar la influencia de dichos parámetros en la distribución de tiempos de residencia.

Para llevar a cabo los cálculos, se recurrió a un paquete de cómputo que contiene una hoja de cálculo (Lotus) así como para la redacción de esta tesis y la

elaboración de las gráficas reportadas.

CONCLUSIONES

CONCLUSIONES

De acuerdo con los datos obtenidos podemos decir que el objetivo de esta investigación fue alcanzado, es decir, analizar la influencia del ángulo del agitador y la geometría de fondo de un tanque continuo de mezcla completa en la distribución de tiempos de residencia de un sólido.

En base a los resultados podemos decir que las dos réplicas para cada prueba son consistentes.

Por el análisis visual de las gráficas, se llegó a la conclusión de que la distribución de tiempos de residencia de un sólido se ve afectada ligeramente por la geometría de fondo del tanque y que la posición del agitador, en un tanque con fondo de cono y filete puede llegar a influir en el comportamiento de la distribución del trazador, aunque este efecto es suficientemente pequeño para que al utilizar la prueba unimuestral de Kolmogorov-Smirnov, hasta niveles de significancia del 20 %, no pueda rechazarse la hipótesis de que los datos experimentales siguen la misma distribución que los datos teóricos, para cada una de las pruebas realizadas en este estudio.

Sin embargo no podemos negar que existe, en algunas de las pruebas realizadas, cierta tendencia al fenómeno del By-Pass (mencionado en el capítulo 5) que nos hace pensar que, para este estudio, la prueba de Kolmogorov-

Smirnov no es lo suficientemente sensible para detectar esta desviación al modelo teórico de mezcla completa, a pesar que en las gráficas correspondientes de E_a vs a , se observa la tendencia a este fenómeno.

Por otra parte, no se observó ninguna diferencia en cuanto a la posición de salida del fluido. Esta diferencia podría llegarse a presentar si la posición de salida número uno estuviera más por encima del fondo del tanque, por lo que se recomienda para estudios posteriores tomar en cuenta este parámetro.

APÉNDICE I

PRUEBA DE KOLMOGOROV-SMIRNOV

P R U E B A D E K O L M O G O R O V - S M I R N O V
PARA FUNCIONES DE DISTRIBUCION DE FRECUENCIAS
(BONDAD DE AJUSTE)

La prueba de Kolmogorov tiene la siguientes variantes:

-La prueba unimuestral.

-La prueba bimuestral o de Kolmogorov-Smirnov.

A. PRUEBA UNIMUESTRAL.-

Esta prueba consiste en la comparación de la distribución de un conjunto de valores de una prueba experimental con alguna distribución teórica. Ayuda a decidir si, razonablemente, puede pensarse que los datos de la prueba experimental provienen de una población que tenga esa distribución teórica.

La prueba conlleva la especificación de la distribución de frecuencia acumulativa, que puede llegar a ocurrir bajo la distribución de la frecuencia teórica comparando con la frecuencia acumulativa observada.

En éstas dos distribuciones, hay un punto en donde existe una mayor divergencia, el cual es calculado y es la clave final para decidir el rechazo o la aceptación de la hipótesis nula. La distribución de frecuencias teóricas presenta lo esperado conforme a dicha hipótesis.

A continuación se da a conocer el método seguido por esta prueba considerando que las funciones de

una ecuación continua. El valor máximo de estos dos parámetros es el que se compara con los valores críticos de la tabla I-2 para decidir si se rechaza H_0 , a los diferentes niveles de significancia dados.

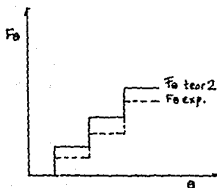


Figura I-1

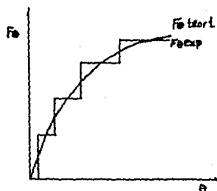


Figura I-2

B. PRUEBA DE KOLMOGOROV-SMIRNOV BIMESTRAL.-

Esta prueba se aplica para comparar dos muestras independientes y nos permite confirmar si han sido extraídas de la misma población.

Si existe una gran divergencia entre las distribuciones acumulativas de estas muestras, la hipótesis nula se rechaza. Por el contrario, si esta divergencia no se presenta, se puede aceptar que las dos muestras han sido extraídas de la misma población.

Si tomamos en cuenta que las funciones de distribución de frecuencias provienen también de una ecuación que da valores discretos, el método a seguir es

el siguiente:

Se examina la diferencia entre la función observada en la prueba F_{eR1} (e) y la función observada en otra prueba o réplica F_{eR2} (e).

Se toma el valor mayor de la diferencia

$$DIF(R1-R2) = \left\{ F_{eR1} (e) - F_{eR2} (e) \right\}$$

al cual se le nombra $DIF(R1-R2) \text{ MAX.}$ Este valor se compara con los valores críticos a diferentes niveles de significancia presentados en la tabla I-2, para después decidir si se rechaza o no la hipótesis nula, H_0 .

TABLA I-1

| TAMANO DE MUESTRA N | NIVEL DE SIGNIFICANCIA PARA D | | | | |
|------------------------|-------------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | 20 % | 15 % | 10 % | 5 % | 1 % |
| > 35 | $\frac{1.07}{\sqrt{N}}$ | $\frac{1.14}{\sqrt{N}}$ | $\frac{1.22}{\sqrt{N}}$ | $\frac{1.36}{\sqrt{N}}$ | $\frac{1.63}{\sqrt{N}}$ |

TABLA I-2

| α | 10 % | 5 % | 2.5 % | 1 % | 0.5 % | 0.1 % |
|----------|--------|--------|--------|--------|--------|--------|
| D | 1.22*f | 1.36*f | 1.48*f | 1.63*f | 1.73*f | 1.95*f |

en donde $f = \sqrt{\frac{n+m}{nm}}$

APÉNDICE II

DESCRIPCIÓN DEL EQUIPO

DESCRIPCIÓN DEL EQUIPO

Se usaron dos tanques: uno de fondo plano y otro de fondo de cono y filete. Ambos son de lámina galvanizada de 1.6mm de espesor y están hechos a mano. Tienen 40 cm de sección recta por 25 cm de diámetro (ver figs. II-1 y II-2).

El tanque de fondo plano tiene una forma de fondo de casquete esférico de 2 cm de profundidad. El tanque de fondo cónico tiene un filete a lo largo de toda la circunferencia de éste, con una inclinación de 45° con respecto al fondo. En la parte media del fondo tiene un cono hacia arriba con una altura de 5 cm y una base circular de 7.5 cm de diámetro.

Ambos tanques tienen perforaciones que están colocadas a 180° , en las que van soldados casquillos de 5.08 cm de largo, 6.35 mm de diámetro y 8 mm de espesor, y los cuales constituyen las entradas y salidas de estos tanques.

Para nuestra investigación se empleó una entrada para el flujo y una salida para el mismo, además se empleó uno de los orificios de las salidas para conectar el indicador de nivel.

Para el tanque de fondo plano, el volumen real del tanque es de 20.4 l, pero el volumen de trabajo fue de 12.7 l, con un nivel de líquido de 23.2 cm, sin agitación. Para el tanque de fondo cónico, el volumen

real es de 18.93 l y el volumen de trabajo fue de 12.7 l, con un nivel de operación de 27 cm, sin agitación.

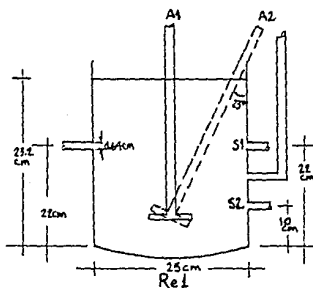


Figura II-1

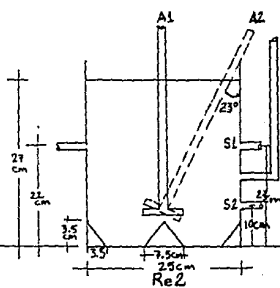


Figura II-2

Se utilizó un agitador marca Caframo de 70 W, 115 V y 60 Hz de corriente alterna. El agitador consta de una flecha de 0.85 cm de diámetro, con un aspa de tipo turbina de hoja sumergida de 10.5 cm de longitud y 4.57 cm de ancho.

Se empleó como tanque de alimentación un recipiente de lámina, alimentado por una manquera. Este tanque estuvo colocado a una altura de 2.30 m, en una estructura que también sostenía todo el equipo empleado. Dicho tanque tenía adaptado un rebosadero para mantener el nivel constante y eliminar el exceso de fluido en el recipiente, así se mantenía la presión hidrostática constante.

Se utilizó un rotámetro para medir el flujo de

entrada al sistema. y para regular dicho flujo se emplearon dos llaves de paso a la entrada y salida del tanque. Para adicionar el trazador se empleó un embudo en la parte superior del tanque cercano a la flecha del agitador. Para recolectar las muestras se usaron setenta tubos de ensayo de 33.5 ml y los tiempos de recolección de muestras fueron medidos con un cronómetro marca Valessa. Para eliminar el exceso de agua en las muestras con trazador, se utilizó un secador marca Felissa y para pesar los tubos se usó una balanza analítica marca O-Hauss. El trazador que se utilizó fue arena sílica de 0.114 mm de diámetro constante (arena para filtros industriales) y se empleó agua como fluido, por su fácil manejo y bajo costo.

APÉNDICE III

CALIBRACIÓN DEL ROTÁMETRO

CALIBRACIÓN DEL ROTÁMETRO

La calibración del medidor de flujo o rotámetro involucra la relación entre la diferencia de presión de éste con el caudal del líquido que fluye.

Ya obtenida esta relación, basta con leer la diferencia de presión (diferencia de altura) y sustituir ésta en la siguiente ecuación:

$$Q = A \Delta h \quad \text{ec. III-1}$$

donde: Q = Caudal del fluido

Δh = Diferencia de presión o altura

A = Constante de orificio

B = Constante de orificio

Aplicando logaritmo natural a la ec. III-1, linealizamos ésta, obteniendo

$$\ln Q = \ln A + B \ln \Delta h \quad \text{ec. III-2}$$

donde A y B se conocen por regresión lineal o por medio de una gráfica de $\ln Q$ vs. $\ln \Delta h$.

El siguiente procedimiento es el que se siguió para la calibración:

1. Se llena el tanque de alimentación.
2. Se abre la llave de paso, lo que origina una caída de presión en el rotámetro, a una altura determinada de la canica.
3. A esta altura, se toma el volumen en un tiempo fijo (en este caso un minuto).
4. Esta operación se realiza a diferentes alturas de la

bolita en el rotámetro, lo cual se consigue abriendo o cerrando la llave de paso, provocando que haya mayor o menor diferencia de presión.

5. Ya que obtenemos los volúmenes a diferentes alturas, en un tiempo fijo, se aplica la regresión lineal con estas parejas de datos, conforme a la ecuación III-2.
6. Viendo el valor de la correlación entre los puntos, podemos decir si los datos corresponden a una recta. Si es así, la pendiente y la ordenada al origen nos dan las constantes de orificio A y B.

Los datos que se obtuvieron se muestran en la tabla III-1, así como la gráfica obtenida con estos valores (fig. III-1).

TABLA III-1

| H | Q (ml/min) | $\ln \Delta h$ | $\ln Q$ |
|-----|------------|----------------|---------|
| 10 | 210.0 | 2.3026 | 5.3471 |
| 20 | 415.0 | 2.9957 | 6.0282 |
| 30 | 618.0 | 3.4012 | 6.4265 |
| 40 | 821.5 | 3.6888 | 6.7105 |
| 50 | 1018.0 | 3.9120 | 6.9256 |
| 60 | 1251.5 | 4.0943 | 7.1321 |
| 70 | 1493.0 | 4.2484 | 7.3085 |
| 80 | 1706.3 | 4.3820 | 7.4421 |
| 90 | 1919.6 | 4.4998 | 7.5599 |
| 100 | 2132.8 | 4.6052 | 7.6652 |

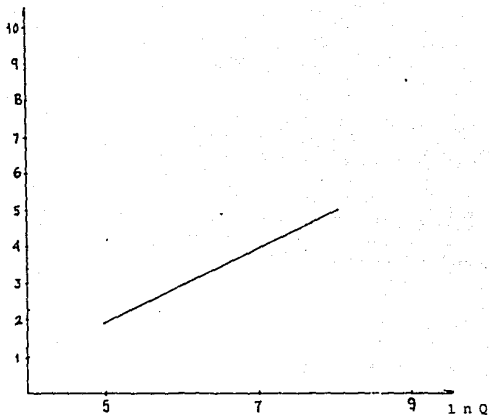
$\ln \Delta h$ 

Figura III-1.

GRAFICA DE CALIBRACION
DEL ROTAMETRO

APÉNDICE IV

CÁLCULOS REALIZADOS

CÁLCULOS REALIZADOS

A. CÁLCULOS EFECTUADOS EN EL CAPÍTULO 3.-

Los cálculos fueron efectuados con las ecuaciones que a continuación se dan:

1. Concentración promedio de arena en el tanque, (C):

$$C = \frac{100}{V} \left(\frac{g}{l} \right) \quad \text{ec. IV-A1}$$

esta concentración se mantiene constante para todas las corridas.

2. Concentración de arena para cada tubo de ensayo,

(CT):

$$CT = \frac{W_{\text{Total}} - W_{\text{Seco}}}{\text{Volumen del tubo}} \left(\frac{g}{l} \right) \quad \text{ec. IV-A2}$$

3. Esperanza de teta, (Ee):

$$Ee = \frac{CT}{C} \left(\frac{g/l}{g/l} \right) \quad \text{ec. IV-A3}$$

4. Teta, (e):

$$e = \frac{t}{r} \left(\frac{s}{s} \right) \quad \text{ec. IV-A4}$$

5. Frecuencia de teta, (Fe):

$$Fe = \frac{[Ee(i+1) + Ee(i)] * [e(i+1) - e(i)]}{2} \quad \text{ec. IV-A5}$$

6. Esperanza de teta teórica, (Ee Teor):

$$Ee = \exp(-e) \quad \text{ec. IV-A6}$$

7. Frecuencia de teta teórica para valores continuos,

(Fe teor):

$$Fe = 1 - \exp(-e) \quad \text{ec. IV-A7}$$

B. Frecuencia de teta teórica para valores discretos.

(F_{θ} teor2):

$$F_{\theta} \text{ teor2} = \frac{[E_{\theta}(i+1) - E_{\theta}(i)]}{2} * [e(i+1) - e(i)] \quad \text{ec. IV-AB}$$

Nota: El calculo de F_{θ} teor1 y F_{θ} teor2 se lleva a cabo con valores de E_{θ} teóricos.

B. CÁLCULOS EFECTUADOS PARA EL ANÁLISIS ESTADÍSTICO MOSTRADO EN EL APÉNDICE VI.-

Las ecuaciones dadas a continuación se aplican cuando el análisis estadístico se va a efectuar entre datos de frecuencias acumuladas, teóricas y experimentales y que son obtenidos a partir de ecuaciones que dan valores discretos:

$$DIF-A = |F_{\theta} \text{ teor2} - F_{\theta}| \quad \text{ec. IV-B1}$$

$$DIF(R1-R2) = |F_{\theta R1} - F_{\theta R2}| \quad \text{ec. IV-B2}$$

La ecuación IV-B1 se aplica cuando queremos conocer la divergencia entre la curva experimental y la teórica en cada corrida. La ecuación IV-B2 se aplica para observar la divergencia entre réplicas.

Para cada prueba se toma el valor máximo de cada una de estas diferencias, para luego ser comparado con cada valor crítico D_c a distintos niveles de significancia. Si el valor máximo obtenido es mayor que el crítico (D_c), se rechaza la hipótesis nula.

Cuando el análisis estadístico se aplica para la comparación entre dos pruebas en las que la frecuencia acumulada experimental se obtiene de una ecuación que da valores discretos y la frecuencia acumulada teórica es

obtenida de una ecuación que da valores continuos, se calculan las siguientes diferencias que a continuación se proponen:

$$A^{\circ}1 = |F_e \text{ teor1}(e) - F_e (e-1)| \quad \text{ec. IV-B3}$$

$$A^{\circ}2 = |F_e \text{ teor1}(e) - F_o (e)| \quad \text{ec. IV-B4}$$

El valor máximo de las diferencias obtenidas en cada prueba es el que se compara con los valores críticos (D), a distintos niveles de significancia (tabla I-1). Si este valor máximo es mayor que cualquier valor de D, la hipótesis nula se rechaza.

APÉNDICE V

TABLAS DE RESULTADOS

TABLAS DE RESULTADOS

Las tablas de resultados que se presentan a continuación tienen una numeración del uno al dieciseis. El primer dígito corresponde al número del apéndice (o sea apéndice V) y el segundo dígito corresponde al número de la prueba.

Por otra parte, las tablas presentan un encabezado que se refiere a las variantes en cuestión. Re se refiere al tipo de fondo del tanque, A corresponde a la posición del agitador, S se refiere a la salida del fluido, R1 es la prueba y R2 es la réplica de la prueba correspondiente. Los encabezados de cada una de las columnas que componen las tablas están definidos en el Capítulo 3.

VARIABLES DE ESTUDIO:

1. Geometría de Fondo.

- Plano (Re1).
- De cono y filate (Re2).

2. Posición de Agitador.

- Recta (A1).
- Angular (A2).

3. Salida del Fluido.

- 22cm del fondo del tanque (S1).
- 10 cm del fondo del tanque (S2).

TABLA V-1
Número

| | tiempo | tota | W Total | RelAISIR1 W Seco | Fa | EW Teor | Fa | Fa Teor |
|---------|--------|--------|----------|---------------------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.0292 | 21.0292 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.2897 | 21.0160 | 0.9817 | 0.9892 | 0.0052 | 0.0108 |
| 2 | 20 | 0.0218 | 21.4240 | 21.1733 | 0.9593 | 0.9785 | 0.0157 | 0.0215 |
| 3 | 30 | 0.0327 | 21.18751 | 21.8220 | 0.9594 | 0.9679 | 0.0261 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6213 | 21.3641 | 0.9750 | 0.9574 | 0.0366 | 0.0426 |
| 5 | 50 | 0.0545 | 22.2227 | 21.9825 | 0.9105 | 0.9470 | 0.0469 | 0.0530 |
| 6 | 60 | 0.0654 | 21.3976 | 21.1575 | 0.9102 | 0.9387 | 0.0568 | 0.0633 |
| 7 | 70 | 0.0762 | 22.0838 | 21.8450 | 0.9052 | 0.9266 | 0.0667 | 0.0734 |
| 8 | 80 | 0.0871 | 20.7960 | 20.5534 | 0.9196 | 0.9185 | 0.0766 | 0.0835 |
| 9 | 90 | 0.0980 | 22.0620 | 21.8285 | 0.8851 | 0.9066 | 0.0864 | 0.0934 |
| 10 | 100 | 0.1089 | 21.4012 | 21.1730 | 0.8650 | 0.8968 | 0.0960 | 0.1032 |
| 11 | 110 | 0.1196 | 21.5669 | 21.3403 | 0.8590 | 0.8871 | 0.1053 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6287 | 21.4048 | 0.8487 | 0.8775 | 0.1146 | 0.1225 |
| 13 | 130 | 0.1414 | 21.0292 | 20.8010 | 0.8550 | 0.8680 | 0.1240 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2329 | 21.0020 | 0.8753 | 0.8586 | 0.1335 | 0.1414 |
| 15 | 150 | 0.1634 | 20.5853 | 20.3598 | 0.8700 | 0.8493 | 0.1430 | 0.1507 |
| 16 | 160 | 0.1743 | 21.3315 | 20.9972 | 0.8503 | 0.8401 | 0.1523 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4192 | 21.2030 | 0.8196 | 0.8310 | 0.1614 | 0.1690 |
| 18 | 180 | 0.1961 | 21.1222 | 20.9006 | 0.8400 | 0.8220 | 0.1705 | 0.1780 |
| 19 | 190 | 0.2070 | 21.2064 | 20.9942 | 0.8044 | 0.8131 | 0.1794 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0342 | 20.8370 | 0.7854 | 0.8042 | 0.1881 | 0.1958 |
| 21 | 210 | 0.2287 | 21.5917 | 21.3978 | 0.7350 | 0.7955 | 0.1964 | 0.2045 |
| 22 | 220 | 0.2396 | 21.2535 | 21.0585 | 0.7506 | 0.7869 | 0.2045 | 0.2131 |
| 23 | 230 | 0.2505 | 21.2070 | 21.0053 | 0.7646 | 0.7784 | 0.2127 | 0.2216 |
| 24 | 240 | 0.2614 | 21.4043 | 21.2029 | 0.7638 | 0.7700 | 0.2210 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2357 | 21.0498 | 0.7388 | 0.7616 | 0.2292 | 0.2384 |
| 26 | 260 | 0.2832 | 23.1072 | 21.9149 | 0.7290 | 0.7534 | 0.2372 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7012 | 21.5932 | 0.7127 | 0.7452 | 0.2451 | 0.2548 |
| 28 | 280 | 0.3050 | 21.4680 | 21.2856 | 0.6914 | 0.7371 | 0.2527 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5256 | 21.3406 | 0.7013 | 0.7291 | 0.2603 | 0.2709 |
| 30 | 300 | 0.3268 | 21.8946 | 21.4334 | 0.6490 | 0.7212 | 0.2676 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4308 | 21.2641 | 0.6598 | 0.6981 | 0.2892 | 0.3019 |
| 32 | 360 | 0.3921 | 21.0887 | 20.9085 | 0.6952 | 0.6756 | 0.3115 | 0.3244 |
| 33 | 390 | 0.4248 | 20.8267 | 20.6457 | 0.6854 | 0.6539 | 0.3340 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4858 | 21.2910 | 0.6247 | 0.6329 | 0.3555 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1557 | 21.0008 | 0.6251 | 0.6125 | 0.3759 | 0.3875 |
| 36 | 480 | 0.5230 | 21.5419 | 21.1733 | 0.6391 | 0.5928 | 0.3945 | 0.4072 |

TABLA V-1
Número

| | tiempo | continuación.. | | Relatividad | | Es | Es teor | Fe | Fe Teor |
|----|--------|----------------|---------|-------------|--------|--------|---------|--------|---------|
| | | total | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.3887 | 21.2265 | 0.6149 | 0.5738 | 0.4170 | 0.4262 | |
| 38 | 540 | 0.5682 | 21.3665 | 21.2122 | 0.5849 | 0.5553 | 0.4366 | 0.4447 | |
| 39 | 570 | 0.5209 | 21.3807 | 21.2352 | 0.5516 | 0.5375 | 0.4552 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4625 | 21.3239 | 0.5254 | 0.5202 | 0.4728 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.7046 | 21.5677 | 0.5190 | 0.5035 | 0.4898 | 0.4965 | |
| 42 | 660 | 0.7169 | 21.0867 | 20.9535 | 0.5049 | 0.4873 | 0.5066 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1993 | 21.0720 | 0.4826 | 0.4716 | 0.5227 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.8680 | 21.7414 | 0.4799 | 0.4565 | 0.5384 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2640 | 21.1387 | 0.4750 | 0.4418 | 0.5540 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.2002 | 21.0880 | 0.4253 | 0.4138 | 0.5835 | 0.5862 | |
| 47 | 870 | 0.9476 | 20.6724 | 20.5723 | 0.3795 | 0.3877 | 0.6098 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5223 | 21.4273 | 0.3601 | 0.3631 | 0.6339 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7529 | 20.6665 | 0.3275 | 0.3402 | 0.6564 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3814 | 21.3022 | 0.3002 | 0.3186 | 0.6769 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4574 | 21.3826 | 0.2835 | 0.2985 | 0.6960 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.0915 | 21.0200 | 0.2710 | 0.2796 | 0.7141 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7612 | 20.6912 | 0.2654 | 0.2619 | 0.7316 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9204 | 20.8560 | 0.2441 | 0.2453 | 0.7483 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1718 | 21.1110 | 0.2305 | 0.2298 | 0.7638 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1598 | 21.1062 | 0.2032 | 0.2153 | 0.7780 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2185 | 21.1645 | 0.2047 | 0.2017 | 0.7913 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0143 | 20.9658 | 0.1839 | 0.1889 | 0.8040 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8251 | 20.7804 | 0.1694 | 0.1769 | 0.8155 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9547 | 20.9112 | 0.1649 | 0.1658 | 0.8265 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.3014 | 21.2579 | 0.1649 | 0.1553 | 0.8372 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7155 | 20.6759 | 0.1501 | 0.1454 | 0.8475 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2652 | 21.2269 | 0.1452 | 0.1362 | 0.8572 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.2048 | 21.1705 | 0.1300 | 0.1276 | 0.8662 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6925 | 21.6530 | 0.1497 | 0.1196 | 0.8753 | 0.8804 | |
| 66 | 2010 | 2.1694 | 20.9962 | 20.9606 | 0.1350 | 0.1120 | 0.8846 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7621 | 20.7380 | 0.0914 | 0.1049 | 0.8920 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4231 | 21.4009 | 0.0842 | 0.0983 | 0.8977 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1177 | 21.0902 | 0.1042 | 0.0920 | 0.9039 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9524 | 20.9533 | 0.0604 | 0.0862 | 0.9073 | 0.9138 | |

TABLA V-2

| Número | tiempo | teta | W total | Retenido W Seco | Ea | Ea Teor | Fe | Fe Teor |
|---------|--------|--------|---------|--------------------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.5626 | 21.5626 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 22.0904 | 21.8351 | 0.9679 | 0.9892 | 0.0053 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2609 | 21.0052 | 0.9694 | 0.9785 | 0.0158 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8738 | 21.6230 | 0.9508 | 0.9679 | 0.0263 | 0.0321 |
| 4 | 40 | 0.0435 | 20.9704 | 20.7218 | 0.9425 | 0.9574 | 0.0366 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5535 | 21.2925 | 0.9205 | 0.9470 | 0.0467 | 0.0530 |
| 6 | 60 | 0.0654 | 21.1746 | 20.9355 | 0.9072 | 0.9367 | 0.0567 | 0.0633 |
| 7 | 70 | 0.0762 | 21.2657 | 21.0274 | 0.8958 | 0.9266 | 0.0665 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5445 | 21.3105 | 0.8871 | 0.9165 | 0.0762 | 0.0835 |
| 9 | 90 | 0.0980 | 21.1150 | 20.8837 | 0.8761 | 0.9066 | 0.0858 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3456 | 21.1145 | 0.8761 | 0.8968 | 0.0954 | 0.1032 |
| 11 | 110 | 0.1198 | 21.0701 | 20.6437 | 0.8583 | 0.8871 | 0.1048 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1245 | 20.8705 | 0.8568 | 0.8775 | 0.1142 | 0.1225 |
| 13 | 130 | 0.1416 | 21.2659 | 21.0316 | 0.8807 | 0.8680 | 0.1236 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2639 | 21.0473 | 0.8770 | 0.8586 | 0.1333 | 0.1414 |
| 15 | 150 | 0.1634 | 21.1180 | 20.8956 | 0.8431 | 0.8493 | 0.1428 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1311 | 20.9023 | 0.8674 | 0.8401 | 0.1521 | 0.1599 |
| 17 | 170 | 0.1852 | 21.1615 | 20.9715 | 0.7961 | 0.8310 | 0.1611 | 0.1690 |
| 18 | 180 | 0.1961 | 21.6626 | 21.4689 | 0.7377 | 0.8220 | 0.1695 | 0.1780 |
| 19 | 190 | 0.2070 | 20.9608 | 20.7805 | 0.7593 | 0.8131 | 0.1777 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4330 | 21.2543 | 0.7495 | 0.8042 | 0.1859 | 0.1958 |
| 21 | 210 | 0.2287 | 21.1130 | 20.9085 | 0.7753 | 0.7959 | 0.1942 | 0.2045 |
| 22 | 220 | 0.2396 | 21.0718 | 20.8615 | 0.7973 | 0.7869 | 0.2027 | 0.2131 |
| 23 | 230 | 0.2505 | 21.4545 | 21.2537 | 0.7612 | 0.7784 | 0.2112 | 0.2216 |
| 24 | 240 | 0.2614 | 21.2415 | 21.1463 | 0.7628 | 0.7700 | 0.2195 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2440 | 21.0388 | 0.7779 | 0.7616 | 0.2279 | 0.2384 |
| 26 | 260 | 0.2832 | 21.3185 | 21.1112 | 0.7859 | 0.7534 | 0.2364 | 0.2466 |
| 27 | 270 | 0.2941 | 21.6914 | 21.4903 | 0.7624 | 0.7452 | 0.2449 | 0.2548 |
| 28 | 280 | 0.3050 | 21.5522 | 21.3807 | 0.6502 | 0.7371 | 0.2526 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1530 | 20.9300 | 0.7355 | 0.7291 | 0.2601 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0528 | 20.8727 | 0.6828 | 0.7212 | 0.2678 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4009 | 21.2205 | 0.6839 | 0.6981 | 0.2902 | 0.3019 |
| 32 | 360 | 0.3921 | 21.4507 | 21.2876 | 0.6183 | 0.6756 | 0.3114 | 0.3244 |
| 33 | 390 | 0.4248 | 21.3643 | 21.2076 | 0.6699 | 0.6539 | 0.3325 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7643 | 21.5916 | 0.6547 | 0.6329 | 0.3541 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4462 | 21.2879 | 0.6001 | 0.6125 | 0.3746 | 0.3875 |
| 36 | 480 | 0.5228 | 21.1966 | 21.0565 | 0.5289 | 0.5928 | 0.3931 | 0.4072 |

TABLA V-2

| Número | Tiempo | continuación.. | | RETAISIR2 | | Ee | Ee Teor | Fe | Fe Teor |
|--------|--------|----------------|---------|-----------|--------|--------|---------|--------|---------|
| | | tota | W Total | W seco | | | | | |
| 37 | 510 | 0.5555 | 21.0070 | 20.8947 | 0.5406 | 0.5738 | 0.4105 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.1518 | 21.0205 | 0.4978 | 0.5553 | 0.4275 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.2247 | 21.0682 | 0.5933 | 0.5375 | 0.4453 | 0.4625 | |
| 40 | 600 | 0.6535 | 20.7350 | 20.8625 | 0.5023 | 0.5202 | 0.4632 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.3705 | 21.2470 | 0.4985 | 0.5035 | 0.4796 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.2931 | 21.1671 | 0.4853 | 0.4873 | 0.4957 | 0.5127 | |
| 43 | 690 | 0.7516 | 20.7906 | 20.8635 | 0.4818 | 0.4716 | 0.5115 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.1746 | 21.0543 | 0.4561 | 0.4565 | 0.5268 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.0325 | 20.9145 | 0.4473 | 0.4418 | 0.5416 | 0.5502 | |
| 46 | 810 | 0.8823 | 21.1285 | 21.0191 | 0.4147 | 0.4138 | 0.5697 | 0.5862 | |
| 47 | 870 | 0.9478 | 21.2050 | 21.1049 | 0.3795 | 0.3677 | 0.5957 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.1049 | 21.0103 | 0.3662 | 0.3631 | 0.6200 | 0.6369 | |
| 49 | 990 | 1.0783 | 21.3000 | 21.2059 | 0.3567 | 0.3402 | 0.6437 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.1471 | 21.0598 | 0.3310 | 0.3186 | 0.6661 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.2555 | 21.1725 | 0.3147 | 0.2985 | 0.6872 | 0.7015 | |
| 52 | 1170 | 1.2744 | 20.7385 | 20.6603 | 0.2965 | 0.2796 | 0.7072 | 0.7204 | |
| 53 | 1230 | 1.3398 | 21.0510 | 20.9752 | 0.2858 | 0.2619 | 0.7262 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9332 | 20.8636 | 0.2639 | 0.2453 | 0.7442 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.2826 | 21.2235 | 0.2241 | 0.2298 | 0.7601 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.2515 | 21.1977 | 0.2040 | 0.2153 | 0.7741 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.1512 | 21.1120 | 0.1965 | 0.2017 | 0.7856 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.9132 | 21.8620 | 0.1941 | 0.1889 | 0.7968 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8549 | 20.8056 | 0.1869 | 0.1769 | 0.8093 | 0.8231 | |
| 60 | 1650 | 1.7972 | 21.7760 | 21.7307 | 0.1717 | 0.1658 | 0.8210 | 0.8342 | |
| 61 | 1710 | 1.8625 | 21.4430 | 21.4005 | 0.1611 | 0.1553 | 0.8319 | 0.8447 | |
| 62 | 1770 | 1.9280 | 21.5413 | 21.4962 | 0.1710 | 0.1454 | 0.8427 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.3465 | 21.3107 | 0.1433 | 0.1362 | 0.8530 | 0.8638 | |
| 64 | 1890 | 2.0587 | 20.7985 | 20.7624 | 0.1369 | 0.1276 | 0.8622 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.4163 | 21.3791 | 0.1410 | 0.1196 | 0.8712 | 0.8804 | |
| 66 | 2010 | 2.1894 | 21.9883 | 21.9524 | 0.1361 | 0.1120 | 0.8803 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.9201 | 20.8939 | 0.1297 | 0.1049 | 0.8890 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.7832 | 21.7511 | 0.1217 | 0.0983 | 0.8972 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.3550 | 21.3276 | 0.1039 | 0.0920 | 0.9046 | 0.9080 | |
| 70 | 2250 | 2.4508 | 21.4440 | 21.4398 | 0.0159 | 0.0662 | 0.9085 | 0.9138 | |

ESTA
TESIS
NO
DEBE
SALIR
DE
LA
BIBLIOTECA

TABLA V-3
 Número

Relat1S2R1

| | Tiempo | leta | W Total | W Seco | Ee | Ee Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.0925 | 21.0925 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.2525 | 21.0160 | 0.8966 | 0.9892 | 0.0049 | 0.0108 |
| 2 | 20 | 0.0218 | 21.3981 | 21.1733 | 0.8522 | 0.9785 | 0.0144 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8963 | 21.6220 | 0.8503 | 0.9679 | 0.0237 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6019 | 21.3641 | 0.9015 | 0.9574 | 0.0332 | 0.0426 |
| 5 | 50 | 0.0545 | 22.2210 | 21.9825 | 0.9042 | 0.9470 | 0.0431 | 0.0530 |
| 6 | 60 | 0.0654 | 21.3759 | 21.1575 | 0.8280 | 0.9367 | 0.0525 | 0.0633 |
| 7 | 70 | 0.0762 | 22.0846 | 21.8450 | 0.9083 | 0.9266 | 0.0619 | 0.0734 |
| 8 | 80 | 0.0871 | 20.7742 | 20.5534 | 0.8371 | 0.9165 | 0.0715 | 0.0835 |
| 9 | 90 | 0.0980 | 22.0367 | 21.8285 | 0.7893 | 0.9066 | 0.0803 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3852 | 21.1730 | 0.8083 | 0.8968 | 0.0890 | 0.1032 |
| 11 | 110 | 0.1198 | 21.5666 | 21.3403 | 0.8579 | 0.8871 | 0.0981 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6185 | 21.4048 | 0.8101 | 0.8775 | 0.1072 | 0.1225 |
| 13 | 130 | 0.1416 | 21.0139 | 20.8010 | 0.8071 | 0.8680 | 0.1160 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2009 | 21.0020 | 0.7540 | 0.8586 | 0.1245 | 0.1414 |
| 15 | 150 | 0.1634 | 20.5548 | 20.3558 | 0.7544 | 0.8493 | 0.1327 | 0.1507 |
| 16 | 160 | 0.1743 | 21.2121 | 20.9972 | 0.8147 | 0.8401 | 0.1412 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4049 | 21.2030 | 0.7654 | 0.8310 | 0.1498 | 0.1690 |
| 18 | 180 | 0.1961 | 21.0925 | 20.9006 | 0.7275 | 0.8220 | 0.1580 | 0.1780 |
| 19 | 190 | 0.2070 | 21.1942 | 20.9942 | 0.7582 | 0.8131 | 0.1661 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0233 | 20.8270 | 0.7442 | 0.8042 | 0.1742 | 0.1958 |
| 21 | 210 | 0.2287 | 21.5831 | 21.3978 | 0.7025 | 0.7955 | 0.1821 | 0.2045 |
| 22 | 220 | 0.2396 | 21.2405 | 21.0555 | 0.7013 | 0.7869 | 0.1898 | 0.2131 |
| 23 | 230 | 0.2505 | 21.1946 | 21.0053 | 0.7176 | 0.7784 | 0.1975 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3870 | 21.2029 | 0.6979 | 0.7700 | 0.2052 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2432 | 21.0408 | 0.7673 | 0.7616 | 0.2132 | 0.2384 |
| 26 | 260 | 0.2832 | 22.0987 | 21.9149 | 0.6968 | 0.7534 | 0.2212 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7715 | 21.5932 | 0.6759 | 0.7452 | 0.2286 | 0.2548 |
| 28 | 280 | 0.3050 | 21.4733 | 21.2856 | 0.7116 | 0.7371 | 0.2362 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5350 | 21.3406 | 0.7370 | 0.7291 | 0.2441 | 0.2709 |
| 30 | 300 | 0.3268 | 21.6103 | 21.4234 | 0.7085 | 0.7212 | 0.2520 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4331 | 21.2621 | 0.6483 | 0.6981 | 0.2741 | 0.3019 |
| 32 | 360 | 0.3921 | 21.0784 | 20.9055 | 0.6555 | 0.6756 | 0.2954 | 0.3244 |
| 33 | 390 | 0.4248 | 20.8059 | 20.6459 | 0.6066 | 0.6539 | 0.3160 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4509 | 21.2910 | 0.6062 | 0.6329 | 0.3359 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1543 | 21.0008 | 0.5819 | 0.6125 | 0.3553 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3360 | 21.1733 | 0.5941 | 0.5928 | 0.3745 | 0.4072 |

TABLA V-3

| Número | tiempo | continuación.. | | RELATOSKI | | Ee | Ee Teor | Fe | Fe Teor |
|--------|--------|----------------|---------|-----------|--------|--------|---------|--------|---------|
| | | teta | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.3635 | 21.2265 | 0.5194 | 0.5738 | 0.3927 | 0.4262 | |
| 38 | 540 | 0.5802 | 21.3542 | 21.2122 | 0.5363 | 0.5553 | 0.4100 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3743 | 21.2352 | 0.5273 | 0.5375 | 0.4274 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4545 | 21.3239 | 0.4951 | 0.5202 | 0.4441 | 0.4798 | |
| 41 | 630 | 0.6852 | 21.6932 | 21.5677 | 0.4758 | 0.5035 | 0.4599 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.0731 | 20.9535 | 0.4534 | 0.4873 | 0.4751 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1922 | 21.0720 | 0.4557 | 0.4716 | 0.4900 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.0590 | 21.7414 | 0.4289 | 0.4565 | 0.5044 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2538 | 21.1387 | 0.4364 | 0.4418 | 0.5185 | 0.5582 | |
| 46 | 810 | 0.8623 | 21.1962 | 21.0680 | 0.4102 | 0.4138 | 0.5462 | 0.5862 | |
| 47 | 870 | 0.9478 | 20.6685 | 20.5723 | 0.3647 | 0.3877 | 0.5715 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5207 | 21.4273 | 0.3541 | 0.3631 | 0.5950 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7634 | 20.6665 | 0.3674 | 0.3402 | 0.6185 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3871 | 21.3022 | 0.3219 | 0.3186 | 0.6411 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4622 | 21.3826 | 0.3018 | 0.2985 | 0.6614 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.1027 | 21.0200 | 0.3135 | 0.2796 | 0.6816 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7667 | 20.6912 | 0.2862 | 0.2619 | 0.7012 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9284 | 20.8560 | 0.2745 | 0.2453 | 0.7195 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1828 | 21.1110 | 0.2722 | 0.2298 | 0.7373 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1760 | 21.1062 | 0.2419 | 0.2153 | 0.7541 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.3230 | 21.1645 | 0.2218 | 0.2017 | 0.7693 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0243 | 20.9658 | 0.2218 | 0.1889 | 0.7838 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8305 | 20.7804 | 0.1899 | 0.1769 | 0.7972 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9632 | 20.9112 | 0.1971 | 0.1658 | 0.8099 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.3043 | 21.2579 | 0.1759 | 0.1553 | 0.8221 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7210 | 20.6759 | 0.1710 | 0.1454 | 0.8334 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2717 | 21.2269 | 0.1698 | 0.1362 | 0.8445 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.3116 | 21.1705 | 0.1558 | 0.1276 | 0.8552 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6917 | 21.6530 | 0.1467 | 0.1196 | 0.8651 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9973 | 20.9606 | 0.1391 | 0.1120 | 0.8744 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7727 | 20.7360 | 0.1315 | 0.1049 | 0.8833 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4348 | 21.4009 | 0.1285 | 0.0983 | 0.8918 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1229 | 21.0902 | 0.1240 | 0.0920 | 0.9000 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9619 | 20.9586 | 0.0125 | 0.0862 | 0.9045 | 0.9138 | |

TABLA V-4

| Número | tiempo | leta | W total | RelAISRC W Seco | Ee | Ee Teor | Fe | Fe Teor |
|---------|--------|--------|---------|--------------------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.6708 | 21.6708 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 22.0837 | 21.8351 | 0.9425 | 0.9892 | 0.0051 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2571 | 21.0052 | 0.9550 | 0.9785 | 0.0155 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8749 | 21.8230 | 0.9550 | 0.9679 | 0.0259 | 0.0321 |
| 4 | 40 | 0.0436 | 20.9606 | 20.7218 | 0.9053 | 0.9574 | 0.0360 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5304 | 21.7925 | 0.9019 | 0.9470 | 0.0458 | 0.0530 |
| 6 | 60 | 0.0654 | 21.1732 | 20.9353 | 0.9019 | 0.9367 | 0.0557 | 0.0633 |
| 7 | 70 | 0.0762 | 21.2345 | 21.0274 | 0.7851 | 0.9266 | 0.0649 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5106 | 21.3105 | 0.7586 | 0.9165 | 0.0733 | 0.0835 |
| 9 | 90 | 0.0980 | 21.0914 | 20.8839 | 0.7866 | 0.9066 | 0.0817 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3278 | 21.1145 | 0.8086 | 0.8968 | 0.0904 | 0.1032 |
| 11 | 110 | 0.1190 | 21.0657 | 20.8437 | 0.8416 | 0.8871 | 0.0994 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1152 | 20.8985 | 0.8215 | 0.8775 | 0.1084 | 0.1225 |
| 13 | 130 | 0.1416 | 21.2428 | 21.0316 | 0.8007 | 0.8680 | 0.1172 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2555 | 21.0473 | 0.7893 | 0.8586 | 0.1259 | 0.1414 |
| 15 | 150 | 0.1634 | 21.0960 | 20.8956 | 0.7597 | 0.8493 | 0.1343 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1023 | 20.9023 | 0.7582 | 0.8401 | 0.1426 | 0.1599 |
| 17 | 170 | 0.1852 | 21.1898 | 20.9715 | 0.7927 | 0.8310 | 0.1511 | 0.1690 |
| 18 | 180 | 0.1961 | 21.6708 | 21.4680 | 0.7688 | 0.8220 | 0.1596 | 0.1780 |
| 19 | 190 | 0.2070 | 20.9790 | 20.7805 | 0.7525 | 0.8131 | 0.1678 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4284 | 21.2343 | 0.7358 | 0.8042 | 0.1759 | 0.1958 |
| 21 | 210 | 0.2287 | 21.1020 | 20.9085 | 0.7336 | 0.7955 | 0.1840 | 0.2045 |
| 22 | 220 | 0.2396 | 21.0618 | 20.8615 | 0.7592 | 0.7869 | 0.1921 | 0.2131 |
| 23 | 230 | 0.2505 | 21.4405 | 21.2537 | 0.7082 | 0.7784 | 0.2001 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3289 | 21.1403 | 0.7150 | 0.7700 | 0.2078 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2076 | 21.0368 | 0.7006 | 0.7616 | 0.2155 | 0.2384 |
| 26 | 260 | 0.2832 | 21.3035 | 21.1112 | 0.7290 | 0.7534 | 0.2233 | 0.2466 |
| 27 | 270 | 0.2941 | 21.6770 | 21.4903 | 0.7078 | 0.7452 | 0.2311 | 0.2548 |
| 28 | 280 | 0.3050 | 21.5673 | 21.3607 | 0.7074 | 0.7371 | 0.2389 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1440 | 20.9590 | 0.7013 | 0.7291 | 0.2465 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0452 | 20.8727 | 0.6540 | 0.7212 | 0.2539 | 0.2788 |
| 31 | 330 | 0.3594 | 21.3919 | 21.2205 | 0.6498 | 0.6981 | 0.2752 | 0.3019 |
| 32 | 360 | 0.3921 | 21.4571 | 21.2876 | 0.6426 | 0.6756 | 0.2963 | 0.3244 |
| 33 | 390 | 0.4248 | 21.3752 | 21.2076 | 0.6354 | 0.6539 | 0.3172 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7553 | 21.5916 | 0.6206 | 0.6329 | 0.3377 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4509 | 21.2879 | 0.6179 | 0.6125 | 0.3580 | 0.3875 |
| 36 | 480 | 0.5228 | 21.2080 | 21.0565 | 0.5743 | 0.5928 | 0.3774 | 0.4072 |

TABLA V-4

| Número | tiempo | continuación.. | | Re1A1S2R2 | | Ee | Ee Teor | Fe | Fe Teor |
|--------|--------|----------------|---------|-----------|--------|--------|---------|--------|---------|
| | | teta | W Total | W Seco | | | | | |
| 37 | 510 | 0.5553 | 21.0406 | 20.8947 | 0.5531 | 0.5738 | 0.3959 | 0.4262 | |
| 38 | 540 | 0.5602 | 21.1656 | 21.0205 | 0.5501 | 0.5553 | 0.4139 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.2982 | 21.0682 | 0.5307 | 0.5375 | 0.4315 | 0.4625 | |
| 40 | 600 | 0.6535 | 20.7396 | 20.6025 | 0.5198 | 0.5202 | 0.4487 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.3761 | 21.2470 | 0.4894 | 0.5035 | 0.4652 | 0.4965 | |
| 42 | 660 | 0.7109 | 21.2922 | 21.1671 | 0.4743 | 0.4873 | 0.4809 | 0.5127 | |
| 43 | 690 | 0.7516 | 20.9860 | 20.8635 | 0.4644 | 0.4716 | 0.4963 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.1733 | 21.0543 | 0.4511 | 0.4565 | 0.5112 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.0281 | 20.9145 | 0.4307 | 0.4418 | 0.5256 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1256 | 21.0191 | 0.4027 | 0.4138 | 0.5529 | 0.5862 | |
| 47 | 870 | 0.9476 | 21.2043 | 21.1049 | 0.3768 | 0.3877 | 0.5784 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.1018 | 21.0103 | 0.3469 | 0.3631 | 0.6021 | 0.6369 | |
| 49 | 990 | 1.0783 | 21.2904 | 21.2059 | 0.3203 | 0.3402 | 0.6239 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.1433 | 21.0590 | 0.3166 | 0.3186 | 0.6447 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.2549 | 21.1725 | 0.3124 | 0.2985 | 0.6652 | 0.7015 | |
| 52 | 1170 | 1.2744 | 20.7378 | 20.6603 | 0.2938 | 0.2796 | 0.6850 | 0.7204 | |
| 53 | 1230 | 1.3398 | 21.0515 | 20.9756 | 0.2877 | 0.2619 | 0.7040 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9301 | 20.8636 | 0.2521 | 0.2453 | 0.7217 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.2948 | 21.2235 | 0.2703 | 0.2298 | 0.7388 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.2686 | 21.1977 | 0.2688 | 0.2153 | 0.7564 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.1761 | 21.1120 | 0.2430 | 0.2017 | 0.7731 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.9212 | 21.8620 | 0.2244 | 0.1889 | 0.7884 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8628 | 20.8058 | 0.2168 | 0.1769 | 0.8028 | 0.8231 | |
| 60 | 1650 | 1.7972 | 21.7802 | 21.7307 | 0.1877 | 0.1658 | 0.8160 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.4485 | 21.4005 | 0.1820 | 0.1553 | 0.8281 | 0.8447 | |
| 62 | 1770 | 1.9280 | 21.5421 | 21.4962 | 0.1740 | 0.1454 | 0.8397 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.3534 | 21.3107 | 0.1619 | 0.1362 | 0.8507 | 0.8638 | |
| 64 | 1890 | 2.0587 | 20.8994 | 20.7624 | 0.1592 | 0.1276 | 0.8612 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.4210 | 21.3791 | 0.1568 | 0.1196 | 0.8716 | 0.8804 | |
| 66 | 2010 | 2.1894 | 21.9912 | 21.9324 | 0.1471 | 0.1120 | 0.8816 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.9268 | 20.8939 | 0.1247 | 0.1049 | 0.8905 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.7023 | 21.7511 | 0.1183 | 0.0983 | 0.8984 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.3554 | 21.3276 | 0.1054 | 0.0920 | 0.9057 | 0.9080 | |
| 70 | 2250 | 2.4508 | 21.4588 | 21.4402 | 0.0705 | 0.0862 | 0.9115 | 0.9138 | |

TABLA V-5
Número

RelAQ261R1

| | tiempo | teta | W Total | W Seco | Ee | Ee Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 20.3558 | 20.3558 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.2660 | 21.0160 | 0.9478 | 0.9892 | 0.0052 | 0.0108 |
| 2 | 20 | 0.0218 | 21.4203 | 21.1733 | 0.9364 | 0.9785 | 0.0154 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8622 | 21.6220 | 0.9864 | 0.9679 | 0.0259 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6272 | 21.3641 | 0.9974 | 0.9574 | 0.0367 | 0.0426 |
| 5 | 50 | 0.0545 | 22.2243 | 21.9825 | 0.9205 | 0.9470 | 0.0471 | 0.0530 |
| 6 | 60 | 0.0654 | 21.4111 | 21.1575 | 0.9614 | 0.9367 | 0.0574 | 0.0633 |
| 7 | 70 | 0.0762 | 22.0925 | 21.8450 | 0.9383 | 0.9266 | 0.0677 | 0.0734 |
| 8 | 80 | 0.0871 | 20.7802 | 20.5534 | 0.8598 | 0.9165 | 0.0775 | 0.0835 |
| 9 | 90 | 0.0980 | 22.0726 | 21.8285 | 0.9254 | 0.9066 | 0.0873 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3936 | 21.1730 | 0.8363 | 0.8968 | 0.0969 | 0.1032 |
| 11 | 110 | 0.1198 | 21.5800 | 21.3403 | 0.9087 | 0.8871 | 0.1064 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6287 | 21.4048 | 0.8488 | 0.8775 | 0.1159 | 0.1225 |
| 13 | 130 | 0.1416 | 21.0115 | 20.8010 | 0.7980 | 0.8680 | 0.1249 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2357 | 21.0020 | 0.8860 | 0.8586 | 0.1341 | 0.1414 |
| 15 | 150 | 0.1634 | 20.5900 | 20.3538 | 0.8879 | 0.8493 | 0.1437 | 0.1507 |
| 16 | 160 | 0.1743 | 21.2159 | 20.9972 | 0.8291 | 0.8401 | 0.1531 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4124 | 21.2030 | 0.7938 | 0.8310 | 0.1619 | 0.1690 |
| 18 | 180 | 0.1961 | 21.1100 | 20.9006 | 0.7938 | 0.8220 | 0.1706 | 0.1780 |
| 19 | 190 | 0.2070 | 21.2031 | 20.9942 | 0.7920 | 0.8131 | 0.1792 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0385 | 20.8270 | 0.8018 | 0.8042 | 0.1879 | 0.1958 |
| 21 | 210 | 0.2287 | 21.6122 | 21.3978 | 0.8126 | 0.7955 | 0.1967 | 0.2045 |
| 22 | 220 | 0.2396 | 21.2661 | 21.0555 | 0.7984 | 0.7869 | 0.2054 | 0.2131 |
| 23 | 230 | 0.2505 | 21.2141 | 21.0053 | 0.7916 | 0.7784 | 0.2141 | 0.2216 |
| 24 | 240 | 0.2614 | 21.4060 | 21.2029 | 0.7700 | 0.7700 | 0.2226 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2372 | 21.0408 | 0.7446 | 0.7616 | 0.2309 | 0.2384 |
| 26 | 260 | 0.2832 | 22.1101 | 21.9149 | 0.7400 | 0.7534 | 0.2389 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7880 | 21.5932 | 0.7309 | 0.7452 | 0.2470 | 0.2548 |
| 28 | 280 | 0.3050 | 21.4862 | 21.2858 | 0.7605 | 0.7371 | 0.2551 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5328 | 21.3406 | 0.6907 | 0.7291 | 0.2630 | 0.2709 |
| 30 | 300 | 0.3268 | 21.8178 | 21.4234 | 0.7370 | 0.7212 | 0.2708 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4450 | 21.2621 | 0.6934 | 0.6981 | 0.2941 | 0.3019 |
| 32 | 360 | 0.3921 | 21.0818 | 20.9055 | 0.6884 | 0.6756 | 0.3164 | 0.3244 |
| 33 | 390 | 0.4248 | 20.8209 | 20.6459 | 0.6634 | 0.6539 | 0.3381 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4662 | 21.2910 | 0.6842 | 0.6329 | 0.3598 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1533 | 21.0000 | 0.6761 | 0.6125 | 0.3801 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3363 | 21.1733 | 0.6179 | 0.5928 | 0.3997 | 0.4072 |

TABLA V-5

| Número | tiempo | continuación.. | | RelACSIRI | | Ea | Ea Teor | Fa | Fa Teor |
|--------|--------|----------------|---------|-----------|--------|--------|---------|--------|---------|
| | | teta | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.3753 | 21.2265 | 0.5641 | 0.5738 | 0.4190 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.3544 | 21.2122 | 0.5391 | 0.5553 | 0.4370 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3756 | 21.2352 | 0.5323 | 0.5375 | 0.4545 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4612 | 21.3259 | 0.5205 | 0.5202 | 0.4717 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.6930 | 21.5677 | 0.4750 | 0.5035 | 0.4880 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.6837 | 20.9535 | 0.4921 | 0.4873 | 0.5038 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1944 | 21.0720 | 0.4640 | 0.4716 | 0.5194 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.8642 | 21.7414 | 0.4655 | 0.4565 | 0.5346 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2575 | 21.1387 | 0.4504 | 0.4418 | 0.5496 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.2091 | 21.0880 | 0.4250 | 0.4138 | 0.5782 | 0.5862 | |
| 47 | 870 | 0.9475 | 20.6685 | 20.5723 | 0.3647 | 0.3877 | 0.6040 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5119 | 21.4273 | 0.3207 | 0.3631 | 0.6264 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7518 | 20.6665 | 0.3234 | 0.3402 | 0.6474 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3920 | 21.3022 | 0.3404 | 0.3186 | 0.6691 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4537 | 21.3826 | 0.2695 | 0.2985 | 0.6890 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.0956 | 21.0200 | 0.2904 | 0.2796 | 0.7073 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7667 | 20.6912 | 0.2862 | 0.2619 | 0.7262 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9143 | 20.8560 | 0.2210 | 0.2453 | 0.7427 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1722 | 21.1110 | 0.2320 | 0.2298 | 0.7575 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1626 | 21.1062 | 0.2138 | 0.2153 | 0.7721 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2170 | 21.1645 | 0.1970 | 0.2017 | 0.7856 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0100 | 20.9858 | 0.1979 | 0.1889 | 0.7986 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8166 | 20.7804 | 0.1372 | 0.1769 | 0.8095 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9474 | 20.9112 | 0.1372 | 0.1658 | 0.8185 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.3090 | 21.2579 | 0.1576 | 0.1553 | 0.8282 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7127 | 20.6759 | 0.1395 | 0.1454 | 0.8380 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2624 | 21.2269 | 0.1346 | 0.1362 | 0.8469 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.2018 | 21.1705 | 0.1187 | 0.1276 | 0.8552 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6808 | 21.6530 | 0.1054 | 0.1194 | 0.8625 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9859 | 20.9606 | 0.0959 | 0.1120 | 0.8691 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7611 | 20.7380 | 0.0876 | 0.1049 | 0.8751 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4233 | 21.4009 | 0.0849 | 0.0983 | 0.8807 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1111 | 21.0902 | 0.0792 | 0.0920 | 0.8861 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9536 | 20.9410 | 0.0478 | 0.0862 | 0.8902 | 0.9138 | |

TABLA V-6
Número

| | Tiempo | Letra | W Total | ReIACSIR2 W Seco | Ee | Ee Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------------------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.5711 | 21.5711 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 22.1903 | 21.8351 | 1.0054 | 0.9892 | 0.0055 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2671 | 21.0052 | 0.9929 | 0.9785 | 0.0164 | 0.0215 |
| 3 | 30 | 0.0327 | 21.0834 | 21.6230 | 0.9872 | 0.9679 | 0.0271 | 0.0321 |
| 4 | 40 | 0.0436 | 20.9656 | 20.7218 | 0.9243 | 0.9574 | 0.0376 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5349 | 21.2925 | 0.9189 | 0.9470 | 0.0476 | 0.0530 |
| 6 | 60 | 0.0654 | 21.1658 | 20.9353 | 0.8738 | 0.9367 | 0.0574 | 0.0633 |
| 7 | 70 | 0.0762 | 21.2562 | 21.0274 | 0.8674 | 0.9266 | 0.0668 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5916 | 21.3105 | 0.8761 | 0.9165 | 0.0763 | 0.0835 |
| 9 | 90 | 0.0980 | 21.1150 | 20.8839 | 0.8761 | 0.9066 | 0.0859 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3400 | 21.1145 | 0.8549 | 0.8968 | 0.0953 | 0.1032 |
| 11 | 110 | 0.1198 | 21.0507 | 20.8437 | 0.7847 | 0.8871 | 0.1042 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1050 | 20.8985 | 0.7829 | 0.8775 | 0.1128 | 0.1225 |
| 13 | 130 | 0.1416 | 21.2344 | 21.0316 | 0.7668 | 0.8680 | 0.1212 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2630 | 21.0473 | 0.8177 | 0.8586 | 0.1299 | 0.1414 |
| 15 | 150 | 0.1634 | 21.1151 | 20.8956 | 0.8321 | 0.8493 | 0.1388 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1073 | 20.9023 | 0.7772 | 0.8401 | 0.1476 | 0.1599 |
| 17 | 170 | 0.1852 | 21.1712 | 20.9715 | 0.7571 | 0.8310 | 0.1560 | 0.1690 |
| 18 | 180 | 0.1961 | 21.6711 | 21.4680 | 0.7700 | 0.8220 | 0.1643 | 0.1780 |
| 19 | 190 | 0.2070 | 20.9805 | 20.7805 | 0.7582 | 0.8131 | 0.1726 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4402 | 21.2343 | 0.7606 | 0.8042 | 0.1810 | 0.1958 |
| 21 | 210 | 0.2287 | 21.1127 | 20.9085 | 0.7741 | 0.7955 | 0.1895 | 0.2045 |
| 22 | 220 | 0.2396 | 21.0613 | 20.8615 | 0.7575 | 0.7869 | 0.1978 | 0.2131 |
| 23 | 230 | 0.2505 | 21.4504 | 21.2537 | 0.7457 | 0.7784 | 0.2060 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3404 | 21.1403 | 0.7586 | 0.7700 | 0.2142 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2401 | 21.0388 | 0.7631 | 0.7616 | 0.2225 | 0.2384 |
| 26 | 260 | 0.2832 | 21.3012 | 21.1112 | 0.7203 | 0.7534 | 0.2305 | 0.2466 |
| 27 | 270 | 0.2941 | 21.6829 | 21.4903 | 0.7302 | 0.7452 | 0.2384 | 0.2548 |
| 28 | 280 | 0.3050 | 21.5705 | 21.3807 | 0.7207 | 0.7371 | 0.2463 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1415 | 20.9590 | 0.6957 | 0.7291 | 0.2541 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0533 | 20.8727 | 0.6847 | 0.7212 | 0.2616 | 0.2788 |
| 31 | 330 | 0.3594 | 21.3990 | 21.2205 | 0.6767 | 0.6981 | 0.2838 | 0.3019 |
| 32 | 360 | 0.3921 | 21.4532 | 21.2876 | 0.6278 | 0.6756 | 0.3051 | 0.3244 |
| 33 | 390 | 0.4248 | 21.3738 | 21.2076 | 0.6301 | 0.6539 | 0.3257 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7549 | 21.5916 | 0.6191 | 0.6329 | 0.3461 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4414 | 21.2879 | 0.5819 | 0.6125 | 0.3657 | 0.3875 |
| 36 | 480 | 0.5228 | 21.2025 | 21.0565 | 0.5535 | 0.5928 | 0.3843 | 0.4072 |

TABLA V-6

continuación..

RelA2S1R2

| Número | tiempo | leta | W Total | W Seco | Ea | Ea Teor | Fe | Fe Teor |
|--------|--------|--------|---------|---------|--------|---------|--------|---------|
| 37 | 510 | 0.5855 | 21.0336 | 20.8947 | 0.5266 | 0.5738 | 0.4019 | 0.4262 |
| 38 | 540 | 0.5882 | 21.1643 | 21.0205 | 0.5452 | 0.5553 | 0.4194 | 0.4447 |
| 39 | 570 | 0.6209 | 21.2036 | 21.0469 | 0.5133 | 0.5375 | 0.4367 | 0.4625 |
| 40 | 600 | 0.6535 | 20.7357 | 20.6025 | 0.5050 | 0.5202 | 0.4534 | 0.4798 |
| 41 | 630 | 0.6662 | 21.3782 | 21.2470 | 0.4974 | 0.5035 | 0.4697 | 0.4965 |
| 42 | 660 | 0.7189 | 21.2951 | 21.1671 | 0.4853 | 0.4873 | 0.4858 | 0.5127 |
| 43 | 690 | 0.7516 | 20.9839 | 20.8635 | 0.4564 | 0.4716 | 0.5012 | 0.5284 |
| 44 | 720 | 0.7843 | 21.1768 | 21.0543 | 0.4644 | 0.4565 | 0.5162 | 0.5435 |
| 45 | 750 | 0.8169 | 21.0286 | 20.9145 | 0.4326 | 0.4418 | 0.5309 | 0.5582 |
| 46 | 810 | 0.8823 | 21.1268 | 21.0191 | 0.4083 | 0.4138 | 0.5583 | 0.5862 |
| 47 | 870 | 0.9475 | 21.2151 | 21.1049 | 0.4216 | 0.3877 | 0.5855 | 0.6123 |
| 48 | 930 | 1.0130 | 21.1060 | 21.0103 | 0.3704 | 0.3631 | 0.6113 | 0.6369 |
| 49 | 990 | 1.0783 | 21.3007 | 21.2057 | 0.3594 | 0.3402 | 0.6352 | 0.6598 |
| 50 | 1050 | 1.1437 | 21.1452 | 21.0598 | 0.3238 | 0.3186 | 0.6575 | 0.6814 |
| 51 | 1110 | 1.2091 | 21.2539 | 21.1725 | 0.3086 | 0.2985 | 0.6782 | 0.7015 |
| 52 | 1170 | 1.2744 | 20.7380 | 20.6603 | 0.2946 | 0.2796 | 0.6979 | 0.7204 |
| 53 | 1230 | 1.3398 | 21.0473 | 20.9758 | 0.2718 | 0.2619 | 0.7164 | 0.7381 |
| 54 | 1290 | 1.4051 | 20.9295 | 20.8636 | 0.2498 | 0.2453 | 0.7334 | 0.7547 |
| 55 | 1350 | 1.4705 | 21.2823 | 21.2235 | 0.2229 | 0.2298 | 0.7489 | 0.7702 |
| 56 | 1410 | 1.5358 | 21.2512 | 21.1977 | 0.2028 | 0.2153 | 0.7628 | 0.7847 |
| 57 | 1470 | 1.6012 | 21.1523 | 21.1120 | 0.1907 | 0.2017 | 0.7757 | 0.7983 |
| 58 | 1530 | 1.6665 | 21.9094 | 21.8620 | 0.1797 | 0.1889 | 0.7878 | 0.8111 |
| 59 | 1590 | 1.7319 | 20.8482 | 20.8056 | 0.1615 | 0.1769 | 0.7989 | 0.8231 |
| 60 | 1650 | 1.7972 | 21.7704 | 21.7307 | 0.1505 | 0.1658 | 0.8091 | 0.8342 |
| 61 | 1710 | 1.8626 | 21.4388 | 21.4005 | 0.1452 | 0.1553 | 0.8188 | 0.8447 |
| 62 | 1770 | 1.9280 | 21.5305 | 21.4962 | 0.1300 | 0.1454 | 0.8278 | 0.8546 |
| 63 | 1830 | 1.9933 | 21.3420 | 21.3167 | 0.1187 | 0.1362 | 0.8359 | 0.8638 |
| 64 | 1890 | 2.0587 | 20.7922 | 20.7624 | 0.1130 | 0.1276 | 0.8435 | 0.8724 |
| 65 | 1950 | 2.1240 | 21.4110 | 21.3791 | 0.1209 | 0.1196 | 0.8511 | 0.8804 |
| 66 | 2010 | 2.1894 | 21.9833 | 21.9524 | 0.1171 | 0.1120 | 0.8589 | 0.8880 |
| 67 | 2070 | 2.2547 | 20.9267 | 20.8939 | 0.1016 | 0.1049 | 0.8660 | 0.8951 |
| 68 | 2130 | 2.3201 | 21.7809 | 21.7511 | 0.1130 | 0.0983 | 0.8730 | 0.9017 |
| 69 | 2190 | 2.3854 | 21.3525 | 21.3276 | 0.0944 | 0.0920 | 0.8798 | 0.9080 |
| 70 | 2250 | 2.4508 | 21.4557 | 21.4335 | 0.0842 | 0.0862 | 0.8857 | 0.9138 |

TABLA V-7
Número

ReiA2S2k1

| | tiempo | Leta | W Total | W Seco | Ee | Ee Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.0854 | 21.0854 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.2453 | 21.0160 | 0.0693 | 0.9892 | 0.0047 | 0.0108 |
| 2 | 20 | 0.0218 | 21.4156 | 21.1733 | 0.9186 | 0.9785 | 0.0145 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8611 | 21.6220 | 0.9064 | 0.9679 | 0.0244 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6028 | 21.3641 | 0.9049 | 0.9574 | 0.0343 | 0.0426 |
| 5 | 50 | 0.0545 | 22.1956 | 21.9825 | 0.8079 | 0.9470 | 0.0436 | 0.0530 |
| 6 | 60 | 0.0654 | 21.3849 | 21.1573 | 0.8621 | 0.9367 | 0.0527 | 0.0633 |
| 7 | 70 | 0.0762 | 22.0653 | 21.8450 | 0.8352 | 0.9266 | 0.0619 | 0.0734 |
| 8 | 80 | 0.0871 | 20.7883 | 20.5534 | 0.8905 | 0.9165 | 0.0713 | 0.0835 |
| 9 | 90 | 0.0980 | 22.0472 | 21.8285 | 0.8291 | 0.9066 | 0.0807 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3866 | 21.1730 | 0.8098 | 0.8968 | 0.0896 | 0.1032 |
| 11 | 110 | 0.1198 | 21.5612 | 21.3403 | 0.8374 | 0.8871 | 0.0986 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6067 | 21.4048 | 0.7654 | 0.8775 | 0.1073 | 0.1225 |
| 13 | 130 | 0.1416 | 20.9866 | 20.8010 | 0.7036 | 0.8680 | 0.1153 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2063 | 21.0020 | 0.7745 | 0.8586 | 0.1234 | 0.1414 |
| 15 | 150 | 0.1634 | 20.5476 | 20.3558 | 0.7271 | 0.8493 | 0.1316 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1973 | 20.9972 | 0.7593 | 0.8401 | 0.1397 | 0.1599 |
| 17 | 170 | 0.1852 | 21.3915 | 21.2030 | 0.7146 | 0.8310 | 0.1477 | 0.1690 |
| 18 | 180 | 0.1961 | 21.0854 | 20.9006 | 0.7006 | 0.8220 | 0.1554 | 0.1780 |
| 19 | 190 | 0.2070 | 21.1910 | 20.9942 | 0.7461 | 0.8131 | 0.1633 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0198 | 20.8270 | 0.7309 | 0.8042 | 0.1713 | 0.1958 |
| 21 | 210 | 0.2287 | 21.5762 | 21.3978 | 0.6763 | 0.7955 | 0.1790 | 0.2045 |
| 22 | 220 | 0.2396 | 21.2470 | 21.0555 | 0.7260 | 0.7869 | 0.1866 | 0.2131 |
| 23 | 230 | 0.2505 | 21.1820 | 21.0053 | 0.7078 | 0.7784 | 0.1944 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3910 | 21.2029 | 0.7131 | 0.7700 | 0.2022 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2255 | 21.0400 | 0.7002 | 0.7616 | 0.2099 | 0.2384 |
| 26 | 260 | 0.2832 | 22.1012 | 21.9149 | 0.7063 | 0.7534 | 0.2175 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7701 | 21.5932 | 0.6706 | 0.7452 | 0.2250 | 0.2548 |
| 28 | 280 | 0.3050 | 21.4568 | 21.2856 | 0.6566 | 0.7371 | 0.2322 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5184 | 21.3404 | 0.6740 | 0.7291 | 0.2395 | 0.2709 |
| 30 | 300 | 0.3268 | 21.6148 | 21.4264 | 0.7256 | 0.7212 | 0.2471 | 0.2788 |
| 31 | 310 | 0.3379 | 21.4315 | 21.2621 | 0.6422 | 0.6981 | 0.2695 | 0.3017 |
| 32 | 320 | 0.3491 | 21.0752 | 20.9055 | 0.6433 | 0.6756 | 0.2905 | 0.3244 |
| 33 | 330 | 0.3608 | 20.7957 | 20.6459 | 0.5679 | 0.6539 | 0.3103 | 0.3461 |
| 34 | 340 | 0.4575 | 21.4537 | 21.2910 | 0.6168 | 0.6329 | 0.3296 | 0.3671 |
| 35 | 350 | 0.4902 | 21.1723 | 21.0000 | 0.6502 | 0.6125 | 0.3503 | 0.3875 |
| 36 | 360 | 0.5228 | 21.3133 | 21.1733 | 0.5307 | 0.5928 | 0.3696 | 0.4072 |

TABLA V-7

| Número | Tiempo | continuación.. | | ReIA2S2R1 | | | | | |
|--------|--------|----------------|---------|-----------|--------|---------|--------|---------|--|
| | | leta | W Total | W Seco | Ee | Ee Teor | Fe | Fe Teor | |
| 37 | 510 | 0.5555 | 21.5700 | 21.2265 | 0.5440 | 0.5738 | 0.3872 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.3543 | 21.2122 | 0.5387 | 0.5553 | 0.4049 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3668 | 21.2352 | 0.4989 | 0.5375 | 0.4218 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4583 | 21.3239 | 0.5095 | 0.5202 | 0.4363 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.7033 | 21.5677 | 0.5141 | 0.5035 | 0.4550 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.0833 | 20.9555 | 0.4921 | 0.4873 | 0.4715 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1943 | 21.0720 | 0.4636 | 0.4716 | 0.4871 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.8528 | 21.7414 | 0.4223 | 0.4565 | 0.5015 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2542 | 21.1587 | 0.4379 | 0.4418 | 0.5154 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1964 | 21.0880 | 0.4110 | 0.4138 | 0.5433 | 0.5862 | |
| 47 | 870 | 0.9478 | 20.6706 | 20.5723 | 0.3727 | 0.3877 | 0.5689 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5235 | 21.4273 | 0.3647 | 0.3631 | 0.5930 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7813 | 20.6665 | 0.3594 | 0.3402 | 0.6167 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.5851 | 21.3022 | 0.3143 | 0.3186 | 0.6387 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4633 | 21.3826 | 0.3059 | 0.2985 | 0.6590 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.1000 | 21.0200 | 0.3063 | 0.2796 | 0.6790 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7609 | 20.6912 | 0.2642 | 0.2619 | 0.6976 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9225 | 20.8560 | 0.2521 | 0.2453 | 0.7145 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1753 | 21.1110 | 0.2438 | 0.2298 | 0.7307 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1657 | 21.1062 | 0.2256 | 0.2153 | 0.7460 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2285 | 21.1645 | 0.2313 | 0.2017 | 0.7610 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0232 | 20.9658 | 0.2176 | 0.1889 | 0.7754 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8300 | 20.7804 | 0.1880 | 0.1789 | 0.7889 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9835 | 20.9112 | 0.1983 | 0.1658 | 0.8015 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.3066 | 21.2579 | 0.1846 | 0.1553 | 0.8140 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7212 | 20.6759 | 0.1717 | 0.1454 | 0.8257 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2667 | 21.2269 | 0.1509 | 0.1362 | 0.8362 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.2089 | 21.1705 | 0.1456 | 0.1276 | 0.8459 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6905 | 21.6530 | 0.1422 | 0.1196 | 0.8553 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9935 | 20.9608 | 0.1247 | 0.1120 | 0.8640 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7729 | 20.7380 | 0.1323 | 0.1049 | 0.8724 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4324 | 21.4009 | 0.1213 | 0.0983 | 0.8807 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1217 | 21.0902 | 0.1194 | 0.0920 | 0.8886 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9609 | 20.9402 | 0.0785 | 0.0862 | 0.8950 | 0.9138 | |

TABLA V-B
Número

ReIATS2R2

| | tiempo | teta | W Total | W Secu | Ea | Ea Teor | Fe | Fe teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.6623 | 21.6623 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 22.0550 | 21.8351 | 0.8337 | 0.9892 | 0.0045 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2136 | 21.0052 | 0.7901 | 0.9785 | 0.0134 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8569 | 21.6230 | 0.8867 | 0.9679 | 0.0225 | 0.0321 |
| 4 | 40 | 0.0436 | 20.9348 | 20.7218 | 0.8075 | 0.9574 | 0.0317 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5110 | 21.2925 | 0.8283 | 0.9470 | 0.0407 | 0.0530 |
| 6 | 60 | 0.0654 | 21.1602 | 20.9353 | 0.8528 | 0.9367 | 0.0498 | 0.0633 |
| 7 | 70 | 0.0762 | 21.2432 | 21.0274 | 0.8181 | 0.9266 | 0.0589 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5133 | 21.3105 | 0.7688 | 0.9165 | 0.0675 | 0.0835 |
| 9 | 90 | 0.0980 | 21.0728 | 20.8839 | 0.7919 | 0.9066 | 0.0760 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3322 | 21.1145 | 0.8253 | 0.8968 | 0.0849 | 0.1032 |
| 11 | 110 | 0.1198 | 21.0505 | 20.8437 | 0.7840 | 0.8871 | 0.0936 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1017 | 20.8985 | 0.7702 | 0.8775 | 0.1021 | 0.1225 |
| 13 | 130 | 0.1416 | 21.2238 | 21.0316 | 0.7286 | 0.8680 | 0.1102 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2512 | 21.0473 | 0.7730 | 0.8586 | 0.1184 | 0.1414 |
| 15 | 150 | 0.1634 | 21.0930 | 20.8956 | 0.7484 | 0.8493 | 0.1267 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1047 | 20.9023 | 0.7673 | 0.8401 | 0.1350 | 0.1599 |
| 17 | 170 | 0.1852 | 21.1785 | 20.9715 | 0.7772 | 0.8310 | 0.1434 | 0.1690 |
| 18 | 180 | 0.1961 | 21.6623 | 21.4680 | 0.7366 | 0.8220 | 0.1516 | 0.1780 |
| 19 | 190 | 0.2070 | 20.9728 | 20.7805 | 0.7290 | 0.8131 | 0.1596 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4266 | 21.2343 | 0.7290 | 0.8042 | 0.1675 | 0.1958 |
| 21 | 210 | 0.2287 | 21.0853 | 20.9085 | 0.6703 | 0.7955 | 0.1752 | 0.2045 |
| 22 | 220 | 0.2396 | 21.0517 | 20.8515 | 0.7211 | 0.7869 | 0.1827 | 0.2131 |
| 23 | 230 | 0.2505 | 21.4462 | 21.2537 | 0.7298 | 0.7784 | 0.1906 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3207 | 21.1403 | 0.6839 | 0.7700 | 0.1983 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2345 | 21.0368 | 0.7419 | 0.7616 | 0.2061 | 0.2384 |
| 26 | 260 | 0.2832 | 21.2940 | 21.1112 | 0.6930 | 0.7534 | 0.2139 | 0.2466 |
| 27 | 270 | 0.2941 | 21.6786 | 21.4903 | 0.7083 | 0.7452 | 0.2215 | 0.2548 |
| 28 | 280 | 0.3050 | 21.8561 | 21.3807 | 0.6725 | 0.7371 | 0.2291 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1232 | 20.9590 | 0.6225 | 0.7291 | 0.2361 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0473 | 20.8727 | 0.6430 | 0.7212 | 0.2430 | 0.2788 |
| 31 | 310 | 0.3377 | 21.3023 | 21.2205 | 0.6134 | 0.6981 | 0.2635 | 0.3019 |
| 32 | 320 | 0.3482 | 21.4504 | 21.2876 | 0.6172 | 0.6756 | 0.2836 | 0.3244 |
| 33 | 330 | 0.4240 | 21.3648 | 21.2076 | 0.5960 | 0.6539 | 0.3035 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7469 | 21.5916 | 0.5887 | 0.6329 | 0.3228 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4368 | 21.2879 | 0.5721 | 0.6125 | 0.3418 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3008 | 21.0565 | 0.5470 | 0.5928 | 0.3601 | 0.4072 |

TABLA V-8

| Número | tiempo | continuación.. | | RelA2S2R2 | | Ea | Ea Teor | Fa | Fa Teor |
|--------|--------|----------------|---------|-----------|--------|--------|---------|--------|---------|
| | | tota | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.0430 | 20.8947 | 0.5622 | 0.5738 | 0.3782 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.1620 | 21.0205 | 0.5395 | 0.5553 | 0.3962 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.2268 | 21.0682 | 0.6013 | 0.5375 | 0.4148 | 0.4625 | |
| 40 | 600 | 0.6535 | 20.7325 | 20.6025 | 0.4920 | 0.5202 | 0.4327 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.3730 | 21.2470 | 0.4777 | 0.5035 | 0.4486 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.2034 | 21.1671 | 0.4409 | 0.4873 | 0.4636 | 0.5127 | |
| 43 | 690 | 0.7515 | 20.9050 | 20.8635 | 0.4606 | 0.4716 | 0.4783 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.1772 | 21.0543 | 0.4659 | 0.4565 | 0.4934 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.0334 | 20.9145 | 0.4508 | 0.4418 | 0.5084 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1326 | 21.0191 | 0.4303 | 0.4138 | 0.5372 | 0.5862 | |
| 47 | 870 | 0.9476 | 21.2108 | 21.1049 | 0.4015 | 0.3877 | 0.5644 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.1113 | 21.0103 | 0.3829 | 0.3631 | 0.5900 | 0.6369 | |
| 49 | 990 | 1.0783 | 21.3026 | 21.2059 | 0.3666 | 0.3402 | 0.6145 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.1449 | 21.0598 | 0.3226 | 0.3186 | 0.6370 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.2535 | 21.1725 | 0.3071 | 0.2985 | 0.6576 | 0.7015 | |
| 52 | 1170 | 1.2744 | 20.7359 | 20.6503 | 0.2866 | 0.2796 | 0.6770 | 0.7204 | |
| 53 | 1230 | 1.3398 | 21.0471 | 20.9756 | 0.2711 | 0.2619 | 0.6952 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9301 | 20.8636 | 0.2521 | 0.2453 | 0.7123 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.2015 | 21.2235 | 0.2199 | 0.2298 | 0.7277 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.2596 | 21.1977 | 0.2347 | 0.2153 | 0.7426 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.1683 | 21.1120 | 0.2134 | 0.2017 | 0.7572 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.9152 | 21.8620 | 0.2017 | 0.1889 | 0.7708 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8338 | 20.8056 | 0.1903 | 0.1769 | 0.7836 | 0.8231 | |
| 60 | 1650 | 1.7972 | 21.7799 | 21.7307 | 0.1865 | 0.1658 | 0.7959 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.4443 | 21.4005 | 0.1660 | 0.1553 | 0.8074 | 0.8447 | |
| 62 | 1770 | 1.9280 | 21.5350 | 21.4962 | 0.1501 | 0.1454 | 0.8178 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.3550 | 21.3107 | 0.1679 | 0.1362 | 0.8282 | 0.8638 | |
| 64 | 1890 | 2.0587 | 20.7973 | 20.7624 | 0.1323 | 0.1276 | 0.8380 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.4094 | 21.3791 | 0.1149 | 0.1196 | 0.8461 | 0.8804 | |
| 66 | 2010 | 2.1894 | 21.9846 | 21.9524 | 0.1221 | 0.1120 | 0.8538 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.9255 | 20.8939 | 0.1198 | 0.1049 | 0.8617 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.7803 | 21.7511 | 0.1107 | 0.0983 | 0.8692 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.3581 | 21.3276 | 0.1156 | 0.0920 | 0.8766 | 0.9080 | |
| 70 | 2250 | 2.4508 | 21.4415 | 21.4294 | 0.0459 | 0.0862 | 0.8819 | 0.9138 | |

TABLA V-9
Número

Re2A1S1R1

| | Tiempo | teta | W Total | W Seco | Ea | Ea Teor | Fa | Fa Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.3068 | 21.0160 | 1.1024 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.3068 | 21.0160 | 1.1024 | 0.9892 | 0.0120 | 0.0108 |
| 2 | 20 | 0.0218 | 21.4486 | 21.1733 | 1.0437 | 0.9785 | 0.0237 | 0.0215 |
| 3 | 30 | 0.0327 | 21.0911 | 21.6220 | 1.0202 | 0.9679 | 0.0349 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6398 | 21.3641 | 1.0452 | 0.9574 | 0.0462 | 0.0426 |
| 5 | 50 | 0.0545 | 22.2549 | 21.9825 | 1.0327 | 0.9470 | 0.0575 | 0.0530 |
| 6 | 60 | 0.0654 | 21.4224 | 21.1575 | 1.0042 | 0.9367 | 0.0686 | 0.0633 |
| 7 | 70 | 0.0762 | 22.1063 | 21.8450 | 0.9982 | 0.9266 | 0.0795 | 0.0734 |
| 8 | 80 | 0.0871 | 20.0130 | 20.5534 | 0.9842 | 0.9165 | 0.0903 | 0.0835 |
| 9 | 90 | 0.0980 | 22.0753 | 21.8285 | 0.9356 | 0.9066 | 0.1008 | 0.0934 |
| 10 | 100 | 0.1089 | 21.4352 | 21.1730 | 0.9940 | 0.8968 | 0.1113 | 0.1032 |
| 11 | 110 | 0.1198 | 21.5974 | 21.3403 | 0.9747 | 0.8871 | 0.1220 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6608 | 21.4048 | 0.9705 | 0.8775 | 0.1326 | 0.1225 |
| 13 | 130 | 0.1416 | 21.0525 | 20.8010 | 0.9686 | 0.8680 | 0.1431 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2529 | 21.0020 | 0.9512 | 0.8586 | 0.1536 | 0.1414 |
| 15 | 150 | 0.1634 | 20.6022 | 20.3558 | 0.9341 | 0.8493 | 0.1639 | 0.1507 |
| 16 | 160 | 0.1743 | 21.2409 | 20.9972 | 0.9239 | 0.8401 | 0.1740 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4422 | 21.2030 | 0.9068 | 0.8310 | 0.1840 | 0.1690 |
| 18 | 180 | 0.1961 | 21.1416 | 20.9006 | 0.9136 | 0.8220 | 0.1939 | 0.1780 |
| 19 | 190 | 0.2070 | 21.2344 | 20.9942 | 0.9106 | 0.8131 | 0.2038 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0652 | 20.8270 | 0.9030 | 0.8042 | 0.2137 | 0.1958 |
| 21 | 210 | 0.2287 | 21.6283 | 21.3978 | 0.8738 | 0.7955 | 0.2234 | 0.2045 |
| 22 | 220 | 0.2396 | 21.2894 | 21.0555 | 0.8867 | 0.7867 | 0.2329 | 0.2131 |
| 23 | 230 | 0.2505 | 21.2373 | 21.0053 | 0.8795 | 0.7784 | 0.2426 | 0.2216 |
| 24 | 240 | 0.2614 | 21.4318 | 21.2029 | 0.8678 | 0.7700 | 0.2521 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2677 | 21.0408 | 0.8602 | 0.7616 | 0.2615 | 0.2384 |
| 26 | 260 | 0.2832 | 22.1240 | 21.9149 | 0.7927 | 0.7534 | 0.2705 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7981 | 21.5932 | 0.7768 | 0.7452 | 0.2790 | 0.2548 |
| 28 | 280 | 0.3050 | 21.4886 | 21.2856 | 0.7696 | 0.7371 | 0.2875 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5344 | 21.3406 | 0.7347 | 0.7291 | 0.2957 | 0.2709 |
| 30 | 300 | 0.3268 | 21.6098 | 21.4234 | 0.7067 | 0.7212 | 0.3035 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4454 | 21.2621 | 0.6949 | 0.6981 | 0.3264 | 0.3019 |
| 32 | 360 | 0.3921 | 21.0853 | 20.9055 | 0.6816 | 0.6756 | 0.3469 | 0.3244 |
| 33 | 390 | 0.4248 | 20.8226 | 20.6459 | 0.6699 | 0.6539 | 0.3710 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4637 | 21.2910 | 0.6547 | 0.6329 | 0.3926 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1599 | 21.0006 | 0.6032 | 0.6125 | 0.4132 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3275 | 21.1733 | 0.5846 | 0.5928 | 0.4326 | 0.4072 |

TABLA V-9

| Número | tiempo | continuación. | | Re2AlSi1R1 | | Ee | Ee Teor | Fe | Fe Teor |
|--------|--------|---------------|---------|------------|--------|--------|---------|--------|---------|
| | | leta | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.3754 | 21.2265 | 0.5645 | 0.5738 | 0.4513 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.3506 | 21.2122 | 0.5247 | 0.5553 | 0.4691 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3763 | 21.2352 | 0.5349 | 0.5375 | 0.4865 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4594 | 21.3239 | 0.5137 | 0.5202 | 0.5036 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.6950 | 21.5677 | 0.4826 | 0.5035 | 0.5199 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.0807 | 20.9535 | 0.4822 | 0.4873 | 0.5356 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1956 | 21.0720 | 0.4686 | 0.4716 | 0.5512 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.8556 | 21.7414 | 0.4329 | 0.4565 | 0.5659 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2537 | 21.1387 | 0.4360 | 0.4418 | 0.5801 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1943 | 21.0800 | 0.4030 | 0.4138 | 0.6075 | 0.5862 | |
| 47 | 870 | 0.9476 | 20.6715 | 20.5723 | 0.3761 | 0.3877 | 0.6330 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5118 | 21.4273 | 0.3203 | 0.3631 | 0.6557 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7468 | 20.6665 | 0.3044 | 0.3402 | 0.6761 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3798 | 21.3022 | 0.2942 | 0.3186 | 0.6957 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4591 | 21.3826 | 0.2900 | 0.2985 | 0.7148 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.0887 | 21.0200 | 0.2604 | 0.2796 | 0.7328 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7576 | 20.6912 | 0.2525 | 0.2619 | 0.7495 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9184 | 20.8560 | 0.2366 | 0.2453 | 0.7655 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1628 | 21.1110 | 0.1964 | 0.2298 | 0.7797 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1609 | 21.1082 | 0.2074 | 0.2153 | 0.7929 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2154 | 21.1645 | 0.1930 | 0.2017 | 0.8059 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0147 | 20.9658 | 0.1854 | 0.1889 | 0.8183 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8205 | 20.7804 | 0.1520 | 0.1769 | 0.8293 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9499 | 20.9112 | 0.1467 | 0.1658 | 0.8391 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.2954 | 21.2579 | 0.1422 | 0.1553 | 0.8485 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7119 | 20.6757 | 0.1365 | 0.1454 | 0.8576 | 0.8542 | |
| 63 | 1830 | 1.9933 | 21.2599 | 21.2269 | 0.1251 | 0.1362 | 0.8662 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.2009 | 21.1705 | 0.1152 | 0.1276 | 0.8740 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6818 | 21.6530 | 0.1084 | 0.1196 | 0.8813 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9840 | 20.9506 | 0.0887 | 0.1120 | 0.8878 | 0.8860 | |
| 67 | 2070 | 2.2547 | 20.7512 | 20.7380 | 0.0500 | 0.1049 | 0.8923 | 0.8931 | |
| 68 | 2130 | 2.3201 | 21.4224 | 21.4009 | 0.0815 | 0.0983 | 0.8966 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1099 | 21.0902 | 0.0747 | 0.0920 | 0.9017 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9495 | 20.9310 | 0.0701 | 0.0862 | 0.9065 | 0.9138 | |

TABLA V-10

ReSISTIR2

| Número | tiempo | teta | W Total | W Seco | Ea | Ea Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.7090 | 21.7090 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.1259 | 21.8351 | 1.1024 | 0.9892 | 0.0060 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2805 | 21.6052 | 1.0437 | 0.9785 | 0.0177 | 0.0215 |
| 3 | 30 | 0.0327 | 21.6921 | 21.6230 | 1.0202 | 0.9679 | 0.0289 | 0.0321 |
| 4 | 40 | 0.0436 | 20.9975 | 20.7218 | 1.0452 | 0.9574 | 0.0402 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5649 | 21.2925 | 1.0327 | 0.9470 | 0.0515 | 0.0530 |
| 6 | 60 | 0.0654 | 21.2002 | 20.9352 | 1.0042 | 0.9367 | 0.0626 | 0.0633 |
| 7 | 70 | 0.0762 | 21.2907 | 21.0274 | 0.9982 | 0.9266 | 0.0735 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5701 | 21.3105 | 0.9842 | 0.9165 | 0.0843 | 0.0835 |
| 9 | 90 | 0.0980 | 21.1307 | 20.8839 | 0.9556 | 0.9066 | 0.0947 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3767 | 21.1145 | 0.9940 | 0.8968 | 0.1053 | 0.1032 |
| 11 | 110 | 0.1198 | 21.1908 | 20.8437 | 0.9747 | 0.8871 | 0.1160 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1466 | 20.8985 | 0.9406 | 0.8775 | 0.1264 | 0.1225 |
| 13 | 130 | 0.1415 | 21.2824 | 21.0316 | 0.9506 | 0.8680 | 0.1367 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2986 | 21.0473 | 0.9527 | 0.8586 | 0.1471 | 0.1414 |
| 15 | 150 | 0.1634 | 21.1473 | 20.8956 | 0.9542 | 0.8493 | 0.1575 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1460 | 20.9023 | 0.9239 | 0.8401 | 0.1677 | 0.1599 |
| 17 | 170 | 0.1852 | 21.2107 | 20.9715 | 0.9068 | 0.8310 | 0.1777 | 0.1690 |
| 18 | 180 | 0.1961 | 21.7090 | 21.4680 | 0.9136 | 0.8220 | 0.1876 | 0.1780 |
| 19 | 190 | 0.2070 | 21.0207 | 20.7805 | 0.9106 | 0.8131 | 0.1975 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4725 | 21.2343 | 0.9030 | 0.8042 | 0.2074 | 0.1958 |
| 21 | 210 | 0.2287 | 21.1590 | 20.9085 | 0.8738 | 0.7955 | 0.2171 | 0.2045 |
| 22 | 220 | 0.2396 | 21.0954 | 20.8615 | 0.8867 | 0.7869 | 0.2267 | 0.2131 |
| 23 | 230 | 0.2505 | 21.8857 | 21.2537 | 0.8795 | 0.7784 | 0.2363 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3692 | 21.1403 | 0.8678 | 0.7700 | 0.2458 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2657 | 21.0388 | 0.8602 | 0.7616 | 0.2552 | 0.2384 |
| 26 | 260 | 0.2832 | 21.3305 | 21.1112 | 0.7927 | 0.7534 | 0.2642 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7052 | 21.4903 | 0.8147 | 0.7452 | 0.2730 | 0.2548 |
| 28 | 280 | 0.3050 | 21.5987 | 21.3807 | 0.8264 | 0.7371 | 0.2819 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1628 | 20.9590 | 0.7726 | 0.7291 | 0.2906 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0691 | 20.8727 | 0.7446 | 0.7212 | 0.2989 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4088 | 21.2205 | 0.7139 | 0.6981 | 0.3227 | 0.3019 |
| 32 | 360 | 0.3921 | 21.4723 | 21.2989 | 0.6574 | 0.6756 | 0.3451 | 0.3244 |
| 33 | 390 | 0.4248 | 21.3903 | 21.2201 | 0.6452 | 0.6539 | 0.3664 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7643 | 21.6016 | 0.6188 | 0.6329 | 0.3870 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4470 | 21.2879 | 0.6032 | 0.6125 | 0.4069 | 0.3875 |
| 36 | 480 | 0.5228 | 21.2107 | 21.0565 | 0.5846 | 0.5928 | 0.4263 | 0.4072 |

TABLA V-10

| Número | tiempo | continuación.. | | Kc1A1S1K2 | | Ee | Ee Teor | Fe | Fe Teor |
|--------|--------|----------------|---------|-----------|--------|--------|---------|--------|---------|
| | | teta | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.0576 | 20.9195 | 0.5235 | 0.5738 | 0.4444 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.1589 | 21.0205 | 0.5247 | 0.5553 | 0.4616 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.2008 | 21.0682 | 0.5027 | 0.5375 | 0.4784 | 0.4625 | |
| 40 | 600 | 0.6535 | 20.7345 | 20.6025 | 0.5004 | 0.5202 | 0.4947 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.3767 | 21.2470 | 0.4917 | 0.5035 | 0.5110 | 0.4985 | |
| 42 | 660 | 0.7189 | 21.2891 | 21.1671 | 0.4625 | 0.4873 | 0.5265 | 0.5127 | |
| 43 | 690 | 0.7516 | 20.9842 | 20.8635 | 0.4576 | 0.4716 | 0.5416 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.1713 | 21.0543 | 0.4436 | 0.4565 | 0.5563 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.0345 | 20.9251 | 0.4146 | 0.4418 | 0.5703 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1202 | 21.0191 | 0.4136 | 0.4138 | 0.5974 | 0.5862 | |
| 47 | 870 | 0.9476 | 21.2104 | 21.1142 | 0.3647 | 0.3877 | 0.6228 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.1120 | 21.0103 | 0.3855 | 0.3631 | 0.6473 | 0.6369 | |
| 49 | 990 | 1.0783 | 21.2919 | 21.2059 | 0.3260 | 0.3402 | 0.6706 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.1389 | 21.0598 | 0.2999 | 0.3186 | 0.6910 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.0460 | 21.1725 | 0.2786 | 0.2985 | 0.7099 | 0.7015 | |
| 52 | 1170 | 1.2744 | 20.7330 | 20.8603 | 0.2756 | 0.2796 | 0.7281 | 0.7204 | |
| 53 | 1230 | 1.3398 | 21.0481 | 20.9906 | 0.2180 | 0.2619 | 0.7442 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9321 | 20.8736 | 0.2218 | 0.2453 | 0.7586 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.0345 | 21.2235 | 0.2313 | 0.2298 | 0.7734 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.2532 | 21.1977 | 0.2104 | 0.2153 | 0.7878 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.1387 | 21.1120 | 0.2150 | 0.2017 | 0.8017 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.9153 | 21.8620 | 0.2021 | 0.1889 | 0.8153 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8958 | 20.8066 | 0.1903 | 0.1769 | 0.8281 | 0.8231 | |
| 60 | 1650 | 1.7972 | 21.7705 | 21.7307 | 0.1812 | 0.1658 | 0.8403 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.4434 | 21.4095 | 0.1826 | 0.1553 | 0.8515 | 0.8447 | |
| 62 | 1770 | 1.9280 | 21.5383 | 21.4562 | 0.1482 | 0.1454 | 0.8617 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.3480 | 21.3107 | 0.1414 | 0.1362 | 0.8711 | 0.8638 | |
| 64 | 1890 | 2.0587 | 20.7873 | 20.7624 | 0.0944 | 0.1276 | 0.8788 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.4030 | 21.3791 | 0.0906 | 0.1196 | 0.8849 | 0.8804 | |
| 66 | 2010 | 2.1894 | 21.2717 | 21.9524 | 0.0732 | 0.1120 | 0.8902 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.9175 | 20.8939 | 0.0895 | 0.1049 | 0.8956 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.7701 | 21.7511 | 0.0720 | 0.0983 | 0.9008 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.3447 | 21.3276 | 0.0648 | 0.0920 | 0.9053 | 0.9080 | |
| 70 | 2250 | 2.4508 | 21.4317 | 21.4211 | 0.0402 | 0.0862 | 0.9087 | 0.9138 | |

TABLA V-11
Número

Re2A1S2R1

| | tiempo | teta | W Total | W Seco | Ea | Ea Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.1261 | 21.1201 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0169 | 21.3003 | 21.0160 | 1.0778 | 0.9892 | 0.0059 | 0.0108 |
| 2 | 20 | 0.0218 | 21.4534 | 21.1733 | 1.0619 | 0.9785 | 0.0175 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8997 | 21.6220 | 1.0528 | 0.9679 | 0.0290 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6414 | 21.3841 | 1.0513 | 0.9574 | 0.0405 | 0.0426 |
| 5 | 50 | 0.0545 | 22.2632 | 21.9825 | 1.0641 | 0.9470 | 0.0520 | 0.0530 |
| 6 | 60 | 0.0654 | 21.4330 | 21.1575 | 1.0444 | 0.9367 | 0.0635 | 0.0633 |
| 7 | 70 | 0.0762 | 22.0967 | 21.8450 | 0.9542 | 0.9266 | 0.0744 | 0.0734 |
| 8 | 80 | 0.0871 | 20.8214 | 20.5354 | 1.0160 | 0.9165 | 0.0851 | 0.0835 |
| 9 | 90 | 0.0980 | 22.1035 | 21.8285 | 1.0425 | 0.9066 | 0.0963 | 0.0934 |
| 10 | 100 | 0.1089 | 21.4308 | 21.1730 | 0.9773 | 0.8968 | 0.1073 | 0.1032 |
| 11 | 110 | 0.1198 | 21.5933 | 21.3463 | 0.9591 | 0.8871 | 0.1179 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6242 | 21.4048 | 0.8697 | 0.8775 | 0.1278 | 0.1225 |
| 13 | 130 | 0.1416 | 21.0444 | 20.8010 | 0.9227 | 0.8680 | 0.1376 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2448 | 21.0020 | 0.9205 | 0.8586 | 0.1476 | 0.1414 |
| 15 | 150 | 0.1634 | 20.5762 | 20.3558 | 0.8355 | 0.8493 | 0.1572 | 0.1507 |
| 16 | 160 | 0.1743 | 21.2417 | 20.9972 | 0.9269 | 0.8401 | 0.1668 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4328 | 21.2030 | 0.8712 | 0.8310 | 0.1766 | 0.1690 |
| 18 | 180 | 0.1961 | 21.1281 | 20.9006 | 0.8625 | 0.8220 | 0.1860 | 0.1780 |
| 19 | 190 | 0.2070 | 21.2269 | 20.9942 | 0.8822 | 0.8131 | 0.1955 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0951 | 20.8270 | 0.8647 | 0.8042 | 0.2050 | 0.1950 |
| 21 | 210 | 0.2287 | 21.6215 | 21.3978 | 0.8481 | 0.7955 | 0.2144 | 0.2045 |
| 22 | 220 | 0.2396 | 21.1701 | 21.0535 | 0.8439 | 0.7869 | 0.2236 | 0.2131 |
| 23 | 230 | 0.2505 | 21.3217 | 21.0053 | 0.8204 | 0.7784 | 0.2327 | 0.2216 |
| 24 | 240 | 0.2614 | 21.4216 | 21.2029 | 0.8291 | 0.7700 | 0.2416 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2485 | 21.0408 | 0.7866 | 0.7616 | 0.2504 | 0.2384 |
| 26 | 260 | 0.2832 | 22.1247 | 21.9149 | 0.7954 | 0.7534 | 0.2591 | 0.2466 |
| 27 | 270 | 0.2941 | 21.8016 | 21.5932 | 0.7901 | 0.7452 | 0.2677 | 0.2548 |
| 28 | 280 | 0.3050 | 21.4815 | 21.2856 | 0.7427 | 0.7371 | 0.2760 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5319 | 21.3406 | 0.7252 | 0.7291 | 0.2840 | 0.2709 |
| 30 | 300 | 0.3268 | 21.6156 | 21.4234 | 0.7284 | 0.7212 | 0.2920 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4521 | 21.2621 | 0.7203 | 0.6981 | 0.3156 | 0.3019 |
| 32 | 360 | 0.3921 | 21.0861 | 20.9055 | 0.5847 | 0.6756 | 0.3386 | 0.3244 |
| 33 | 390 | 0.4248 | 20.8249 | 20.6459 | 0.6786 | 0.6539 | 0.3609 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4598 | 21.2910 | 0.6399 | 0.6329 | 0.3824 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1639 | 21.0068 | 0.6183 | 0.6125 | 0.4030 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3282 | 21.1733 | 0.5872 | 0.5928 | 0.4227 | 0.4072 |

TABLA V-11

| Número | tiempo | continuación.. | | Re2AlS2RI | | Ee | Ee Teor | Fe | Fe Teor |
|--------|--------|----------------|---------|-----------|--------|--------|---------|--------|---------|
| | | teta | W Total | W Seco | | | | | |
| 37 | 510 | 0.5555 | 21.3793 | 21.2265 | 0.5793 | 0.5738 | 0.4417 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.3610 | 21.2122 | 0.5641 | 0.5553 | 0.4604 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3730 | 21.2352 | 0.5224 | 0.5375 | 0.4781 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4636 | 21.3239 | 0.5296 | 0.5202 | 0.4953 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.7021 | 21.5677 | 0.5095 | 0.5035 | 0.5123 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.0811 | 20.9535 | 0.4837 | 0.4873 | 0.5285 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1876 | 21.0720 | 0.4458 | 0.4716 | 0.5437 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.8595 | 21.7414 | 0.4477 | 0.4565 | 0.5583 | 0.5425 | |
| 45 | 750 | 0.8169 | 21.2429 | 21.1387 | 0.3950 | 0.4418 | 0.5721 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1903 | 21.0880 | 0.3878 | 0.4138 | 0.5977 | 0.5862 | |
| 47 | 870 | 0.9476 | 20.6712 | 20.5723 | 0.3749 | 0.3877 | 0.6226 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5189 | 21.4273 | 0.3473 | 0.3631 | 0.6462 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7557 | 20.6665 | 0.3382 | 0.3402 | 0.6686 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3815 | 21.3022 | 0.3006 | 0.3186 | 0.6895 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4559 | 21.3826 | 0.2779 | 0.2985 | 0.7084 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.0094 | 21.0200 | 0.2631 | 0.2796 | 0.7261 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7587 | 20.6912 | 0.2559 | 0.2619 | 0.7430 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9171 | 20.8560 | 0.2316 | 0.2453 | 0.7589 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1594 | 21.1110 | 0.1835 | 0.2298 | 0.7725 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1590 | 21.1062 | 0.2002 | 0.2153 | 0.7850 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2122 | 21.1645 | 0.1808 | 0.2017 | 0.7975 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0206 | 20.9658 | 0.2077 | 0.1889 | 0.8102 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8279 | 20.7804 | 0.1801 | 0.1769 | 0.8229 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9583 | 20.9112 | 0.1786 | 0.1658 | 0.8346 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.3039 | 21.2579 | 0.1744 | 0.1553 | 0.8461 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7177 | 20.6759 | 0.1585 | 0.1454 | 0.8570 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2589 | 21.2269 | 0.1213 | 0.1362 | 0.8661 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.1988 | 21.1705 | 0.1073 | 0.1276 | 0.8736 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6824 | 21.6530 | 0.1115 | 0.1196 | 0.8808 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9877 | 20.9606 | 0.1027 | 0.1120 | 0.8878 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7818 | 20.7380 | 0.0902 | 0.1049 | 0.8941 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4287 | 21.4009 | 0.1054 | 0.0983 | 0.9005 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1147 | 21.0902 | 0.0929 | 0.0920 | 0.9069 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9483 | 20.9310 | 0.0656 | 0.0862 | 0.9121 | 0.9138 | |

TABLA V-12

| Número | tiempo | teta | W Total | W Seco | Ea | Ea Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.6834 | 21.6834 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 22.1059 | 21.8351 | 1.0266 | 0.9892 | 0.0056 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2842 | 21.0052 | 1.0577 | 0.9785 | 0.0169 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8840 | 21.6230 | 0.9895 | 0.9679 | 0.0281 | 0.0321 |
| 4 | 40 | 0.0436 | 20.9805 | 20.7218 | 0.9807 | 0.9574 | 0.0388 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5508 | 21.2925 | 0.9792 | 0.9470 | 0.0495 | 0.0530 |
| 6 | 60 | 0.0654 | 21.1903 | 20.9353 | 0.9667 | 0.9367 | 0.0601 | 0.0633 |
| 7 | 70 | 0.0762 | 21.2851 | 21.0274 | 0.9770 | 0.9266 | 0.0707 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5674 | 21.3105 | 0.9739 | 0.9165 | 0.0813 | 0.0835 |
| 9 | 90 | 0.0980 | 21.1413 | 20.8839 | 0.9758 | 0.9066 | 0.0919 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3714 | 21.1145 | 0.9739 | 0.8968 | 0.1025 | 0.1032 |
| 11 | 110 | 0.1198 | 21.0950 | 20.8437 | 0.9527 | 0.8871 | 0.1130 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1347 | 20.8985 | 0.8954 | 0.8775 | 0.1231 | 0.1225 |
| 13 | 130 | 0.1416 | 21.2873 | 21.0316 | 0.9694 | 0.8680 | 0.1333 | 0.1320 |
| 14 | 140 | 0.1525 | 21.3100 | 21.0473 | 0.9959 | 0.8586 | 0.1440 | 0.1414 |
| 15 | 150 | 0.1634 | 21.1420 | 20.8956 | 0.9341 | 0.8493 | 0.1545 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1431 | 20.9023 | 0.9129 | 0.8401 | 0.1645 | 0.1599 |
| 17 | 170 | 0.1852 | 21.1986 | 20.9715 | 0.8609 | 0.8310 | 0.1742 | 0.1690 |
| 18 | 180 | 0.1961 | 21.6834 | 21.4660 | 0.8166 | 0.8220 | 0.1833 | 0.1780 |
| 19 | 190 | 0.2070 | 21.0026 | 20.7805 | 0.8420 | 0.8131 | 0.1924 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4593 | 21.2343 | 0.8530 | 0.8042 | 0.2016 | 0.1958 |
| 21 | 210 | 0.2287 | 21.1667 | 20.9085 | 0.9788 | 0.7955 | 0.2116 | 0.2045 |
| 22 | 220 | 0.2396 | 21.1038 | 20.8615 | 0.9186 | 0.7869 | 0.2219 | 0.2131 |
| 23 | 230 | 0.2505 | 21.4829 | 21.2537 | 0.8689 | 0.7784 | 0.2316 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3642 | 21.1403 | 0.8488 | 0.7700 | 0.2410 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2843 | 21.0388 | 0.9307 | 0.7616 | 0.2507 | 0.2384 |
| 26 | 260 | 0.2832 | 21.3422 | 21.1112 | 0.8757 | 0.7534 | 0.2605 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7342 | 21.4903 | 0.9246 | 0.7452 | 0.2703 | 0.2540 |
| 28 | 280 | 0.3050 | 21.6071 | 21.3607 | 0.8583 | 0.7371 | 0.2800 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1686 | 20.9590 | 0.7946 | 0.7291 | 0.2890 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0706 | 20.8727 | 0.7502 | 0.7212 | 0.2975 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4103 | 21.2205 | 0.7195 | 0.6981 | 0.3215 | 0.3019 |
| 32 | 360 | 0.3921 | 21.4671 | 21.2876 | 0.6805 | 0.6756 | 0.3443 | 0.3244 |
| 33 | 390 | 0.4248 | 21.3813 | 21.2076 | 0.6585 | 0.6539 | 0.3662 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7579 | 21.5916 | 0.6305 | 0.6329 | 0.3873 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4478 | 21.2879 | 0.6062 | 0.6125 | 0.4075 | 0.3875 |
| 36 | 480 | 0.5228 | 21.2135 | 21.0565 | 0.5952 | 0.5928 | 0.4271 | 0.4072 |

TABLA V-12

continuación..

ReCAISCR2

| Número | tiempo | teta | W Total | W Seco | Ea | Ew Teor | Fe | Fe Teor |
|--------|--------|--------|---------|---------|--------|---------|--------|---------|
| 37 | 510 | 0.5555 | 21.0460 | 20.8947 | 0.5736 | 0.5738 | 0.4462 | 0.4262 |
| 38 | 540 | 0.5882 | 21.1705 | 21.0205 | 0.5690 | 0.5553 | 0.4649 | 0.4447 |
| 39 | 570 | 0.6209 | 21.2101 | 21.0682 | 0.5379 | 0.5375 | 0.4830 | 0.4625 |
| 40 | 600 | 0.6535 | 20.7371 | 20.6025 | 0.5103 | 0.5202 | 0.5001 | 0.4798 |
| 41 | 630 | 0.6862 | 21.3828 | 21.2470 | 0.5148 | 0.5035 | 0.5168 | 0.4965 |
| 42 | 660 | 0.7189 | 21.2970 | 21.1671 | 0.4925 | 0.4873 | 0.5333 | 0.5127 |
| 43 | 690 | 0.7516 | 20.9859 | 20.8635 | 0.4640 | 0.4716 | 0.5489 | 0.5284 |
| 44 | 720 | 0.7843 | 21.1676 | 21.0543 | 0.4295 | 0.4565 | 0.5635 | 0.5435 |
| 45 | 750 | 0.8169 | 21.0206 | 20.9145 | 0.4022 | 0.4418 | 0.5771 | 0.5582 |
| 46 | 810 | 0.8823 | 21.1215 | 21.0191 | 0.3882 | 0.4138 | 0.6029 | 0.5862 |
| 47 | 870 | 0.9476 | 21.2060 | 21.1049 | 0.3833 | 0.3877 | 0.6282 | 0.6123 |
| 48 | 930 | 1.0130 | 21.1025 | 21.0103 | 0.3495 | 0.3631 | 0.6521 | 0.6369 |
| 49 | 990 | 1.0783 | 21.2946 | 21.2059 | 0.3363 | 0.3402 | 0.6745 | 0.6598 |
| 50 | 1050 | 1.1437 | 21.1381 | 21.0598 | 0.2968 | 0.3186 | 0.6952 | 0.6814 |
| 51 | 1110 | 1.2091 | 21.2498 | 21.1725 | 0.2930 | 0.2985 | 0.7145 | 0.7015 |
| 52 | 1170 | 1.2744 | 20.7293 | 20.6603 | 0.2616 | 0.2796 | 0.7326 | 0.7204 |
| 53 | 1230 | 1.3398 | 21.0417 | 20.9756 | 0.2506 | 0.2619 | 0.7493 | 0.7381 |
| 54 | 1290 | 1.4051 | 20.9266 | 20.8636 | 0.2388 | 0.2453 | 0.7653 | 0.7547 |
| 55 | 1350 | 1.4705 | 21.2765 | 21.2235 | 0.2009 | 0.2298 | 0.7797 | 0.7702 |
| 56 | 1410 | 1.5358 | 21.2642 | 21.1977 | 0.2142 | 0.2153 | 0.7933 | 0.7847 |
| 57 | 1470 | 1.6012 | 21.1711 | 21.1120 | 0.2241 | 0.2017 | 0.8076 | 0.7983 |
| 58 | 1530 | 1.6665 | 21.9135 | 21.8620 | 0.1952 | 0.1889 | 0.8213 | 0.8111 |
| 59 | 1590 | 1.7319 | 20.8493 | 20.8056 | 0.1657 | 0.1769 | 0.8331 | 0.8231 |
| 60 | 1650 | 1.7972 | 21.7651 | 21.7307 | 0.1304 | 0.1658 | 0.8427 | 0.8342 |
| 61 | 1710 | 1.8626 | 21.4386 | 21.4003 | 0.1444 | 0.1553 | 0.8517 | 0.8447 |
| 62 | 1770 | 1.9280 | 21.5309 | 21.4962 | 0.1315 | 0.1454 | 0.8607 | 0.8546 |
| 63 | 1830 | 1.9933 | 21.3388 | 21.3107 | 0.1065 | 0.1362 | 0.8685 | 0.8638 |
| 64 | 1890 | 2.0587 | 20.7894 | 20.7624 | 0.1024 | 0.1276 | 0.8754 | 0.8724 |
| 65 | 1950 | 2.1240 | 21.4105 | 21.3791 | 0.1190 | 0.1196 | 0.8826 | 0.8804 |
| 66 | 2010 | 2.1894 | 21.9759 | 21.9524 | 0.0891 | 0.1120 | 0.8894 | 0.8880 |
| 67 | 2070 | 2.2547 | 20.9176 | 20.8939 | 0.0898 | 0.1049 | 0.8952 | 0.8951 |
| 68 | 2130 | 2.3201 | 21.7760 | 21.7511 | 0.0944 | 0.0983 | 0.9013 | 0.9017 |
| 69 | 2190 | 2.3854 | 21.3521 | 21.3276 | 0.0929 | 0.0920 | 0.9074 | 0.9080 |
| 70 | 2250 | 2.4508 | 21.4150 | 21.4135 | 0.0057 | 0.0882 | 0.9106 | 0.9138 |

TABLA V-13

Re2A2S1R1

| Número | tiempo | teta | W Total | W Seco | Ee | Ee Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.1619 | 21.1619 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.3095 | 21.0160 | 1.1127 | 0.9892 | 0.0061 | 0.0108 |
| 2 | 20 | 0.0218 | 21.4641 | 21.1733 | 1.1024 | 0.9785 | 0.0181 | 0.0215 |
| 3 | 30 | 0.0327 | 21.9107 | 21.6220 | 1.0945 | 0.9679 | 0.0301 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6510 | 21.3641 | 1.0877 | 0.9574 | 0.0420 | 0.0426 |
| 5 | 50 | 0.0545 | 22.2672 | 21.9825 | 1.0793 | 0.9470 | 0.0538 | 0.0530 |
| 6 | 60 | 0.0654 | 21.4352 | 21.1575 | 1.0528 | 0.9367 | 0.0654 | 0.0633 |
| 7 | 70 | 0.0762 | 22.1193 | 21.8450 | 1.0399 | 0.9266 | 0.0768 | 0.0734 |
| 8 | 80 | 0.0871 | 20.8290 | 20.5534 | 1.0448 | 0.9165 | 0.0881 | 0.0835 |
| 9 | 90 | 0.0980 | 22.1009 | 21.8285 | 1.0327 | 0.9066 | 0.0995 | 0.0934 |
| 10 | 100 | 0.1089 | 21.4437 | 21.1730 | 1.0262 | 0.8968 | 0.1107 | 0.1032 |
| 11 | 110 | 0.1198 | 21.6078 | 21.3403 | 1.0141 | 0.8871 | 0.1218 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6680 | 21.4048 | 0.9978 | 0.8775 | 0.1327 | 0.1225 |
| 13 | 130 | 0.1416 | 21.0619 | 20.8010 | 0.9891 | 0.8680 | 0.1436 | 0.1320 |
| 14 | 140 | 0.1525 | 21.2585 | 21.0020 | 0.9724 | 0.8586 | 0.1542 | 0.1414 |
| 15 | 150 | 0.1634 | 20.6118 | 20.3558 | 0.9705 | 0.8493 | 0.1648 | 0.1507 |
| 16 | 160 | 0.1743 | 21.2526 | 20.9972 | 0.9682 | 0.8401 | 0.1754 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4641 | 21.2030 | 0.9898 | 0.8310 | 0.1860 | 0.1690 |
| 18 | 180 | 0.1961 | 21.1619 | 20.9006 | 0.9906 | 0.8220 | 0.1968 | 0.1780 |
| 19 | 190 | 0.2070 | 21.2529 | 20.9942 | 0.9807 | 0.8131 | 0.2076 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0843 | 20.8270 | 0.9754 | 0.8042 | 0.2182 | 0.1958 |
| 21 | 210 | 0.2287 | 21.6538 | 21.3978 | 0.9705 | 0.7955 | 0.2288 | 0.2045 |
| 22 | 220 | 0.2396 | 21.3096 | 21.0555 | 0.9633 | 0.7869 | 0.2393 | 0.2131 |
| 23 | 230 | 0.2505 | 21.2560 | 21.0053 | 0.9504 | 0.7784 | 0.2498 | 0.2216 |
| 24 | 240 | 0.2614 | 21.4573 | 21.2029 | 0.9644 | 0.7700 | 0.2602 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2868 | 21.0408 | 0.9326 | 0.7616 | 0.2705 | 0.2384 |
| 26 | 260 | 0.2832 | 22.1578 | 21.9149 | 0.9208 | 0.7534 | 0.2806 | 0.2466 |
| 27 | 270 | 0.2941 | 21.8327 | 21.5932 | 0.9080 | 0.7452 | 0.2906 | 0.2548 |
| 28 | 280 | 0.3050 | 21.5205 | 21.2856 | 0.8905 | 0.7371 | 0.3004 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5739 | 21.3406 | 0.8845 | 0.7291 | 0.3100 | 0.2709 |
| 30 | 300 | 0.3268 | 21.6506 | 21.4234 | 0.8613 | 0.7212 | 0.3196 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4887 | 21.2621 | 0.8591 | 0.6981 | 0.3477 | 0.3019 |
| 32 | 360 | 0.3921 | 21.1175 | 20.9055 | 0.8037 | 0.6756 | 0.3748 | 0.3244 |
| 33 | 390 | 0.4248 | 20.8475 | 20.6459 | 0.7643 | 0.6539 | 0.4004 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4857 | 21.2910 | 0.7381 | 0.6329 | 0.4250 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1875 | 21.0008 | 0.7078 | 0.6125 | 0.4486 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3435 | 21.1733 | 0.6452 | 0.5928 | 0.4707 | 0.4072 |

TABLA V-13

| Número | tiempo | continuación.. | | Re2A2SIR1 | | | | | |
|--------|--------|----------------|---------|-----------|--------|---------|--------|---------|--|
| | | leta | W Total | W Seco | Ee | Ee Teor | Fe | Fe Teor | |
| 37 | 510 | 0.5555 | 21.3854 | 21.2265 | 0.6024 | 0.5738 | 0.4911 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.3688 | 21.2122 | 0.5937 | 0.5553 | 0.5107 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3779 | 21.2352 | 0.5410 | 0.5375 | 0.5292 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4592 | 21.3239 | 0.5129 | 0.5202 | 0.5464 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.6949 | 21.5677 | 0.4822 | 0.5035 | 0.5627 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.0755 | 20.9535 | 0.4625 | 0.4873 | 0.5781 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1909 | 21.0720 | 0.4508 | 0.4716 | 0.5930 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.8555 | 21.7414 | 0.4326 | 0.4565 | 0.6075 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2552 | 21.1387 | 0.4417 | 0.4418 | 0.6217 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1987 | 21.0080 | 0.4197 | 0.4138 | 0.6499 | 0.5862 | |
| 47 | 870 | 0.9476 | 20.6723 | 20.5723 | 0.3791 | 0.3877 | 0.6760 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5218 | 21.4273 | 0.3583 | 0.3631 | 0.7001 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7452 | 20.6665 | 0.2984 | 0.3402 | 0.7215 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3768 | 21.3022 | 0.2828 | 0.3186 | 0.7405 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4530 | 21.3826 | 0.2669 | 0.2985 | 0.7585 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.0803 | 21.0200 | 0.2286 | 0.2796 | 0.7747 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7452 | 20.6912 | 0.2047 | 0.2619 | 0.7888 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9088 | 20.8560 | 0.2002 | 0.2453 | 0.8021 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1582 | 21.1110 | 0.1789 | 0.2298 | 0.8145 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1464 | 21.1062 | 0.1524 | 0.2153 | 0.8253 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2034 | 21.1645 | 0.1475 | 0.2017 | 0.8351 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0035 | 20.9658 | 0.1429 | 0.1889 | 0.8446 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8124 | 20.7804 | 0.1213 | 0.1769 | 0.8532 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9402 | 20.9112 | 0.1099 | 0.1658 | 0.8608 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.2842 | 21.2579 | 0.0997 | 0.1553 | 0.8676 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7012 | 20.6759 | 0.0959 | 0.1454 | 0.8740 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2506 | 21.2269 | 0.0898 | 0.1362 | 0.8801 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.1900 | 21.1705 | 0.0739 | 0.1276 | 0.8854 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6730 | 21.6530 | 0.0758 | 0.1196 | 0.8903 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9790 | 20.9606 | 0.0698 | 0.1120 | 0.8951 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7533 | 20.7380 | 0.0580 | 0.1049 | 0.8993 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4143 | 21.4009 | 0.0508 | 0.0983 | 0.9028 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.1022 | 21.0902 | 0.0455 | 0.0920 | 0.9060 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9372 | 20.9310 | 0.0235 | 0.0862 | 0.9082 | 0.9138 | |

TABLA V-14

| Número | tiempo | leta | W Total | Re2A2S1R2 W Seco | Ee | Ee Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------------------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.7198 | 21.7198 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 22.1244 | 21.8351 | 1.0967 | 0.9892 | 0.0060 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2960 | 21.0052 | 1.1024 | 0.9785 | 0.0180 | 0.0215 |
| 3 | 30 | 0.0327 | 21.8980 | 21.6230 | 1.0425 | 0.9679 | 0.0296 | 0.0321 |
| 4 | 40 | 0.0436 | 21.0026 | 20.7218 | 1.0645 | 0.9574 | 0.0411 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5666 | 21.2925 | 1.0391 | 0.9470 | 0.0526 | 0.0530 |
| 6 | 60 | 0.0654 | 21.2114 | 20.9353 | 1.0467 | 0.9367 | 0.0639 | 0.0633 |
| 7 | 70 | 0.0762 | 21.3035 | 21.0274 | 1.0467 | 0.9266 | 0.0753 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5750 | 21.3105 | 1.0027 | 0.9165 | 0.0865 | 0.0835 |
| 9 | 90 | 0.0980 | 21.1470 | 20.8839 | 0.9974 | 0.9066 | 0.0974 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3822 | 21.1145 | 1.0149 | 0.8968 | 0.1083 | 0.1032 |
| 11 | 110 | 0.1198 | 21.1127 | 20.8437 | 1.0198 | 0.8871 | 0.1194 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1635 | 20.8965 | 1.0046 | 0.8775 | 0.1304 | 0.1225 |
| 13 | 130 | 0.1416 | 21.2990 | 21.0316 | 1.0157 | 0.8680 | 0.1414 | 0.1320 |
| 14 | 140 | 0.1525 | 21.3120 | 21.0473 | 1.0035 | 0.8586 | 0.1524 | 0.1414 |
| 15 | 150 | 0.1634 | 21.1535 | 20.8956 | 0.9777 | 0.8493 | 0.1632 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1615 | 20.9023 | 0.9826 | 0.8401 | 0.1739 | 0.1599 |
| 17 | 170 | 0.1852 | 21.2227 | 20.9715 | 0.9523 | 0.8310 | 0.1844 | 0.1690 |
| 18 | 180 | 0.1961 | 21.7198 | 21.4680 | 0.9546 | 0.8220 | 0.1948 | 0.1780 |
| 19 | 190 | 0.2070 | 21.0358 | 20.7805 | 0.9679 | 0.8131 | 0.2053 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4803 | 21.2343 | 0.9326 | 0.8042 | 0.2156 | 0.1958 |
| 21 | 210 | 0.2287 | 21.1457 | 20.9085 | 0.8992 | 0.7955 | 0.2256 | 0.2045 |
| 22 | 220 | 0.2396 | 21.0898 | 20.8615 | 0.8655 | 0.7869 | 0.2352 | 0.2131 |
| 23 | 230 | 0.2505 | 21.4866 | 21.2537 | 0.8029 | 0.7784 | 0.2447 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3717 | 21.1403 | 0.8772 | 0.7700 | 0.2543 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2656 | 21.0388 | 0.8598 | 0.7616 | 0.2638 | 0.2384 |
| 26 | 260 | 0.2832 | 21.2158 | 20.9758 | 0.8340 | 0.7534 | 0.2730 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7091 | 21.4903 | 0.8295 | 0.7452 | 0.2821 | 0.2548 |
| 28 | 280 | 0.3050 | 21.6184 | 21.3807 | 0.9011 | 0.7371 | 0.2915 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1897 | 20.9590 | 0.8746 | 0.7291 | 0.3012 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0974 | 20.8727 | 0.8526 | 0.7212 | 0.3106 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4326 | 21.2205 | 0.8041 | 0.6981 | 0.3376 | 0.3019 |
| 32 | 360 | 0.3921 | 21.4929 | 21.2876 | 0.7783 | 0.6756 | 0.3635 | 0.3244 |
| 33 | 390 | 0.4248 | 21.4052 | 21.2076 | 0.7529 | 0.6539 | 0.3885 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7820 | 21.5916 | 0.7218 | 0.6329 | 0.4126 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4751 | 21.2879 | 0.7097 | 0.6125 | 0.4360 | 0.3875 |
| 36 | 480 | 0.5228 | 21.2286 | 21.0565 | 0.6524 | 0.5928 | 0.4583 | 0.4072 |

TABLA V-14

| Número | Tiempo | continuación.. | | Re2A2SIR2 | | | | | |
|--------|--------|----------------|---------|-----------|--------|---------|--------|---------|--|
| | | tota | W total | W Seco | Ee | Ee Teor | Fe | Fe Teor | |
| 37 | 510 | 0.5555 | 21.0520 | 20.8947 | 0.5963 | 0.5738 | 0.4787 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.1800 | 21.0205 | 0.6047 | 0.5553 | 0.4983 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.2239 | 21.0682 | 0.5903 | 0.5375 | 0.5178 | 0.4625 | |
| 40 | 600 | 0.6535 | 20.7606 | 20.6025 | 0.5994 | 0.5202 | 0.5372 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.3846 | 21.2470 | 0.5216 | 0.5035 | 0.5556 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.3061 | 21.1671 | 0.5270 | 0.4873 | 0.5727 | 0.5127 | |
| 43 | 690 | 0.7516 | 20.9975 | 20.8635 | 0.5080 | 0.4716 | 0.5896 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.1805 | 21.0543 | 0.4784 | 0.4565 | 0.6057 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.0217 | 20.9145 | 0.4064 | 0.4418 | 0.6202 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1244 | 21.0191 | 0.3992 | 0.4138 | 0.6465 | 0.5862 | |
| 47 | 870 | 0.9476 | 21.2038 | 21.1049 | 0.3749 | 0.3877 | 0.6718 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.1003 | 21.0103 | 0.3412 | 0.3631 | 0.6952 | 0.6369 | |
| 49 | 990 | 1.0783 | 21.2942 | 21.2059 | 0.3347 | 0.3402 | 0.7173 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.1367 | 21.0598 | 0.2915 | 0.3186 | 0.7378 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.2425 | 21.1723 | 0.2654 | 0.2985 | 0.7559 | 0.7015 | |
| 52 | 1170 | 1.2744 | 20.7300 | 20.6603 | 0.2642 | 0.2796 | 0.7733 | 0.7204 | |
| 53 | 1230 | 1.3398 | 21.0316 | 20.9756 | 0.2123 | 0.2619 | 0.7888 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9186 | 20.8636 | 0.2085 | 0.2453 | 0.8026 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.2710 | 21.2235 | 0.1801 | 0.2298 | 0.8153 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.2380 | 21.1977 | 0.1528 | 0.2153 | 0.8262 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.1466 | 21.1120 | 0.1312 | 0.2017 | 0.8354 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.8965 | 21.8620 | 0.1308 | 0.1889 | 0.8440 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8359 | 20.8056 | 0.1149 | 0.1769 | 0.8520 | 0.8231 | |
| 60 | 1650 | 1.7972 | 21.7601 | 21.7307 | 0.1115 | 0.1658 | 0.8594 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.4295 | 21.4005 | 0.1099 | 0.1553 | 0.8666 | 0.8447 | |
| 62 | 1770 | 1.9280 | 21.5226 | 21.4962 | 0.1001 | 0.1454 | 0.8735 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.3362 | 21.3107 | 0.0957 | 0.1362 | 0.8799 | 0.8638 | |
| 64 | 1890 | 2.0587 | 20.7866 | 20.7624 | 0.0917 | 0.1276 | 0.8861 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.3989 | 21.3791 | 0.0751 | 0.1196 | 0.8915 | 0.8804 | |
| 66 | 2010 | 2.1894 | 21.9716 | 21.9524 | 0.0728 | 0.1120 | 0.8964 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.9096 | 20.8939 | 0.0595 | 0.1049 | 0.9007 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.7652 | 21.7511 | 0.0535 | 0.0983 | 0.9044 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.3400 | 21.3276 | 0.0470 | 0.0920 | 0.9077 | 0.9080 | |
| 70 | 2250 | 2.4508 | 21.4202 | 21.4135 | 0.0254 | 0.0862 | 0.9100 | 0.9138 | |

TABLA V-15

Re2A2S2K1

| Número | tiempo | teta | W Total | W Seco | Ea | Ea Teor | Fe | Fe Teor |
|---------|--------|--------|---------|---------|--------|---------|--------|---------|
| inicial | 0 | 0.0000 | 21.1378 | 21.1378 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 21.2918 | 21.0160 | 1.0456 | 0.9892 | 0.0057 | 0.0108 |
| 2 | 20 | 0.0218 | 21.4540 | 21.1733 | 1.0641 | 0.9785 | 0.0172 | 0.0215 |
| 3 | 30 | 0.0327 | 21.7049 | 21.6220 | 1.0725 | 0.9679 | 0.0288 | 0.0321 |
| 4 | 40 | 0.0436 | 21.6530 | 21.3641 | 1.0952 | 0.9574 | 0.0406 | 0.0426 |
| 5 | 50 | 0.0545 | 22.2604 | 21.9825 | 1.0535 | 0.9470 | 0.0523 | 0.0530 |
| 6 | 60 | 0.0654 | 21.4386 | 21.1575 | 1.0657 | 0.9367 | 0.0639 | 0.0633 |
| 7 | 70 | 0.0762 | 22.1152 | 21.8459 | 1.0243 | 0.9266 | 0.0753 | 0.0734 |
| 8 | 80 | 0.0871 | 20.8214 | 20.5534 | 1.0160 | 0.9165 | 0.0864 | 0.0835 |
| 9 | 90 | 0.0980 | 22.1043 | 21.8285 | 1.0456 | 0.9066 | 0.0976 | 0.0934 |
| 10 | 100 | 0.1089 | 21.4412 | 21.1730 | 1.0168 | 0.8968 | 0.1088 | 0.1032 |
| 11 | 110 | 0.1198 | 21.5914 | 21.3463 | 0.9519 | 0.8871 | 0.1195 | 0.1129 |
| 12 | 120 | 0.1307 | 21.6658 | 21.4048 | 0.9895 | 0.8775 | 0.1301 | 0.1225 |
| 13 | 130 | 0.1416 | 21.9357 | 20.8010 | 0.8936 | 0.8680 | 0.1404 | 0.1320 |
| 14 | 140 | 0.1525 | 21.3516 | 21.0020 | 0.9462 | 0.8586 | 0.1504 | 0.1414 |
| 15 | 150 | 0.1634 | 20.5945 | 20.3558 | 0.9049 | 0.8493 | 0.1605 | 0.1507 |
| 16 | 160 | 0.1743 | 21.2362 | 20.9972 | 0.9061 | 0.8401 | 0.1703 | 0.1599 |
| 17 | 170 | 0.1852 | 21.4324 | 21.2030 | 0.8697 | 0.8310 | 0.1800 | 0.1690 |
| 18 | 180 | 0.1961 | 21.1378 | 20.9006 | 0.8992 | 0.8220 | 0.1896 | 0.1780 |
| 19 | 190 | 0.2070 | 21.2243 | 20.9942 | 0.8723 | 0.8131 | 0.1993 | 0.1869 |
| 20 | 200 | 0.2178 | 21.0608 | 20.8270 | 0.8863 | 0.8042 | 0.2089 | 0.1958 |
| 21 | 210 | 0.2287 | 21.6225 | 21.3978 | 0.8518 | 0.7953 | 0.2183 | 0.2045 |
| 22 | 220 | 0.2396 | 21.2828 | 21.0555 | 0.8617 | 0.7869 | 0.2277 | 0.2131 |
| 23 | 230 | 0.2505 | 21.2320 | 21.0053 | 0.8594 | 0.7784 | 0.2370 | 0.2216 |
| 24 | 240 | 0.2614 | 21.4300 | 21.2029 | 0.8609 | 0.7700 | 0.2464 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2732 | 21.0408 | 0.8810 | 0.7616 | 0.2559 | 0.2384 |
| 26 | 260 | 0.2832 | 22.1358 | 21.9149 | 0.8374 | 0.7534 | 0.2653 | 0.2466 |
| 27 | 270 | 0.2941 | 21.8146 | 21.5932 | 0.8393 | 0.7452 | 0.2744 | 0.2548 |
| 28 | 280 | 0.3050 | 21.5062 | 21.2856 | 0.8363 | 0.7371 | 0.2835 | 0.2629 |
| 29 | 290 | 0.3159 | 21.5469 | 21.3406 | 0.7821 | 0.7291 | 0.2923 | 0.2709 |
| 30 | 300 | 0.3268 | 21.6342 | 21.4234 | 0.7992 | 0.7212 | 0.3009 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4664 | 21.2621 | 0.7745 | 0.6981 | 0.3267 | 0.3019 |
| 32 | 360 | 0.3921 | 21.1058 | 20.9055 | 0.7592 | 0.6756 | 0.3517 | 0.3244 |
| 33 | 390 | 0.4248 | 20.8306 | 20.6459 | 0.7002 | 0.6539 | 0.3756 | 0.3461 |
| 34 | 420 | 0.4575 | 21.4720 | 21.2910 | 0.6862 | 0.6329 | 0.3982 | 0.3671 |
| 35 | 450 | 0.4902 | 21.1803 | 21.0008 | 0.6805 | 0.6125 | 0.4205 | 0.3875 |
| 36 | 480 | 0.5228 | 21.3416 | 21.1733 | 0.6380 | 0.5928 | 0.4421 | 0.4072 |

TABLA V-15

| Número | Tiempo | continuación.. | | Re2A252R1 | | | | | |
|--------|--------|----------------|---------|-----------|--------|---------|--------|---------|--|
| | | teta | W Total | W Seco | Ea | Ea Teor | Fe | Fe Teor | |
| 37 | 510 | 0.5555 | 21.3777 | 21.2265 | 0.5732 | 0.5738 | 0.4619 | 0.4262 | |
| 38 | 540 | 0.5882 | 21.3542 | 21.2122 | 0.5383 | 0.5553 | 0.4800 | 0.4447 | |
| 39 | 570 | 0.6209 | 21.3766 | 21.2352 | 0.5361 | 0.5375 | 0.4976 | 0.4625 | |
| 40 | 600 | 0.6535 | 21.4637 | 21.3239 | 0.5300 | 0.5202 | 0.5150 | 0.4798 | |
| 41 | 630 | 0.6862 | 21.7015 | 21.5677 | 0.5072 | 0.5035 | 0.5320 | 0.4965 | |
| 42 | 660 | 0.7189 | 21.0746 | 20.9535 | 0.4591 | 0.4873 | 0.5477 | 0.5127 | |
| 43 | 690 | 0.7516 | 21.1923 | 21.0720 | 0.4561 | 0.4716 | 0.5627 | 0.5284 | |
| 44 | 720 | 0.7843 | 21.0637 | 21.7414 | 0.4636 | 0.4565 | 0.5777 | 0.5435 | |
| 45 | 750 | 0.8169 | 21.2516 | 21.1387 | 0.4280 | 0.4418 | 0.5923 | 0.5582 | |
| 46 | 810 | 0.8823 | 21.1936 | 21.0880 | 0.4003 | 0.4138 | 0.6194 | 0.5862 | |
| 47 | 870 | 0.9476 | 20.6716 | 20.5723 | 0.3765 | 0.3877 | 0.6447 | 0.6123 | |
| 48 | 930 | 1.0130 | 21.5220 | 21.4273 | 0.3590 | 0.3631 | 0.6688 | 0.6369 | |
| 49 | 990 | 1.0783 | 20.7542 | 20.6665 | 0.3325 | 0.3402 | 0.6914 | 0.6598 | |
| 50 | 1050 | 1.1437 | 21.3773 | 21.3022 | 0.2847 | 0.3186 | 0.7115 | 0.6814 | |
| 51 | 1110 | 1.2091 | 21.4571 | 21.3826 | 0.2824 | 0.2985 | 0.7301 | 0.7015 | |
| 52 | 1170 | 1.2744 | 21.0872 | 21.0200 | 0.2548 | 0.2796 | 0.7476 | 0.7204 | |
| 53 | 1230 | 1.3398 | 20.7571 | 20.6912 | 0.2498 | 0.2619 | 0.7641 | 0.7381 | |
| 54 | 1290 | 1.4051 | 20.9164 | 20.8560 | 0.2290 | 0.2453 | 0.7798 | 0.7547 | |
| 55 | 1350 | 1.4705 | 21.1652 | 21.1110 | 0.2055 | 0.2298 | 0.7940 | 0.7702 | |
| 56 | 1410 | 1.5358 | 21.1617 | 21.1062 | 0.2104 | 0.2153 | 0.8075 | 0.7847 | |
| 57 | 1470 | 1.6012 | 21.2153 | 21.1645 | 0.1926 | 0.2017 | 0.8207 | 0.7983 | |
| 58 | 1530 | 1.6665 | 21.0109 | 20.9658 | 0.1710 | 0.1889 | 0.8326 | 0.8111 | |
| 59 | 1590 | 1.7319 | 20.8224 | 20.7804 | 0.1592 | 0.1769 | 0.8434 | 0.8231 | |
| 60 | 1650 | 1.7972 | 20.9488 | 20.9112 | 0.1425 | 0.1658 | 0.8532 | 0.8342 | |
| 61 | 1710 | 1.8626 | 21.2928 | 21.2579 | 0.1323 | 0.1553 | 0.8622 | 0.8447 | |
| 62 | 1770 | 1.9280 | 20.7070 | 20.6759 | 0.1179 | 0.1454 | 0.8704 | 0.8546 | |
| 63 | 1830 | 1.9933 | 21.2566 | 21.2269 | 0.1126 | 0.1362 | 0.8779 | 0.8638 | |
| 64 | 1890 | 2.0587 | 21.1928 | 21.1705 | 0.0845 | 0.1276 | 0.8844 | 0.8724 | |
| 65 | 1950 | 2.1240 | 21.6721 | 21.6530 | 0.0724 | 0.1196 | 0.8895 | 0.8804 | |
| 66 | 2010 | 2.1894 | 20.9739 | 20.9606 | 0.0504 | 0.1120 | 0.8935 | 0.8880 | |
| 67 | 2070 | 2.2547 | 20.7504 | 20.7380 | 0.0470 | 0.1049 | 0.8967 | 0.8951 | |
| 68 | 2130 | 2.3201 | 21.4112 | 21.4009 | 0.0390 | 0.0983 | 0.8995 | 0.9017 | |
| 69 | 2190 | 2.3854 | 21.0976 | 21.0902 | 0.0281 | 0.0920 | 0.9017 | 0.9080 | |
| 70 | 2250 | 2.4508 | 20.9382 | 20.9310 | 0.0273 | 0.0862 | 0.9035 | 0.9138 | |

TABLA V-16

| Número | tiempo | beta | Re2A2S2R2 | | Ea | Ea Teor | Fe | Fe Teor |
|---------|--------|--------|-----------|---------|--------|---------|--------|---------|
| | | | W Total | W Seco | | | | |
| inicial | 0 | 0.0000 | 21.7065 | 21.7065 | 0.0000 | 1.0000 | 0.0000 | 0.0000 |
| 1 | 10 | 0.0109 | 22.1275 | 21.8351 | 1.1085 | 0.9692 | 0.0060 | 0.0108 |
| 2 | 20 | 0.0218 | 21.2770 | 21.0052 | 1.0304 | 0.9785 | 0.0177 | 0.0215 |
| 3 | 30 | 0.0327 | 21.9029 | 21.6230 | 1.0611 | 0.9879 | 0.0291 | 0.0321 |
| 4 | 40 | 0.0436 | 20.9981 | 20.7218 | 1.0475 | 0.9574 | 0.0406 | 0.0426 |
| 5 | 50 | 0.0545 | 21.5565 | 21.2925 | 1.0008 | 0.9470 | 0.0517 | 0.0530 |
| 6 | 60 | 0.0654 | 21.2035 | 20.9205 | 1.0168 | 0.9367 | 0.0627 | 0.0633 |
| 7 | 70 | 0.0762 | 21.2941 | 21.0274 | 1.0111 | 0.9266 | 0.0737 | 0.0734 |
| 8 | 80 | 0.0871 | 21.5681 | 21.3105 | 1.0524 | 0.9165 | 0.0850 | 0.0835 |
| 9 | 90 | 0.0980 | 21.1512 | 20.8039 | 1.0133 | 0.9066 | 0.0962 | 0.0934 |
| 10 | 100 | 0.1089 | 21.3667 | 21.1145 | 0.9561 | 0.8968 | 0.1070 | 0.1032 |
| 11 | 110 | 0.1198 | 21.0923 | 20.8437 | 0.9425 | 0.8871 | 0.1173 | 0.1129 |
| 12 | 120 | 0.1307 | 21.1512 | 20.8985 | 0.9580 | 0.8775 | 0.1277 | 0.1225 |
| 13 | 130 | 0.1416 | 21.2747 | 21.0316 | 0.9216 | 0.8680 | 0.1379 | 0.1320 |
| 14 | 140 | 0.1525 | 21.3029 | 21.0473 | 0.9690 | 0.8586 | 0.1482 | 0.1414 |
| 15 | 150 | 0.1634 | 21.1354 | 20.8956 | 0.9091 | 0.8493 | 0.1584 | 0.1507 |
| 16 | 160 | 0.1743 | 21.1423 | 20.9023 | 0.9099 | 0.8401 | 0.1683 | 0.1599 |
| 17 | 170 | 0.1852 | 21.2060 | 20.9715 | 0.8663 | 0.8310 | 0.1780 | 0.1690 |
| 18 | 180 | 0.1961 | 21.7065 | 21.4680 | 0.9042 | 0.8220 | 0.1876 | 0.1780 |
| 19 | 190 | 0.2070 | 21.6050 | 20.7865 | 0.8511 | 0.8131 | 0.1972 | 0.1869 |
| 20 | 200 | 0.2178 | 21.4574 | 21.2343 | 0.8458 | 0.8042 | 0.2064 | 0.1958 |
| 21 | 210 | 0.2287 | 21.1340 | 20.9085 | 0.8200 | 0.7955 | 0.2155 | 0.2045 |
| 22 | 220 | 0.2396 | 21.0720 | 20.8615 | 0.7980 | 0.7869 | 0.2243 | 0.2131 |
| 23 | 230 | 0.2505 | 21.4731 | 21.2537 | 0.8318 | 0.7784 | 0.2332 | 0.2216 |
| 24 | 240 | 0.2614 | 21.3532 | 21.1403 | 0.8071 | 0.7700 | 0.2421 | 0.2300 |
| 25 | 250 | 0.2723 | 21.2544 | 21.0388 | 0.8173 | 0.7616 | 0.2510 | 0.2384 |
| 26 | 260 | 0.2832 | 21.2170 | 20.9958 | 0.8386 | 0.7534 | 0.2600 | 0.2466 |
| 27 | 270 | 0.2941 | 21.7049 | 21.4903 | 0.8136 | 0.7452 | 0.2690 | 0.2548 |
| 28 | 280 | 0.3050 | 21.5915 | 21.3807 | 0.7992 | 0.7371 | 0.2778 | 0.2629 |
| 29 | 290 | 0.3159 | 21.1731 | 20.9500 | 0.8117 | 0.7291 | 0.2865 | 0.2709 |
| 30 | 300 | 0.3268 | 21.0812 | 20.8727 | 0.7904 | 0.7212 | 0.2953 | 0.2788 |
| 31 | 330 | 0.3594 | 21.4220 | 21.2205 | 0.7639 | 0.6981 | 0.3207 | 0.3019 |
| 32 | 360 | 0.3921 | 21.4863 | 21.2876 | 0.7533 | 0.6756 | 0.3455 | 0.3244 |
| 33 | 390 | 0.4248 | 21.3939 | 21.2075 | 0.7063 | 0.6539 | 0.3693 | 0.3461 |
| 34 | 420 | 0.4575 | 21.7624 | 21.5916 | 0.6975 | 0.6329 | 0.3914 | 0.3671 |
| 35 | 450 | 0.4902 | 21.4426 | 21.2679 | 0.6016 | 0.6125 | 0.4118 | 0.3875 |
| 36 | 480 | 0.5228 | 21.2065 | 21.0565 | 0.5887 | 0.5928 | 0.4309 | 0.4072 |

TABLA V-16

continuacion..

Re2N2S2K2

| Número | tiempo | Letra | W Total | W Seco | Ea | Ea Teor | Fe | Fe Teor |
|--------|--------|--------|---------|---------|--------|---------|--------|---------|
| 37 | 510 | 0.5555 | 21.0363 | 20.8947 | 0.5368 | 0.5738 | 0.4490 | 0.4262 |
| 38 | 540 | 0.5802 | 21.1665 | 21.0205 | 0.5535 | 0.5553 | 0.4668 | 0.4447 |
| 39 | 570 | 0.6209 | 21.2113 | 21.0682 | 0.5425 | 0.5375 | 0.4847 | 0.4625 |
| 40 | 600 | 0.6535 | 20.7425 | 20.6025 | 0.5307 | 0.5202 | 0.5023 | 0.4798 |
| 41 | 630 | 0.6662 | 21.3798 | 21.2470 | 0.5035 | 0.5035 | 0.5192 | 0.4965 |
| 42 | 660 | 0.7189 | 21.2895 | 21.1671 | 0.4640 | 0.4873 | 0.5350 | 0.5127 |
| 43 | 690 | 0.7516 | 20.9862 | 20.8635 | 0.4652 | 0.4716 | 0.5502 | 0.5284 |
| 44 | 720 | 0.7843 | 21.1676 | 21.0543 | 0.4295 | 0.4565 | 0.5648 | 0.5435 |
| 45 | 750 | 0.8169 | 21.0227 | 20.9145 | 0.4102 | 0.4418 | 0.5785 | 0.5582 |
| 46 | 810 | 0.8823 | 21.1196 | 21.0191 | 0.3810 | 0.4138 | 0.6043 | 0.5862 |
| 47 | 870 | 0.9476 | 21.2020 | 21.1049 | 0.3681 | 0.3877 | 0.6288 | 0.6123 |
| 48 | 930 | 1.0130 | 21.1045 | 21.0103 | 0.3571 | 0.3631 | 0.6525 | 0.6369 |
| 49 | 990 | 1.0783 | 21.2965 | 21.2059 | 0.3435 | 0.3402 | 0.6754 | 0.6598 |
| 50 | 1050 | 1.1437 | 21.1364 | 21.0598 | 0.2904 | 0.3186 | 0.6961 | 0.6814 |
| 51 | 1110 | 1.2091 | 21.2416 | 21.1725 | 0.2620 | 0.2985 | 0.7142 | 0.7015 |
| 52 | 1170 | 1.2744 | 20.7249 | 20.6603 | 0.2449 | 0.2796 | 0.7307 | 0.7204 |
| 53 | 1230 | 1.3398 | 21.0428 | 20.9756 | 0.2548 | 0.2619 | 0.7471 | 0.7381 |
| 54 | 1290 | 1.4051 | 20.9269 | 20.8636 | 0.2400 | 0.2453 | 0.7632 | 0.7547 |
| 55 | 1350 | 1.4705 | 21.2824 | 21.2235 | 0.2233 | 0.2298 | 0.7784 | 0.7702 |
| 56 | 1410 | 1.5358 | 21.2528 | 21.1977 | 0.2089 | 0.2153 | 0.7925 | 0.7847 |
| 57 | 1470 | 1.6012 | 21.1615 | 21.1120 | 0.1877 | 0.2017 | 0.8055 | 0.7983 |
| 58 | 1530 | 1.6665 | 21.9054 | 21.8620 | 0.1645 | 0.1889 | 0.8170 | 0.8111 |
| 59 | 1590 | 1.7319 | 20.8475 | 20.8056 | 0.1588 | 0.1769 | 0.8275 | 0.8231 |
| 60 | 1650 | 1.7972 | 21.7684 | 21.7307 | 0.1429 | 0.1658 | 0.8374 | 0.8342 |
| 61 | 1710 | 1.8626 | 21.4398 | 21.4005 | 0.1490 | 0.1553 | 0.8469 | 0.8447 |
| 62 | 1770 | 1.9280 | 21.5379 | 21.4962 | 0.1202 | 0.1454 | 0.8557 | 0.8546 |
| 63 | 1830 | 1.9933 | 21.3416 | 21.3107 | 0.1171 | 0.1362 | 0.8635 | 0.8638 |
| 64 | 1890 | 2.0587 | 20.7921 | 20.7624 | 0.1126 | 0.1276 | 0.8710 | 0.8724 |
| 65 | 1950 | 2.1240 | 21.4041 | 21.3791 | 0.0948 | 0.1196 | 0.8778 | 0.8804 |
| 66 | 2010 | 2.1894 | 21.9742 | 21.9524 | 0.0826 | 0.1120 | 0.8836 | 0.8880 |
| 67 | 2070 | 2.2547 | 20.9109 | 20.8939 | 0.0644 | 0.1049 | 0.8884 | 0.8951 |
| 68 | 2130 | 2.3201 | 21.7650 | 21.7511 | 0.0527 | 0.0983 | 0.8922 | 0.9017 |
| 69 | 2190 | 2.3854 | 21.3402 | 21.3276 | 0.0478 | 0.0920 | 0.8955 | 0.9080 |
| 70 | 2250 | 2.4508 | 21.4195 | 21.4135 | 0.0227 | 0.0862 | 0.8978 | 0.9138 |

APÉNDICE VI

TRATAMIENTO ESTADÍSTICO

T R A T A M I E N T O E S T A D Í S T I C O

La siguiente serie de tablas corresponde al tratamiento estadístico aplicado a cada corrida, con el fin de comprobar si la curva experimental tiene la misma distribución que la curva teórica.

La numeración de estas tablas incluye la letra A que equivale al tratamiento estadístico para cada una de las corridas. El número romano corresponde al número del apéndice (en este caso apéndice VI) y el segundo dígito corresponde al número de la corrida.

Para esta primera serie de tablas, la nomenclatura se explica a continuación:

Número = Número de frecuencias acumuladas.

F_e = Frecuencia acumulada experimental.

F_e Teor = Frecuencia teórica acumulada, calculada a partir de valores continuos (ec. IV-A7).

F_e teor2 = Frecuencia teórica acumulada, calculada a partir de valores discretos (ec. IV-A8).

DIF-A = Desviación para la prueba estadística

$$\left| F_e \text{ teor2}(e) - F_e(e) \right|.$$

A°1 = Desviación para la prueba estadística

$$\left| F_e \text{ teor1}(e) - F_e(e-1) \right|.$$

A°2 = Desviación para la prueba estadística

$$\left| F_e \text{ teor1}(e) - F_o(e) \right|.$$

TABLA VI-1-A

| Número | RelAISIR1 | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0052 | 0.0108 | 0.0108 | 0.0108 | 0.0056 | 0.0056 |
| 2 | 0.0157 | 0.0215 | 0.0215 | 0.0163 | 0.0059 | 0.0059 |
| 3 | 0.0261 | 0.0321 | 0.0321 | 0.0165 | 0.0061 | 0.0061 |
| 4 | 0.0366 | 0.0426 | 0.0426 | 0.0166 | 0.0060 | 0.0060 |
| 5 | 0.0469 | 0.0530 | 0.0530 | 0.0164 | 0.0061 | 0.0061 |
| 6 | 0.0568 | 0.0633 | 0.0633 | 0.0164 | 0.0065 | 0.0065 |
| 7 | 0.0667 | 0.0734 | 0.0734 | 0.0166 | 0.0068 | 0.0068 |
| 8 | 0.0766 | 0.0835 | 0.0835 | 0.0168 | 0.0069 | 0.0069 |
| 9 | 0.0864 | 0.0934 | 0.0934 | 0.0168 | 0.0070 | 0.0070 |
| 10 | 0.0960 | 0.1032 | 0.1032 | 0.0168 | 0.0072 | 0.0072 |
| 11 | 0.1053 | 0.1129 | 0.1129 | 0.0170 | 0.0076 | 0.0076 |
| 12 | 0.1146 | 0.1225 | 0.1225 | 0.0172 | 0.0079 | 0.0079 |
| 13 | 0.1240 | 0.1320 | 0.1320 | 0.0174 | 0.0081 | 0.0081 |
| 14 | 0.1335 | 0.1414 | 0.1414 | 0.0175 | 0.0080 | 0.0080 |
| 15 | 0.1430 | 0.1507 | 0.1507 | 0.0173 | 0.0078 | 0.0078 |
| 16 | 0.1523 | 0.1599 | 0.1599 | 0.0170 | 0.0076 | 0.0076 |
| 17 | 0.1614 | 0.1690 | 0.1690 | 0.0167 | 0.0076 | 0.0076 |
| 18 | 0.1705 | 0.1780 | 0.1780 | 0.0166 | 0.0076 | 0.0076 |
| 19 | 0.1794 | 0.1869 | 0.1869 | 0.0165 | 0.0075 | 0.0075 |
| 20 | 0.1881 | 0.1958 | 0.1958 | 0.0163 | 0.0077 | 0.0077 |
| 21 | 0.1964 | 0.2045 | 0.2045 | 0.0164 | 0.0081 | 0.0081 |
| 22 | 0.2045 | 0.2131 | 0.2131 | 0.0167 | 0.0086 | 0.0086 |
| 23 | 0.2127 | 0.2216 | 0.2216 | 0.0172 | 0.0089 | 0.0089 |
| 24 | 0.2210 | 0.2300 | 0.2300 | 0.0173 | 0.0090 | 0.0090 |
| 25 | 0.2292 | 0.2384 | 0.2384 | 0.0174 | 0.0092 | 0.0092 |
| 26 | 0.2372 | 0.2466 | 0.2466 | 0.0174 | 0.0094 | 0.0094 |
| 27 | 0.2451 | 0.2548 | 0.2548 | 0.0176 | 0.0097 | 0.0097 |
| 28 | 0.2527 | 0.2629 | 0.2629 | 0.0178 | 0.0102 | 0.0102 |
| 29 | 0.2603 | 0.2709 | 0.2709 | 0.0182 | 0.0106 | 0.0106 |
| 30 | 0.2676 | 0.2788 | 0.2788 | 0.0185 | 0.0111 | 0.0111 |
| 31 | 0.2892 | 0.3019 | 0.3019 | 0.0343 | 0.0128 | 0.0128 |
| 32 | 0.3115 | 0.3244 | 0.3244 | 0.0352 | 0.0129 | 0.0129 |
| 33 | 0.3340 | 0.3461 | 0.3461 | 0.0346 | 0.0121 | 0.0121 |
| 34 | 0.3555 | 0.3671 | 0.3671 | 0.0331 | 0.0117 | 0.0117 |
| 35 | 0.3759 | 0.3875 | 0.3875 | 0.0320 | 0.0116 | 0.0116 |
| 36 | 0.3965 | 0.4072 | 0.4072 | 0.0313 | 0.0106 | 0.0106 |

TABLA VI-1-A
Número

| | continuación.. | | ReIAISIRI | Ao1 | Ao2 | DIF-A |
|----|----------------|---------|-----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | | | |
| 37 | 0.4170 | 0.4262 | 0.4262 | 0.0297 | 0.0092 | 0.0092 |
| 38 | 0.4366 | 0.4447 | 0.4447 | 0.0277 | 0.0080 | 0.0081 |
| 39 | 0.4552 | 0.4625 | 0.4625 | 0.0259 | 0.0073 | 0.0074 |
| 40 | 0.4728 | 0.4798 | 0.4798 | 0.0246 | 0.0070 | 0.0070 |
| 41 | 0.4898 | 0.4965 | 0.4965 | 0.0237 | 0.0067 | 0.0067 |
| 42 | 0.5066 | 0.5127 | 0.5127 | 0.0229 | 0.0061 | 0.0062 |
| 43 | 0.5227 | 0.5284 | 0.5284 | 0.0218 | 0.0057 | 0.0057 |
| 44 | 0.5384 | 0.5435 | 0.5436 | 0.0208 | 0.0051 | 0.0051 |
| 45 | 0.5540 | 0.5582 | 0.5582 | 0.0198 | 0.0042 | 0.0042 |
| 46 | 0.5635 | 0.5662 | 0.5662 | 0.0321 | 0.0027 | 0.0027 |
| 47 | 0.6098 | 0.6123 | 0.6124 | 0.0289 | 0.0026 | 0.0026 |
| 48 | 0.6339 | 0.6369 | 0.6369 | 0.0271 | 0.0029 | 0.0030 |
| 49 | 0.6564 | 0.6598 | 0.6599 | 0.0259 | 0.0035 | 0.0035 |
| 50 | 0.6769 | 0.6814 | 0.6814 | 0.0250 | 0.0045 | 0.0045 |
| 51 | 0.6960 | 0.7015 | 0.7016 | 0.0246 | 0.0055 | 0.0056 |
| 52 | 0.7141 | 0.7204 | 0.7205 | 0.0244 | 0.0063 | 0.0064 |
| 53 | 0.7316 | 0.7381 | 0.7382 | 0.0240 | 0.0065 | 0.0066 |
| 54 | 0.7483 | 0.7547 | 0.7548 | 0.0230 | 0.0064 | 0.0065 |
| 55 | 0.7638 | 0.7702 | 0.7703 | 0.0219 | 0.0064 | 0.0065 |
| 56 | 0.7780 | 0.7847 | 0.7848 | 0.0209 | 0.0068 | 0.0069 |
| 57 | 0.7913 | 0.7983 | 0.7985 | 0.0204 | 0.0071 | 0.0072 |
| 58 | 0.8040 | 0.8111 | 0.8112 | 0.0198 | 0.0071 | 0.0072 |
| 59 | 0.8155 | 0.8231 | 0.8232 | 0.0191 | 0.0075 | 0.0076 |
| 60 | 0.8265 | 0.8342 | 0.8344 | 0.0187 | 0.0078 | 0.0079 |
| 61 | 0.8372 | 0.8447 | 0.8449 | 0.0183 | 0.0075 | 0.0076 |
| 62 | 0.8475 | 0.8546 | 0.8547 | 0.0173 | 0.0070 | 0.0072 |
| 63 | 0.8572 | 0.8638 | 0.8639 | 0.0162 | 0.0066 | 0.0067 |
| 64 | 0.8662 | 0.8724 | 0.8725 | 0.0152 | 0.0062 | 0.0063 |
| 65 | 0.8753 | 0.8804 | 0.8806 | 0.0143 | 0.0051 | 0.0053 |
| 66 | 0.8846 | 0.8880 | 0.8882 | 0.0127 | 0.0034 | 0.0035 |
| 67 | 0.8920 | 0.8951 | 0.8952 | 0.0105 | 0.0031 | 0.0032 |
| 68 | 0.8977 | 0.9017 | 0.9019 | 0.0097 | 0.0040 | 0.0041 |
| 69 | 0.9039 | 0.9080 | 0.9081 | 0.0102 | 0.0041 | 0.0042 |
| 70 | 0.9073 | 0.9138 | 0.9139 | 0.0099 | 0.0065 | 0.0066 |

TABLA VI-2-A

| Número | RelAISIRL | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fa | Fa Teor | Fa teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0053 | 0.0108 | 0.0108 | 0.0108 | 0.0056 | 0.0056 |
| 2 | 0.0158 | 0.0215 | 0.0215 | 0.0163 | 0.0057 | 0.0057 |
| 3 | 0.0263 | 0.0321 | 0.0321 | 0.0163 | 0.0059 | 0.0059 |
| 4 | 0.0366 | 0.0426 | 0.0426 | 0.0164 | 0.0060 | 0.0060 |
| 5 | 0.0467 | 0.0530 | 0.0530 | 0.0164 | 0.0063 | 0.0063 |
| 6 | 0.0567 | 0.0633 | 0.0633 | 0.0165 | 0.0066 | 0.0066 |
| 7 | 0.0665 | 0.0734 | 0.0734 | 0.0167 | 0.0069 | 0.0069 |
| 8 | 0.0762 | 0.0835 | 0.0835 | 0.0169 | 0.0072 | 0.0072 |
| 9 | 0.0858 | 0.0934 | 0.0934 | 0.0172 | 0.0076 | 0.0076 |
| 10 | 0.0954 | 0.1032 | 0.1032 | 0.0174 | 0.0078 | 0.0078 |
| 11 | 0.1048 | 0.1129 | 0.1129 | 0.0176 | 0.0081 | 0.0081 |
| 12 | 0.1142 | 0.1225 | 0.1225 | 0.0177 | 0.0084 | 0.0084 |
| 13 | 0.1236 | 0.1320 | 0.1320 | 0.0179 | 0.0084 | 0.0084 |
| 14 | 0.1333 | 0.1414 | 0.1414 | 0.0178 | 0.0081 | 0.0081 |
| 15 | 0.1428 | 0.1507 | 0.1507 | 0.0174 | 0.0080 | 0.0080 |
| 16 | 0.1521 | 0.1599 | 0.1599 | 0.0172 | 0.0078 | 0.0079 |
| 17 | 0.1611 | 0.1690 | 0.1690 | 0.0169 | 0.0079 | 0.0079 |
| 18 | 0.1695 | 0.1780 | 0.1780 | 0.0169 | 0.0085 | 0.0085 |
| 19 | 0.1777 | 0.1869 | 0.1869 | 0.0174 | 0.0093 | 0.0093 |
| 20 | 0.1859 | 0.1958 | 0.1958 | 0.0181 | 0.0099 | 0.0099 |
| 21 | 0.1942 | 0.2045 | 0.2045 | 0.0186 | 0.0103 | 0.0103 |
| 22 | 0.2027 | 0.2131 | 0.2131 | 0.0189 | 0.0103 | 0.0103 |
| 23 | 0.2112 | 0.2216 | 0.2216 | 0.0189 | 0.0104 | 0.0104 |
| 24 | 0.2195 | 0.2300 | 0.2300 | 0.0188 | 0.0105 | 0.0105 |
| 25 | 0.2279 | 0.2384 | 0.2384 | 0.0189 | 0.0105 | 0.0105 |
| 26 | 0.2364 | 0.2466 | 0.2466 | 0.0187 | 0.0102 | 0.0102 |
| 27 | 0.2449 | 0.2548 | 0.2548 | 0.0184 | 0.0099 | 0.0099 |
| 28 | 0.2526 | 0.2629 | 0.2629 | 0.0180 | 0.0103 | 0.0103 |
| 29 | 0.2601 | 0.2709 | 0.2709 | 0.0183 | 0.0107 | 0.0107 |
| 30 | 0.2678 | 0.2788 | 0.2788 | 0.0186 | 0.0109 | 0.0109 |
| 31 | 0.2902 | 0.3019 | 0.3019 | 0.0341 | 0.0118 | 0.0118 |
| 32 | 0.3114 | 0.3244 | 0.3244 | 0.0342 | 0.0129 | 0.0130 |
| 33 | 0.3325 | 0.3461 | 0.3461 | 0.0347 | 0.0136 | 0.0136 |
| 34 | 0.3541 | 0.3671 | 0.3671 | 0.0346 | 0.0130 | 0.0130 |
| 35 | 0.3746 | 0.3875 | 0.3875 | 0.0333 | 0.0128 | 0.0129 |
| 36 | 0.3931 | 0.4072 | 0.4072 | 0.0325 | 0.0141 | 0.0141 |

TABLA VI-2-A
 Número

| | continuación.. | | RelA1S1R2 | | | |
|----|----------------|---------|-----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
| 37 | 0.4105 | 0.4262 | 0.4262 | 0.0331 | 0.0157 | 0.0157 |
| 38 | 0.4275 | 0.4447 | 0.4447 | 0.0341 | 0.0172 | 0.0172 |
| 39 | 0.4453 | 0.4625 | 0.4625 | 0.0350 | 0.0172 | 0.0172 |
| 40 | 0.4632 | 0.4798 | 0.4798 | 0.0345 | 0.0166 | 0.0166 |
| 41 | 0.4796 | 0.4965 | 0.4965 | 0.0333 | 0.0169 | 0.0170 |
| 42 | 0.4957 | 0.5127 | 0.5127 | 0.0331 | 0.0170 | 0.0171 |
| 43 | 0.5115 | 0.5284 | 0.5284 | 0.0327 | 0.0169 | 0.0169 |
| 44 | 0.5268 | 0.5435 | 0.5436 | 0.0321 | 0.0167 | 0.0168 |
| 45 | 0.5416 | 0.5582 | 0.5582 | 0.0314 | 0.0167 | 0.0167 |
| 46 | 0.5697 | 0.5862 | 0.5862 | 0.0446 | 0.0164 | 0.0165 |
| 47 | 0.5957 | 0.6123 | 0.6124 | 0.0426 | 0.0167 | 0.0167 |
| 48 | 0.6200 | 0.6369 | 0.6369 | 0.0412 | 0.0168 | 0.0169 |
| 49 | 0.6437 | 0.6598 | 0.6599 | 0.0398 | 0.0162 | 0.0162 |
| 50 | 0.6661 | 0.6814 | 0.6814 | 0.0377 | 0.0152 | 0.0153 |
| 51 | 0.6872 | 0.7015 | 0.7016 | 0.0354 | 0.0143 | 0.0144 |
| 52 | 0.7072 | 0.7204 | 0.7205 | 0.0332 | 0.0132 | 0.0133 |
| 53 | 0.7262 | 0.7381 | 0.7382 | 0.0309 | 0.0119 | 0.0120 |
| 54 | 0.7442 | 0.7547 | 0.7548 | 0.0284 | 0.0105 | 0.0106 |
| 55 | 0.7601 | 0.7702 | 0.7703 | 0.0260 | 0.0100 | 0.0101 |
| 56 | 0.7741 | 0.7847 | 0.7848 | 0.0246 | 0.0106 | 0.0107 |
| 57 | 0.7856 | 0.7983 | 0.7985 | 0.0242 | 0.0127 | 0.0128 |
| 58 | 0.7968 | 0.8111 | 0.8112 | 0.0255 | 0.0143 | 0.0144 |
| 59 | 0.8093 | 0.8231 | 0.8232 | 0.0262 | 0.0138 | 0.0139 |
| 60 | 0.8210 | 0.8342 | 0.8344 | 0.0249 | 0.0132 | 0.0134 |
| 61 | 0.8319 | 0.8447 | 0.8449 | 0.0237 | 0.0128 | 0.0130 |
| 62 | 0.8427 | 0.8546 | 0.8547 | 0.0227 | 0.0118 | 0.0119 |
| 63 | 0.8530 | 0.8638 | 0.8639 | 0.0210 | 0.0107 | 0.0109 |
| 64 | 0.8622 | 0.8724 | 0.8725 | 0.0194 | 0.0102 | 0.0103 |
| 65 | 0.8712 | 0.8804 | 0.8806 | 0.0183 | 0.0092 | 0.0093 |
| 66 | 0.8803 | 0.8880 | 0.8882 | 0.0168 | 0.0077 | 0.0079 |
| 67 | 0.8890 | 0.8951 | 0.8952 | 0.0148 | 0.0061 | 0.0063 |
| 68 | 0.8972 | 0.9017 | 0.9019 | 0.0127 | 0.0045 | 0.0047 |
| 69 | 0.9046 | 0.9080 | 0.9081 | 0.0108 | 0.0034 | 0.0035 |
| 70 | 0.9085 | 0.9138 | 0.9139 | 0.0092 | 0.0053 | 0.0054 |

TABLA VI-3-A

| Número | RelA1S2R1 | | RelA1S2R2 | | Ao1 | Ao2 | DIF-A |
|---------|-----------|---------|-----------|--------|--------|--------|--------|
| | Fu | Fo Teor | Fu | teor2 | | | |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0049 | 0.0108 | 0.0108 | 0.0108 | 0.0060 | 0.0060 | 0.0060 |
| 2 | 0.0144 | 0.0215 | 0.0215 | 0.0215 | 0.0167 | 0.0071 | 0.0071 |
| 3 | 0.0237 | 0.0321 | 0.0321 | 0.0321 | 0.0177 | 0.0085 | 0.0085 |
| 4 | 0.0332 | 0.0426 | 0.0426 | 0.0426 | 0.0190 | 0.0094 | 0.0094 |
| 5 | 0.0431 | 0.0530 | 0.0530 | 0.0530 | 0.0198 | 0.0100 | 0.0100 |
| 6 | 0.0525 | 0.0633 | 0.0633 | 0.0633 | 0.0202 | 0.0108 | 0.0108 |
| 7 | 0.0619 | 0.0734 | 0.0734 | 0.0734 | 0.0209 | 0.0115 | 0.0115 |
| 8 | 0.0715 | 0.0835 | 0.0835 | 0.0835 | 0.0215 | 0.0120 | 0.0120 |
| 9 | 0.0803 | 0.0934 | 0.0934 | 0.0934 | 0.0219 | 0.0131 | 0.0131 |
| 10 | 0.0890 | 0.1032 | 0.1032 | 0.1032 | 0.0229 | 0.0142 | 0.0142 |
| 11 | 0.0981 | 0.1129 | 0.1129 | 0.1129 | 0.0239 | 0.0148 | 0.0148 |
| 12 | 0.1072 | 0.1225 | 0.1225 | 0.1225 | 0.0244 | 0.0154 | 0.0154 |
| 13 | 0.1160 | 0.1320 | 0.1320 | 0.1320 | 0.0249 | 0.0161 | 0.0161 |
| 14 | 0.1245 | 0.1414 | 0.1414 | 0.1414 | 0.0255 | 0.0170 | 0.0170 |
| 15 | 0.1327 | 0.1507 | 0.1507 | 0.1507 | 0.0263 | 0.0180 | 0.0180 |
| 16 | 0.1412 | 0.1599 | 0.1599 | 0.1599 | 0.0272 | 0.0187 | 0.0187 |
| 17 | 0.1498 | 0.1690 | 0.1690 | 0.1690 | 0.0278 | 0.0192 | 0.0192 |
| 18 | 0.1580 | 0.1780 | 0.1780 | 0.1780 | 0.0282 | 0.0201 | 0.0201 |
| 19 | 0.1661 | 0.1869 | 0.1869 | 0.1869 | 0.0290 | 0.0209 | 0.0209 |
| 20 | 0.1742 | 0.1958 | 0.1958 | 0.1958 | 0.0297 | 0.0215 | 0.0215 |
| 21 | 0.1821 | 0.2045 | 0.2045 | 0.2045 | 0.0302 | 0.0223 | 0.0223 |
| 22 | 0.1898 | 0.2131 | 0.2131 | 0.2131 | 0.0310 | 0.0233 | 0.0233 |
| 23 | 0.1975 | 0.2216 | 0.2216 | 0.2216 | 0.0318 | 0.0241 | 0.0241 |
| 24 | 0.2052 | 0.2300 | 0.2300 | 0.2300 | 0.0325 | 0.0248 | 0.0248 |
| 25 | 0.2132 | 0.2384 | 0.2384 | 0.2384 | 0.0332 | 0.0252 | 0.0252 |
| 26 | 0.2212 | 0.2466 | 0.2466 | 0.2466 | 0.0334 | 0.0255 | 0.0255 |
| 27 | 0.2286 | 0.2548 | 0.2548 | 0.2548 | 0.0336 | 0.0262 | 0.0262 |
| 28 | 0.2362 | 0.2629 | 0.2629 | 0.2629 | 0.0342 | 0.0267 | 0.0267 |
| 29 | 0.2441 | 0.2709 | 0.2709 | 0.2709 | 0.0347 | 0.0268 | 0.0268 |
| 30 | 0.2520 | 0.2788 | 0.2788 | 0.2788 | 0.0347 | 0.0268 | 0.0268 |
| 31 | 0.2741 | 0.3019 | 0.3019 | 0.3019 | 0.0500 | 0.0278 | 0.0278 |
| 32 | 0.2954 | 0.3244 | 0.3244 | 0.3244 | 0.0503 | 0.0290 | 0.0290 |
| 33 | 0.3160 | 0.3461 | 0.3461 | 0.3461 | 0.0507 | 0.0301 | 0.0301 |
| 34 | 0.3359 | 0.3671 | 0.3671 | 0.3671 | 0.0511 | 0.0313 | 0.0313 |
| 35 | 0.3553 | 0.3875 | 0.3875 | 0.3875 | 0.0516 | 0.0322 | 0.0322 |
| 36 | 0.3745 | 0.4072 | 0.4072 | 0.4072 | 0.0519 | 0.0327 | 0.0327 |

TABLA VI-3-A
Número

| | continuación.. | | ReJAIS2R1 | Ao1 | Ao2 | DIF-A |
|----|----------------|---------|-----------|--------|--------|--------|
| | Fa | Fa Teor | Fa teor2 | | | |
| 37 | 0.3927 | 0.4262 | 0.4262 | 0.0517 | 0.0335 | 0.0336 |
| 38 | 0.4100 | 0.4447 | 0.4447 | 0.0520 | 0.0347 | 0.0347 |
| 39 | 0.4274 | 0.4625 | 0.4625 | 0.0526 | 0.0351 | 0.0352 |
| 40 | 0.4441 | 0.4798 | 0.4798 | 0.0524 | 0.0357 | 0.0357 |
| 41 | 0.4599 | 0.4965 | 0.4965 | 0.0524 | 0.0366 | 0.0366 |
| 42 | 0.4751 | 0.5127 | 0.5127 | 0.0528 | 0.0376 | 0.0376 |
| 43 | 0.4900 | 0.5284 | 0.5284 | 0.0533 | 0.0384 | 0.0384 |
| 44 | 0.5044 | 0.5435 | 0.5436 | 0.0536 | 0.0391 | 0.0392 |
| 45 | 0.5185 | 0.5582 | 0.5582 | 0.0538 | 0.0397 | 0.0397 |
| 46 | 0.5462 | 0.5862 | 0.5862 | 0.0677 | 0.0400 | 0.0400 |
| 47 | 0.5715 | 0.6123 | 0.6124 | 0.0662 | 0.0409 | 0.0409 |
| 48 | 0.5950 | 0.6369 | 0.6369 | 0.0654 | 0.0419 | 0.0420 |
| 49 | 0.6185 | 0.6598 | 0.6599 | 0.0649 | 0.0413 | 0.0414 |
| 50 | 0.6411 | 0.6814 | 0.6814 | 0.0628 | 0.0403 | 0.0404 |
| 51 | 0.6614 | 0.7015 | 0.7016 | 0.0605 | 0.0401 | 0.0402 |
| 52 | 0.6816 | 0.7204 | 0.7205 | 0.0590 | 0.0389 | 0.0389 |
| 53 | 0.7012 | 0.7381 | 0.7382 | 0.0565 | 0.0369 | 0.0370 |
| 54 | 0.7195 | 0.7547 | 0.7548 | 0.0535 | 0.0352 | 0.0353 |
| 55 | 0.7373 | 0.7702 | 0.7703 | 0.0507 | 0.0328 | 0.0329 |
| 56 | 0.7541 | 0.7847 | 0.7848 | 0.0474 | 0.0306 | 0.0307 |
| 57 | 0.7693 | 0.7983 | 0.7985 | 0.0442 | 0.0291 | 0.0292 |
| 58 | 0.7838 | 0.8111 | 0.8112 | 0.0418 | 0.0273 | 0.0274 |
| 59 | 0.7972 | 0.8231 | 0.8232 | 0.0393 | 0.0258 | 0.0259 |
| 60 | 0.8099 | 0.8342 | 0.8344 | 0.0370 | 0.0244 | 0.0245 |
| 61 | 0.8221 | 0.8447 | 0.8449 | 0.0348 | 0.0227 | 0.0228 |
| 62 | 0.8334 | 0.8546 | 0.8547 | 0.0325 | 0.0211 | 0.0213 |
| 63 | 0.8445 | 0.8638 | 0.8639 | 0.0303 | 0.0192 | 0.0193 |
| 64 | 0.8552 | 0.8724 | 0.8725 | 0.0278 | 0.0172 | 0.0173 |
| 65 | 0.8651 | 0.8804 | 0.8806 | 0.0253 | 0.0154 | 0.0155 |
| 66 | 0.8744 | 0.8880 | 0.8882 | 0.0229 | 0.0136 | 0.0137 |
| 67 | 0.8833 | 0.8951 | 0.8952 | 0.0207 | 0.0118 | 0.0120 |
| 68 | 0.8918 | 0.9017 | 0.9019 | 0.0185 | 0.0100 | 0.0101 |
| 69 | 0.9000 | 0.9080 | 0.9081 | 0.0162 | 0.0079 | 0.0081 |
| 70 | 0.9045 | 0.9138 | 0.9139 | 0.0142 | 0.0093 | 0.0095 |

TABLA VI-4-A

| Número | RelAIS2RS | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0051 | 0.0108 | 0.0108 | 0.0108 | 0.0057 | 0.0057 |
| 2 | 0.0155 | 0.0215 | 0.0215 | 0.0108 | 0.0061 | 0.0061 |
| 3 | 0.0259 | 0.0321 | 0.0321 | 0.0167 | 0.0063 | 0.0063 |
| 4 | 0.0360 | 0.0426 | 0.0426 | 0.0168 | 0.0066 | 0.0066 |
| 5 | 0.0458 | 0.0530 | 0.0530 | 0.0170 | 0.0072 | 0.0072 |
| 6 | 0.0557 | 0.0633 | 0.0633 | 0.0174 | 0.0076 | 0.0076 |
| 7 | 0.0649 | 0.0734 | 0.0734 | 0.0177 | 0.0086 | 0.0086 |
| 8 | 0.0733 | 0.0835 | 0.0835 | 0.0186 | 0.0102 | 0.0102 |
| 9 | 0.0817 | 0.0934 | 0.0934 | 0.0201 | 0.0117 | 0.0117 |
| 10 | 0.0904 | 0.1032 | 0.1032 | 0.0215 | 0.0128 | 0.0128 |
| 11 | 0.0994 | 0.1129 | 0.1129 | 0.0226 | 0.0136 | 0.0136 |
| 12 | 0.1084 | 0.1225 | 0.1225 | 0.0232 | 0.0141 | 0.0141 |
| 13 | 0.1172 | 0.1320 | 0.1320 | 0.0236 | 0.0148 | 0.0148 |
| 14 | 0.1259 | 0.1414 | 0.1414 | 0.0242 | 0.0155 | 0.0155 |
| 15 | 0.1343 | 0.1507 | 0.1507 | 0.0248 | 0.0164 | 0.0164 |
| 16 | 0.1426 | 0.1599 | 0.1599 | 0.0256 | 0.0173 | 0.0173 |
| 17 | 0.1511 | 0.1690 | 0.1690 | 0.0264 | 0.0180 | 0.0180 |
| 18 | 0.1596 | 0.1780 | 0.1780 | 0.0270 | 0.0185 | 0.0185 |
| 19 | 0.1678 | 0.1869 | 0.1869 | 0.0274 | 0.0191 | 0.0191 |
| 20 | 0.1759 | 0.1958 | 0.1958 | 0.0279 | 0.0198 | 0.0198 |
| 21 | 0.1840 | 0.2045 | 0.2045 | 0.0285 | 0.0205 | 0.0205 |
| 22 | 0.1921 | 0.2131 | 0.2131 | 0.0291 | 0.0210 | 0.0210 |
| 23 | 0.2001 | 0.2216 | 0.2216 | 0.0295 | 0.0215 | 0.0215 |
| 24 | 0.2078 | 0.2300 | 0.2300 | 0.0300 | 0.0222 | 0.0222 |
| 25 | 0.2155 | 0.2384 | 0.2384 | 0.0306 | 0.0228 | 0.0228 |
| 26 | 0.2233 | 0.2466 | 0.2466 | 0.0311 | 0.0233 | 0.0233 |
| 27 | 0.2311 | 0.2548 | 0.2548 | 0.0315 | 0.0236 | 0.0236 |
| 28 | 0.2389 | 0.2629 | 0.2629 | 0.0317 | 0.0240 | 0.0240 |
| 29 | 0.2465 | 0.2709 | 0.2709 | 0.0320 | 0.0243 | 0.0243 |
| 30 | 0.2539 | 0.2788 | 0.2788 | 0.0322 | 0.0248 | 0.0248 |
| 31 | 0.2752 | 0.3019 | 0.3019 | 0.0480 | 0.0267 | 0.0267 |
| 32 | 0.2963 | 0.3244 | 0.3244 | 0.0492 | 0.0281 | 0.0281 |
| 33 | 0.3172 | 0.3461 | 0.3461 | 0.0498 | 0.0289 | 0.0289 |
| 34 | 0.3377 | 0.3671 | 0.3671 | 0.0499 | 0.0294 | 0.0294 |
| 35 | 0.3580 | 0.3875 | 0.3875 | 0.0497 | 0.0295 | 0.0295 |
| 36 | 0.3774 | 0.4072 | 0.4072 | 0.0492 | 0.0297 | 0.0297 |

TABLA VI-4-A
Número

| | continuación.. | | RelAIS2R2 | | Ao1 | Ao2 | DIF-A |
|----|----------------|---------|-----------|--------|--------|--------|-------|
| | Fo | Fo Teor | Fo | teor2 | | | |
| 37 | 0.3959 | 0.4262 | 0.4262 | 0.0488 | 0.0304 | 0.0304 | |
| 38 | 0.4139 | 0.4447 | 0.4447 | 0.0408 | 0.0308 | 0.0308 | |
| 39 | 0.4315 | 0.4625 | 0.4625 | 0.0486 | 0.0310 | 0.0310 | |
| 40 | 0.4487 | 0.4798 | 0.4798 | 0.0483 | 0.0311 | 0.0311 | |
| 41 | 0.4652 | 0.4965 | 0.4965 | 0.0478 | 0.0313 | 0.0313 | |
| 42 | 0.4809 | 0.5127 | 0.5127 | 0.0475 | 0.0318 | 0.0318 | |
| 43 | 0.4963 | 0.5284 | 0.5284 | 0.0474 | 0.0321 | 0.0321 | |
| 44 | 0.5112 | 0.5435 | 0.5436 | 0.0473 | 0.0323 | 0.0323 | |
| 45 | 0.5256 | 0.5582 | 0.5582 | 0.0470 | 0.0326 | 0.0326 | |
| 46 | 0.5529 | 0.5862 | 0.5862 | 0.0605 | 0.0333 | 0.0333 | |
| 47 | 0.5784 | 0.6123 | 0.6124 | 0.0594 | 0.0339 | 0.0340 | |
| 48 | 0.6021 | 0.6369 | 0.6369 | 0.0585 | 0.0348 | 0.0349 | |
| 49 | 0.6239 | 0.6598 | 0.6599 | 0.0578 | 0.0360 | 0.0360 | |
| 50 | 0.6447 | 0.6814 | 0.6814 | 0.0575 | 0.0367 | 0.0368 | |
| 51 | 0.6652 | 0.7015 | 0.7016 | 0.0568 | 0.0363 | 0.0364 | |
| 52 | 0.6850 | 0.7204 | 0.7205 | 0.0552 | 0.0354 | 0.0354 | |
| 53 | 0.7040 | 0.7381 | 0.7382 | 0.0530 | 0.0340 | 0.0341 | |
| 54 | 0.7217 | 0.7547 | 0.7548 | 0.0506 | 0.0330 | 0.0331 | |
| 55 | 0.7388 | 0.7702 | 0.7703 | 0.0485 | 0.0314 | 0.0315 | |
| 56 | 0.7564 | 0.7847 | 0.7848 | 0.0460 | 0.0283 | 0.0285 | |
| 57 | 0.7731 | 0.7983 | 0.7985 | 0.0420 | 0.0252 | 0.0254 | |
| 58 | 0.7884 | 0.8111 | 0.8112 | 0.0380 | 0.0227 | 0.0228 | |
| 59 | 0.8028 | 0.8231 | 0.8232 | 0.0347 | 0.0203 | 0.0204 | |
| 60 | 0.8160 | 0.8342 | 0.8344 | 0.0315 | 0.0182 | 0.0184 | |
| 61 | 0.8281 | 0.8447 | 0.8449 | 0.0287 | 0.0166 | 0.0168 | |
| 62 | 0.8397 | 0.8546 | 0.8547 | 0.0265 | 0.0148 | 0.0150 | |
| 63 | 0.8507 | 0.8638 | 0.8639 | 0.0240 | 0.0131 | 0.0132 | |
| 64 | 0.8612 | 0.8724 | 0.8725 | 0.0217 | 0.0112 | 0.0113 | |
| 65 | 0.8716 | 0.8804 | 0.8806 | 0.0193 | 0.0089 | 0.0090 | |
| 66 | 0.8816 | 0.8880 | 0.8882 | 0.0164 | 0.0064 | 0.0066 | |
| 67 | 0.8905 | 0.8951 | 0.8952 | 0.0135 | 0.0046 | 0.0048 | |
| 68 | 0.8984 | 0.9017 | 0.9019 | 0.0113 | 0.0033 | 0.0035 | |
| 69 | 0.9057 | 0.9080 | 0.9081 | 0.0095 | 0.0022 | 0.0024 | |
| 70 | 0.9115 | 0.9138 | 0.9139 | 0.0081 | 0.0023 | 0.0025 | |

TABLA VI-5-A

| Número | RelA2SIR1 | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0052 | 0.0108 | 0.0108 | 0.0108 | 0.0057 | 0.0057 |
| 2 | 0.0154 | 0.0215 | 0.0215 | 0.0164 | 0.0061 | 0.0061 |
| 3 | 0.0259 | 0.0321 | 0.0321 | 0.0167 | 0.0063 | 0.0063 |
| 4 | 0.0367 | 0.0426 | 0.0426 | 0.0167 | 0.0059 | 0.0059 |
| 5 | 0.0471 | 0.0530 | 0.0530 | 0.0163 | 0.0059 | 0.0059 |
| 6 | 0.0574 | 0.0633 | 0.0633 | 0.0161 | 0.0059 | 0.0059 |
| 7 | 0.0677 | 0.0734 | 0.0734 | 0.0160 | 0.0057 | 0.0057 |
| 8 | 0.0775 | 0.0835 | 0.0835 | 0.0157 | 0.0059 | 0.0059 |
| 9 | 0.0873 | 0.0934 | 0.0934 | 0.0158 | 0.0061 | 0.0061 |
| 10 | 0.0969 | 0.1032 | 0.1032 | 0.0159 | 0.0064 | 0.0064 |
| 11 | 0.1064 | 0.1129 | 0.1129 | 0.0161 | 0.0066 | 0.0066 |
| 12 | 0.1159 | 0.1225 | 0.1225 | 0.0162 | 0.0066 | 0.0066 |
| 13 | 0.1249 | 0.1320 | 0.1320 | 0.0161 | 0.0071 | 0.0071 |
| 14 | 0.1341 | 0.1414 | 0.1414 | 0.0165 | 0.0074 | 0.0074 |
| 15 | 0.1437 | 0.1507 | 0.1507 | 0.0167 | 0.0070 | 0.0070 |
| 16 | 0.1531 | 0.1599 | 0.1599 | 0.0162 | 0.0069 | 0.0069 |
| 17 | 0.1619 | 0.1690 | 0.1690 | 0.0160 | 0.0071 | 0.0071 |
| 18 | 0.1706 | 0.1780 | 0.1780 | 0.0161 | 0.0075 | 0.0075 |
| 19 | 0.1792 | 0.1869 | 0.1869 | 0.0164 | 0.0077 | 0.0077 |
| 20 | 0.1879 | 0.1958 | 0.1958 | 0.0166 | 0.0079 | 0.0079 |
| 21 | 0.1967 | 0.2045 | 0.2045 | 0.0166 | 0.0078 | 0.0078 |
| 22 | 0.2054 | 0.2131 | 0.2131 | 0.0164 | 0.0076 | 0.0076 |
| 23 | 0.2141 | 0.2216 | 0.2216 | 0.0162 | 0.0075 | 0.0075 |
| 24 | 0.2226 | 0.2300 | 0.2300 | 0.0159 | 0.0074 | 0.0074 |
| 25 | 0.2309 | 0.2384 | 0.2384 | 0.0158 | 0.0075 | 0.0075 |
| 26 | 0.2389 | 0.2466 | 0.2466 | 0.0158 | 0.0077 | 0.0077 |
| 27 | 0.2470 | 0.2548 | 0.2548 | 0.0158 | 0.0078 | 0.0078 |
| 28 | 0.2551 | 0.2629 | 0.2629 | 0.0159 | 0.0078 | 0.0078 |
| 29 | 0.2630 | 0.2709 | 0.2709 | 0.0158 | 0.0079 | 0.0079 |
| 30 | 0.2708 | 0.2788 | 0.2788 | 0.0158 | 0.0080 | 0.0080 |
| 31 | 0.2794 | 0.3019 | 0.3019 | 0.0312 | 0.0078 | 0.0078 |
| 32 | 0.3164 | 0.3244 | 0.3244 | 0.0303 | 0.0080 | 0.0080 |
| 33 | 0.3381 | 0.3461 | 0.3461 | 0.0297 | 0.0080 | 0.0080 |
| 34 | 0.3598 | 0.3671 | 0.3671 | 0.0290 | 0.0073 | 0.0073 |
| 35 | 0.3801 | 0.3875 | 0.3875 | 0.0276 | 0.0073 | 0.0074 |
| 36 | 0.3997 | 0.4072 | 0.4072 | 0.0270 | 0.0075 | 0.0075 |

TABLA VI-5-A

| Número | continuación.. | | RelA2S1R1 | | Ao1 | Ao2 | DIF-A |
|--------|----------------|---------|-----------|----------|--------|--------|-------|
| | Fe | Fe Teor | Fe | Fe teor2 | | | |
| 37 | 0.4190 | 0.4262 | 0.4262 | 0.0266 | 0.0072 | 0.0073 | |
| 38 | 0.4370 | 0.4447 | 0.4447 | 0.0257 | 0.0077 | 0.0077 | |
| 39 | 0.4545 | 0.4625 | 0.4625 | 0.0255 | 0.0080 | 0.0080 | |
| 40 | 0.4717 | 0.4798 | 0.4798 | 0.0253 | 0.0081 | 0.0081 | |
| 41 | 0.4880 | 0.4965 | 0.4965 | 0.0248 | 0.0085 | 0.0086 | |
| 42 | 0.5038 | 0.5127 | 0.5127 | 0.0247 | 0.0089 | 0.0090 | |
| 43 | 0.5194 | 0.5284 | 0.5284 | 0.0246 | 0.0090 | 0.0090 | |
| 44 | 0.5346 | 0.5435 | 0.5436 | 0.0241 | 0.0090 | 0.0090 | |
| 45 | 0.5496 | 0.5582 | 0.5582 | 0.0236 | 0.0087 | 0.0087 | |
| 46 | 0.5782 | 0.5862 | 0.5862 | 0.0366 | 0.0080 | 0.0080 | |
| 47 | 0.6040 | 0.6123 | 0.6124 | 0.0342 | 0.0084 | 0.0084 | |
| 48 | 0.6264 | 0.6369 | 0.6369 | 0.0329 | 0.0105 | 0.0106 | |
| 49 | 0.6474 | 0.6598 | 0.6599 | 0.0335 | 0.0124 | 0.0125 | |
| 50 | 0.6691 | 0.6814 | 0.6814 | 0.0340 | 0.0123 | 0.0123 | |
| 51 | 0.6890 | 0.7015 | 0.7016 | 0.0324 | 0.0125 | 0.0126 | |
| 52 | 0.7073 | 0.7204 | 0.7205 | 0.0314 | 0.0131 | 0.0132 | |
| 53 | 0.7262 | 0.7381 | 0.7382 | 0.0308 | 0.0119 | 0.0120 | |
| 54 | 0.7427 | 0.7547 | 0.7548 | 0.0285 | 0.0119 | 0.0120 | |
| 55 | 0.7575 | 0.7702 | 0.7703 | 0.0274 | 0.0126 | 0.0127 | |
| 56 | 0.7721 | 0.7847 | 0.7848 | 0.0272 | 0.0126 | 0.0127 | |
| 57 | 0.7856 | 0.7983 | 0.7985 | 0.0262 | 0.0127 | 0.0128 | |
| 58 | 0.7986 | 0.8111 | 0.8112 | 0.0255 | 0.0125 | 0.0126 | |
| 59 | 0.8095 | 0.8231 | 0.8232 | 0.0245 | 0.0135 | 0.0136 | |
| 60 | 0.8185 | 0.8342 | 0.8344 | 0.0247 | 0.0157 | 0.0159 | |
| 61 | 0.8282 | 0.8447 | 0.8449 | 0.0262 | 0.0165 | 0.0167 | |
| 62 | 0.8380 | 0.8546 | 0.8547 | 0.0264 | 0.0166 | 0.0167 | |
| 63 | 0.8469 | 0.8638 | 0.8639 | 0.0258 | 0.0168 | 0.0170 | |
| 64 | 0.8552 | 0.8724 | 0.8725 | 0.0254 | 0.0172 | 0.0173 | |
| 65 | 0.8625 | 0.8804 | 0.8806 | 0.0252 | 0.0179 | 0.0181 | |
| 66 | 0.8691 | 0.8880 | 0.8882 | 0.0255 | 0.0189 | 0.0191 | |
| 67 | 0.8751 | 0.8951 | 0.8952 | 0.0260 | 0.0200 | 0.0201 | |
| 68 | 0.8807 | 0.9017 | 0.9019 | 0.0266 | 0.0210 | 0.0211 | |
| 69 | 0.8861 | 0.9080 | 0.9081 | 0.0272 | 0.0219 | 0.0220 | |
| 70 | 0.8902 | 0.9138 | 0.9139 | 0.0277 | 0.0235 | 0.0237 | |

TABLA VI-6-A

| Número | RelA2SIR3 | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0055 | 0.0108 | 0.0108 | 0.0108 | 0.0054 | 0.0054 |
| 2 | 0.0164 | 0.0215 | 0.0215 | 0.0161 | 0.0052 | 0.0052 |
| 3 | 0.0271 | 0.0321 | 0.0321 | 0.0158 | 0.0050 | 0.0050 |
| 4 | 0.0376 | 0.0426 | 0.0426 | 0.0155 | 0.0051 | 0.0051 |
| 5 | 0.0476 | 0.0530 | 0.0530 | 0.0155 | 0.0054 | 0.0054 |
| 6 | 0.0574 | 0.0633 | 0.0633 | 0.0157 | 0.0059 | 0.0059 |
| 7 | 0.0668 | 0.0734 | 0.0734 | 0.0161 | 0.0066 | 0.0066 |
| 8 | 0.0763 | 0.0835 | 0.0835 | 0.0166 | 0.0071 | 0.0071 |
| 9 | 0.0859 | 0.0934 | 0.0934 | 0.0170 | 0.0075 | 0.0075 |
| 10 | 0.0953 | 0.1032 | 0.1032 | 0.0173 | 0.0079 | 0.0079 |
| 11 | 0.1042 | 0.1129 | 0.1129 | 0.0176 | 0.0087 | 0.0087 |
| 12 | 0.1128 | 0.1225 | 0.1225 | 0.0183 | 0.0098 | 0.0098 |
| 13 | 0.1212 | 0.1320 | 0.1320 | 0.0193 | 0.0108 | 0.0108 |
| 14 | 0.1299 | 0.1414 | 0.1414 | 0.0202 | 0.0116 | 0.0116 |
| 15 | 0.1388 | 0.1507 | 0.1507 | 0.0209 | 0.0119 | 0.0119 |
| 16 | 0.1476 | 0.1599 | 0.1599 | 0.0211 | 0.0123 | 0.0123 |
| 17 | 0.1560 | 0.1690 | 0.1690 | 0.0214 | 0.0131 | 0.0131 |
| 18 | 0.1643 | 0.1780 | 0.1780 | 0.0221 | 0.0138 | 0.0138 |
| 19 | 0.1726 | 0.1869 | 0.1869 | 0.0227 | 0.0143 | 0.0143 |
| 20 | 0.1810 | 0.1958 | 0.1958 | 0.0231 | 0.0148 | 0.0148 |
| 21 | 0.1895 | 0.2045 | 0.2045 | 0.0235 | 0.0150 | 0.0150 |
| 22 | 0.1978 | 0.2131 | 0.2131 | 0.0236 | 0.0153 | 0.0153 |
| 23 | 0.2060 | 0.2216 | 0.2216 | 0.0238 | 0.0156 | 0.0156 |
| 24 | 0.2142 | 0.2300 | 0.2300 | 0.0241 | 0.0159 | 0.0159 |
| 25 | 0.2225 | 0.2384 | 0.2384 | 0.0242 | 0.0159 | 0.0159 |
| 26 | 0.2305 | 0.2466 | 0.2466 | 0.0242 | 0.0161 | 0.0161 |
| 27 | 0.2384 | 0.2548 | 0.2548 | 0.0243 | 0.0164 | 0.0164 |
| 28 | 0.2463 | 0.2629 | 0.2629 | 0.0244 | 0.0165 | 0.0165 |
| 29 | 0.2541 | 0.2709 | 0.2709 | 0.0245 | 0.0168 | 0.0168 |
| 30 | 0.2616 | 0.2788 | 0.2788 | 0.0247 | 0.0172 | 0.0172 |
| 31 | 0.2698 | 0.3019 | 0.3019 | 0.0404 | 0.0181 | 0.0181 |
| 32 | 0.3051 | 0.3244 | 0.3244 | 0.0406 | 0.0193 | 0.0193 |
| 33 | 0.3257 | 0.3461 | 0.3461 | 0.0410 | 0.0204 | 0.0204 |
| 34 | 0.3461 | 0.3671 | 0.3671 | 0.0414 | 0.0210 | 0.0210 |
| 35 | 0.3657 | 0.3875 | 0.3875 | 0.0414 | 0.0218 | 0.0218 |
| 36 | 0.3843 | 0.4072 | 0.4072 | 0.0414 | 0.0229 | 0.0229 |

TABLA VI-6-A
Número

| | continuación.. | | ReIA2SIR2 | Ao1 | Ao2 | DIF-A |
|----|----------------|---------|-----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | | | |
| 37 | 0.4019 | 0.4262 | 0.4262 | 0.0420 | 0.0243 | 0.0243 |
| 38 | 0.4194 | 0.4447 | 0.4447 | 0.0428 | 0.0252 | 0.0253 |
| 39 | 0.4367 | 0.4625 | 0.4625 | 0.0431 | 0.0258 | 0.0258 |
| 40 | 0.4534 | 0.4798 | 0.4798 | 0.0431 | 0.0264 | 0.0265 |
| 41 | 0.4697 | 0.4965 | 0.4965 | 0.0432 | 0.0268 | 0.0268 |
| 42 | 0.4858 | 0.5127 | 0.5127 | 0.0430 | 0.0269 | 0.0269 |
| 43 | 0.5012 | 0.5284 | 0.5284 | 0.0426 | 0.0272 | 0.0272 |
| 44 | 0.5162 | 0.5435 | 0.5436 | 0.0424 | 0.0273 | 0.0273 |
| 45 | 0.5309 | 0.5582 | 0.5582 | 0.0420 | 0.0273 | 0.0274 |
| 46 | 0.5583 | 0.5862 | 0.5862 | 0.0553 | 0.0278 | 0.0279 |
| 47 | 0.5855 | 0.6123 | 0.6124 | 0.0540 | 0.0269 | 0.0269 |
| 48 | 0.6113 | 0.6369 | 0.6369 | 0.0514 | 0.0255 | 0.0256 |
| 49 | 0.6352 | 0.6598 | 0.6599 | 0.0485 | 0.0247 | 0.0247 |
| 50 | 0.6575 | 0.6814 | 0.6814 | 0.0462 | 0.0238 | 0.0239 |
| 51 | 0.6782 | 0.7015 | 0.7016 | 0.0440 | 0.0233 | 0.0234 |
| 52 | 0.6979 | 0.7204 | 0.7205 | 0.0422 | 0.0225 | 0.0226 |
| 53 | 0.7164 | 0.7381 | 0.7382 | 0.0402 | 0.0217 | 0.0218 |
| 54 | 0.7334 | 0.7547 | 0.7548 | 0.0383 | 0.0212 | 0.0213 |
| 55 | 0.7489 | 0.7702 | 0.7703 | 0.0367 | 0.0213 | 0.0214 |
| 56 | 0.7628 | 0.7847 | 0.7848 | 0.0358 | 0.0219 | 0.0220 |
| 57 | 0.7757 | 0.7983 | 0.7985 | 0.0355 | 0.0227 | 0.0228 |
| 58 | 0.7878 | 0.8111 | 0.8112 | 0.0354 | 0.0233 | 0.0235 |
| 59 | 0.7989 | 0.8231 | 0.8232 | 0.0353 | 0.0241 | 0.0243 |
| 60 | 0.8091 | 0.8342 | 0.8344 | 0.0353 | 0.0251 | 0.0253 |
| 61 | 0.8188 | 0.8447 | 0.8449 | 0.0356 | 0.0260 | 0.0261 |
| 62 | 0.8278 | 0.8546 | 0.8547 | 0.0358 | 0.0268 | 0.0269 |
| 63 | 0.8359 | 0.8638 | 0.8639 | 0.0360 | 0.0279 | 0.0280 |
| 64 | 0.8435 | 0.8724 | 0.8725 | 0.0365 | 0.0289 | 0.0291 |
| 65 | 0.8511 | 0.8804 | 0.8806 | 0.0370 | 0.0293 | 0.0295 |
| 66 | 0.8589 | 0.8880 | 0.8882 | 0.0369 | 0.0291 | 0.0293 |
| 67 | 0.8660 | 0.8951 | 0.8952 | 0.0362 | 0.0291 | 0.0292 |
| 68 | 0.8730 | 0.9017 | 0.9019 | 0.0357 | 0.0287 | 0.0288 |
| 69 | 0.8798 | 0.9080 | 0.9081 | 0.0349 | 0.0281 | 0.0283 |
| 70 | 0.8857 | 0.9138 | 0.9139 | 0.0340 | 0.0281 | 0.0283 |

TABLA VI-7-A
Número

RelA2S2R1

| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
|---------|--------|---------|----------|--------|--------|--------|
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0047 | 0.0108 | 0.0108 | 0.0108 | 0.0061 | 0.0061 |
| 2 | 0.0145 | 0.0215 | 0.0215 | 0.0168 | 0.0071 | 0.0071 |
| 3 | 0.0244 | 0.0321 | 0.0321 | 0.0177 | 0.0077 | 0.0077 |
| 4 | 0.0343 | 0.0426 | 0.0426 | 0.0182 | 0.0084 | 0.0084 |
| 5 | 0.0436 | 0.0530 | 0.0530 | 0.0187 | 0.0094 | 0.0094 |
| 6 | 0.0527 | 0.0633 | 0.0633 | 0.0197 | 0.0106 | 0.0106 |
| 7 | 0.0619 | 0.0734 | 0.0734 | 0.0207 | 0.0115 | 0.0115 |
| 8 | 0.0713 | 0.0835 | 0.0835 | 0.0215 | 0.0121 | 0.0121 |
| 9 | 0.0807 | 0.0934 | 0.0934 | 0.0220 | 0.0127 | 0.0127 |
| 10 | 0.0896 | 0.1032 | 0.1032 | 0.0225 | 0.0136 | 0.0136 |
| 11 | 0.0986 | 0.1129 | 0.1129 | 0.0233 | 0.0143 | 0.0143 |
| 12 | 0.1073 | 0.1225 | 0.1225 | 0.0239 | 0.0152 | 0.0152 |
| 13 | 0.1153 | 0.1320 | 0.1320 | 0.0247 | 0.0167 | 0.0167 |
| 14 | 0.1234 | 0.1414 | 0.1414 | 0.0261 | 0.0181 | 0.0181 |
| 15 | 0.1316 | 0.1507 | 0.1507 | 0.0274 | 0.0192 | 0.0192 |
| 16 | 0.1397 | 0.1599 | 0.1599 | 0.0284 | 0.0203 | 0.0203 |
| 17 | 0.1477 | 0.1690 | 0.1690 | 0.0294 | 0.0214 | 0.0214 |
| 18 | 0.1554 | 0.1780 | 0.1780 | 0.0304 | 0.0226 | 0.0226 |
| 19 | 0.1633 | 0.1869 | 0.1869 | 0.0316 | 0.0237 | 0.0237 |
| 20 | 0.1713 | 0.1958 | 0.1958 | 0.0325 | 0.0244 | 0.0244 |
| 21 | 0.1790 | 0.2045 | 0.2045 | 0.0331 | 0.0255 | 0.0255 |
| 22 | 0.1866 | 0.2131 | 0.2131 | 0.0341 | 0.0265 | 0.0265 |
| 23 | 0.1944 | 0.2216 | 0.2216 | 0.0350 | 0.0272 | 0.0272 |
| 24 | 0.2022 | 0.2300 | 0.2300 | 0.0356 | 0.0279 | 0.0279 |
| 25 | 0.2099 | 0.2384 | 0.2384 | 0.0362 | 0.0285 | 0.0285 |
| 26 | 0.2175 | 0.2466 | 0.2466 | 0.0368 | 0.0291 | 0.0291 |
| 27 | 0.2250 | 0.2548 | 0.2548 | 0.0373 | 0.0298 | 0.0298 |
| 28 | 0.2322 | 0.2629 | 0.2629 | 0.0378 | 0.0306 | 0.0306 |
| 29 | 0.2395 | 0.2709 | 0.2709 | 0.0386 | 0.0314 | 0.0314 |
| 30 | 0.2471 | 0.2788 | 0.2788 | 0.0393 | 0.0316 | 0.0316 |
| 31 | 0.2695 | 0.3019 | 0.3019 | 0.0548 | 0.0325 | 0.0325 |
| 32 | 0.2905 | 0.3244 | 0.3244 | 0.0549 | 0.0339 | 0.0339 |
| 33 | 0.3103 | 0.3461 | 0.3461 | 0.0556 | 0.0358 | 0.0359 |
| 34 | 0.3296 | 0.3671 | 0.3671 | 0.0569 | 0.0375 | 0.0375 |
| 35 | 0.3503 | 0.3875 | 0.3875 | 0.0579 | 0.0372 | 0.0372 |
| 36 | 0.3696 | 0.4072 | 0.4072 | 0.0568 | 0.0376 | 0.0376 |

TABLA VI-7-A
Número

continuación... Ref: 252R1

| | Fe | Fe teor | Fe teor2 | A°1 | A°2 | DIF-A |
|----|---------|---------|----------|--------|--------|--------|
| 37 | 0.43872 | 0.4262 | 0.4262 | 0.0566 | 0.0391 | 0.0391 |
| 38 | 0.4049 | 0.4447 | 0.4447 | 0.0575 | 0.0398 | 0.0398 |
| 39 | 0.4216 | 0.4625 | 0.4625 | 0.0577 | 0.0407 | 0.0407 |
| 40 | 0.4353 | 0.4798 | 0.4798 | 0.0580 | 0.0415 | 0.0415 |
| 41 | 0.4526 | 0.4965 | 0.4965 | 0.0582 | 0.0415 | 0.0415 |
| 42 | 0.4715 | 0.5127 | 0.5127 | 0.0577 | 0.0413 | 0.0413 |
| 43 | 0.4871 | 0.5284 | 0.5284 | 0.0569 | 0.0413 | 0.0413 |
| 44 | 0.5015 | 0.5435 | 0.5435 | 0.0565 | 0.0420 | 0.0420 |
| 45 | 0.5156 | 0.5582 | 0.5582 | 0.0567 | 0.0426 | 0.0426 |
| 46 | 0.5433 | 0.5862 | 0.5862 | 0.0706 | 0.0428 | 0.0429 |
| 47 | 0.5569 | 0.6123 | 0.6123 | 0.0690 | 0.0434 | 0.0434 |
| 48 | 0.5930 | 0.6369 | 0.6369 | 0.0679 | 0.0438 | 0.0439 |
| 49 | 0.6167 | 0.6598 | 0.6599 | 0.0668 | 0.0431 | 0.0432 |
| 50 | 0.6387 | 0.6814 | 0.6814 | 0.0647 | 0.0427 | 0.0427 |
| 51 | 0.6590 | 0.7015 | 0.7016 | 0.0628 | 0.0425 | 0.0426 |
| 52 | 0.6790 | 0.7204 | 0.7205 | 0.0614 | 0.0414 | 0.0415 |
| 53 | 0.6976 | 0.7381 | 0.7382 | 0.0591 | 0.0405 | 0.0406 |
| 54 | 0.7145 | 0.7547 | 0.7548 | 0.0570 | 0.0402 | 0.0403 |
| 55 | 0.7307 | 0.7702 | 0.7703 | 0.0557 | 0.0395 | 0.0396 |
| 56 | 0.7460 | 0.7847 | 0.7848 | 0.0540 | 0.0387 | 0.0388 |
| 57 | 0.7610 | 0.7983 | 0.7985 | 0.0523 | 0.0374 | 0.0375 |
| 58 | 0.7756 | 0.8111 | 0.8112 | 0.0501 | 0.0355 | 0.0356 |
| 59 | 0.7889 | 0.8231 | 0.8232 | 0.0474 | 0.0342 | 0.0343 |
| 60 | 0.8015 | 0.8342 | 0.8344 | 0.0454 | 0.0327 | 0.0329 |
| 61 | 0.8146 | 0.8447 | 0.8449 | 0.0432 | 0.0307 | 0.0308 |
| 62 | 0.8267 | 0.8546 | 0.8547 | 0.0405 | 0.0289 | 0.0290 |
| 63 | 0.8382 | 0.8638 | 0.8639 | 0.0381 | 0.0275 | 0.0277 |
| 64 | 0.8459 | 0.8724 | 0.8725 | 0.0362 | 0.0265 | 0.0266 |
| 65 | 0.8533 | 0.8804 | 0.8806 | 0.0345 | 0.0251 | 0.0253 |
| 66 | 0.8600 | 0.8880 | 0.8882 | 0.0327 | 0.0240 | 0.0241 |
| 67 | 0.8724 | 0.8951 | 0.8952 | 0.0311 | 0.0227 | 0.0228 |
| 68 | 0.8807 | 0.9017 | 0.9019 | 0.0293 | 0.0210 | 0.0212 |
| 69 | 0.8886 | 0.9060 | 0.9081 | 0.0272 | 0.0194 | 0.0195 |
| 70 | 0.8950 | 0.9138 | 0.9139 | 0.0252 | 0.0187 | 0.0189 |

FABLA VI-B-A
Número

RelAZS2R2

| | Fa | Fa teor | Fa teor 2 | A*1 | A*2 | DIF-A |
|---------|--------|---------|-----------|--------|--------|--------|
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0045 | 0.0102 | 0.0102 | 0.0102 | 0.0063 | 0.0063 |
| 2 | 0.0134 | 0.0215 | 0.0215 | 0.0170 | 0.0082 | 0.0082 |
| 3 | 0.0225 | 0.0321 | 0.0321 | 0.0188 | 0.0096 | 0.0096 |
| 4 | 0.0317 | 0.0426 | 0.0426 | 0.0201 | 0.0109 | 0.0109 |
| 5 | 0.0407 | 0.0530 | 0.0530 | 0.0213 | 0.0124 | 0.0124 |
| 6 | 0.0498 | 0.0633 | 0.0633 | 0.0226 | 0.0135 | 0.0135 |
| 7 | 0.0589 | 0.0734 | 0.0734 | 0.0236 | 0.0145 | 0.0145 |
| 8 | 0.0675 | 0.0835 | 0.0835 | 0.0245 | 0.0159 | 0.0159 |
| 9 | 0.0760 | 0.0934 | 0.0934 | 0.0258 | 0.0173 | 0.0173 |
| 10 | 0.0849 | 0.1032 | 0.1032 | 0.0272 | 0.0183 | 0.0183 |
| 11 | 0.0936 | 0.1129 | 0.1129 | 0.0281 | 0.0193 | 0.0193 |
| 12 | 0.1021 | 0.1225 | 0.1225 | 0.0289 | 0.0204 | 0.0204 |
| 13 | 0.1102 | 0.1320 | 0.1320 | 0.0299 | 0.0218 | 0.0218 |
| 14 | 0.1184 | 0.1414 | 0.1414 | 0.0312 | 0.0230 | 0.0230 |
| 15 | 0.1267 | 0.1507 | 0.1507 | 0.0323 | 0.0240 | 0.0240 |
| 16 | 0.1350 | 0.1599 | 0.1599 | 0.0332 | 0.0250 | 0.0250 |
| 17 | 0.1434 | 0.1690 | 0.1690 | 0.0341 | 0.0257 | 0.0257 |
| 18 | 0.1516 | 0.1780 | 0.1780 | 0.0347 | 0.0264 | 0.0264 |
| 19 | 0.1596 | 0.1869 | 0.1869 | 0.0353 | 0.0273 | 0.0273 |
| 20 | 0.1675 | 0.1958 | 0.1958 | 0.0361 | 0.0282 | 0.0282 |
| 21 | 0.1752 | 0.2045 | 0.2045 | 0.0369 | 0.0293 | 0.0293 |
| 22 | 0.1827 | 0.2131 | 0.2131 | 0.0379 | 0.0303 | 0.0303 |
| 23 | 0.1906 | 0.2216 | 0.2216 | 0.0389 | 0.0310 | 0.0310 |
| 24 | 0.1983 | 0.2300 | 0.2300 | 0.0394 | 0.0317 | 0.0317 |
| 25 | 0.2061 | 0.2384 | 0.2384 | 0.0400 | 0.0323 | 0.0323 |
| 26 | 0.2139 | 0.2466 | 0.2466 | 0.0405 | 0.0327 | 0.0327 |
| 27 | 0.2215 | 0.2548 | 0.2548 | 0.0409 | 0.0332 | 0.0333 |
| 28 | 0.2291 | 0.2629 | 0.2629 | 0.0413 | 0.0338 | 0.0338 |
| 29 | 0.2361 | 0.2709 | 0.2709 | 0.0418 | 0.0347 | 0.0347 |
| 30 | 0.2430 | 0.2788 | 0.2788 | 0.0426 | 0.0358 | 0.0358 |
| 31 | 0.2505 | 0.2869 | 0.2869 | 0.0589 | 0.0384 | 0.0384 |
| 32 | 0.2576 | 0.2944 | 0.2944 | 0.0407 | 0.0407 | 0.0408 |
| 33 | 0.2655 | 0.3021 | 0.3021 | 0.0425 | 0.0426 | 0.0427 |
| 34 | 0.2728 | 0.3071 | 0.3071 | 0.0437 | 0.0443 | 0.0443 |
| 35 | 0.2810 | 0.3075 | 0.3075 | 0.0447 | 0.0457 | 0.0457 |
| 36 | 0.2801 | 0.4072 | 0.4072 | 0.0654 | 0.0471 | 0.0471 |

TABLA VI-8-A
Número

| | continuación.. | | Re1A2S2R2 | | Ao1 | Ao2 | DIF-A |
|----|----------------|---------|-----------|--------|--------|--------|-------|
| | Fø | Fø teor | Fø | teor2 | | | |
| 37 | 0.3782 | 0.4262 | 0.4262 | 0.0662 | 0.0480 | 0.0481 | |
| 38 | 0.3962 | 0.4447 | 0.4447 | 0.0665 | 0.0485 | 0.0485 | |
| 39 | 0.4148 | 0.4625 | 0.4625 | 0.0663 | 0.0477 | 0.0477 | |
| 40 | 0.4327 | 0.4798 | 0.4798 | 0.0650 | 0.0471 | 0.0471 | |
| 41 | 0.4486 | 0.4965 | 0.4965 | 0.0638 | 0.0480 | 0.0480 | |
| 42 | 0.4636 | 0.5127 | 0.5127 | 0.0642 | 0.0491 | 0.0492 | |
| 43 | 0.4783 | 0.5284 | 0.5284 | 0.0648 | 0.0501 | 0.0501 | |
| 44 | 0.4934 | 0.5435 | 0.5436 | 0.0652 | 0.0501 | 0.0501 | |
| 45 | 0.5084 | 0.5582 | 0.5582 | 0.0648 | 0.0498 | 0.0498 | |
| 46 | 0.5372 | 0.5862 | 0.5862 | 0.0778 | 0.0490 | 0.0490 | |
| 47 | 0.5644 | 0.6123 | 0.6124 | 0.0751 | 0.0480 | 0.0480 | |
| 48 | 0.5900 | 0.6369 | 0.6369 | 0.0725 | 0.0469 | 0.0469 | |
| 49 | 0.6145 | 0.6598 | 0.6599 | 0.0698 | 0.0453 | 0.0454 | |
| 50 | 0.6370 | 0.6814 | 0.6814 | 0.0669 | 0.0443 | 0.0444 | |
| 51 | 0.6576 | 0.7015 | 0.7016 | 0.0645 | 0.0439 | 0.0440 | |
| 52 | 0.6770 | 0.7204 | 0.7205 | 0.0628 | 0.0434 | 0.0435 | |
| 53 | 0.6952 | 0.7381 | 0.7382 | 0.0611 | 0.0429 | 0.0430 | |
| 54 | 0.7123 | 0.7547 | 0.7548 | 0.0594 | 0.0423 | 0.0424 | |
| 55 | 0.7277 | 0.7702 | 0.7703 | 0.0579 | 0.0424 | 0.0425 | |
| 56 | 0.7426 | 0.7847 | 0.7848 | 0.0570 | 0.0421 | 0.0422 | |
| 57 | 0.7572 | 0.7983 | 0.7985 | 0.0558 | 0.0411 | 0.0412 | |
| 58 | 0.7708 | 0.8111 | 0.8112 | 0.0539 | 0.0403 | 0.0404 | |
| 59 | 0.7836 | 0.8231 | 0.8232 | 0.0523 | 0.0394 | 0.0396 | |
| 60 | 0.7959 | 0.8342 | 0.8344 | 0.0506 | 0.0383 | 0.0384 | |
| 61 | 0.8074 | 0.8447 | 0.8449 | 0.0488 | 0.0373 | 0.0374 | |
| 62 | 0.8178 | 0.8546 | 0.8547 | 0.0471 | 0.0368 | 0.0369 | |
| 63 | 0.8282 | 0.8638 | 0.8639 | 0.0460 | 0.0356 | 0.0357 | |
| 64 | 0.8380 | 0.8724 | 0.8725 | 0.0442 | 0.0344 | 0.0345 | |
| 65 | 0.8461 | 0.8804 | 0.8806 | 0.0425 | 0.0344 | 0.0345 | |
| 66 | 0.8538 | 0.8880 | 0.8882 | 0.0420 | 0.0342 | 0.0344 | |
| 67 | 0.8617 | 0.8951 | 0.8952 | 0.0413 | 0.0334 | 0.0335 | |
| 68 | 0.8692 | 0.9017 | 0.9019 | 0.0400 | 0.0325 | 0.0326 | |
| 69 | 0.8766 | 0.9080 | 0.9081 | 0.0387 | 0.0313 | 0.0315 | |
| 70 | 0.8819 | 0.9138 | 0.9139 | 0.0371 | 0.0319 | 0.0320 | |

TABLA VI-9-A

| Número | F ₀ | F ₀ Teor | Re2A1S1R1 F ₀ teor2 | A ₀₁ | A ₀₂ | DIF-A |
|---------|----------------|---------------------|-----------------------------------|-----------------|-----------------|--------|
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0120 | 0.0108 | 0.0108 | 0.0108 | 0.0012 | 0.0012 |
| 2 | 0.0237 | 0.0215 | 0.0215 | 0.0095 | 0.0021 | 0.0021 |
| 3 | 0.0349 | 0.0321 | 0.0321 | 0.0085 | 0.0028 | 0.0028 |
| 4 | 0.0462 | 0.0426 | 0.0426 | 0.0077 | 0.0036 | 0.0036 |
| 5 | 0.0575 | 0.0530 | 0.0530 | 0.0068 | 0.0045 | 0.0045 |
| 6 | 0.0686 | 0.0633 | 0.0633 | 0.0058 | 0.0053 | 0.0053 |
| 7 | 0.0795 | 0.0734 | 0.0734 | 0.0048 | 0.0061 | 0.0061 |
| 8 | 0.0903 | 0.0835 | 0.0835 | 0.0039 | 0.0068 | 0.0068 |
| 9 | 0.1008 | 0.0934 | 0.0934 | 0.0031 | 0.0074 | 0.0074 |
| 10 | 0.1113 | 0.1032 | 0.1032 | 0.0024 | 0.0081 | 0.0081 |
| 11 | 0.1220 | 0.1129 | 0.1129 | 0.0017 | 0.0091 | 0.0091 |
| 12 | 0.1326 | 0.1225 | 0.1225 | 0.0005 | 0.0101 | 0.0100 |
| 13 | 0.1431 | 0.1320 | 0.1320 | 0.0005 | 0.0111 | 0.0111 |
| 14 | 0.1536 | 0.1414 | 0.1414 | 0.0017 | 0.0122 | 0.0122 |
| 15 | 0.1639 | 0.1507 | 0.1507 | 0.0029 | 0.0131 | 0.0131 |
| 16 | 0.1740 | 0.1599 | 0.1599 | 0.0039 | 0.0140 | 0.0140 |
| 17 | 0.1840 | 0.1690 | 0.1690 | 0.0049 | 0.0149 | 0.0149 |
| 18 | 0.1939 | 0.1780 | 0.1780 | 0.0059 | 0.0158 | 0.0158 |
| 19 | 0.2038 | 0.1869 | 0.1869 | 0.0069 | 0.0169 | 0.0169 |
| 20 | 0.2137 | 0.1958 | 0.1958 | 0.0080 | 0.0179 | 0.0179 |
| 21 | 0.2234 | 0.2045 | 0.2045 | 0.0092 | 0.0189 | 0.0189 |
| 22 | 0.2329 | 0.2131 | 0.2131 | 0.0103 | 0.0199 | 0.0199 |
| 23 | 0.2426 | 0.2216 | 0.2216 | 0.0113 | 0.0210 | 0.0210 |
| 24 | 0.2521 | 0.2300 | 0.2300 | 0.0125 | 0.0220 | 0.0220 |
| 25 | 0.2615 | 0.2384 | 0.2384 | 0.0137 | 0.0231 | 0.0231 |
| 26 | 0.2705 | 0.2466 | 0.2466 | 0.0149 | 0.0239 | 0.0239 |
| 27 | 0.2790 | 0.2548 | 0.2548 | 0.0157 | 0.0242 | 0.0242 |
| 28 | 0.2875 | 0.2629 | 0.2629 | 0.0162 | 0.0246 | 0.0246 |
| 29 | 0.2957 | 0.2709 | 0.2709 | 0.0166 | 0.0248 | 0.0248 |
| 30 | 0.3035 | 0.2788 | 0.2788 | 0.0169 | 0.0248 | 0.0247 |
| 31 | 0.3264 | 0.3019 | 0.3019 | 0.0016 | 0.0245 | 0.0245 |
| 32 | 0.3489 | 0.3244 | 0.3244 | 0.0020 | 0.0245 | 0.0245 |
| 33 | 0.3710 | 0.3461 | 0.3461 | 0.0028 | 0.0249 | 0.0249 |
| 34 | 0.3926 | 0.3671 | 0.3671 | 0.0039 | 0.0255 | 0.0255 |
| 35 | 0.4132 | 0.3875 | 0.3875 | 0.0051 | 0.0257 | 0.0257 |
| 36 | 0.4326 | 0.4072 | 0.4072 | 0.0060 | 0.0254 | 0.0254 |

TABLA VI-9-A
Número

| | continuación.. | | Re2A1S1R1 | Ao1 | Ao2 | DIF-A |
|----|----------------|---------|-----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | | | |
| 37 | 0.4513 | 0.4262 | 0.4262 | 0.0064 | 0.0251 | 0.0251 |
| 38 | 0.4691 | 0.4447 | 0.4447 | 0.0067 | 0.0245 | 0.0245 |
| 39 | 0.4865 | 0.4625 | 0.4625 | 0.0066 | 0.0239 | 0.0239 |
| 40 | 0.5036 | 0.4798 | 0.4798 | 0.0067 | 0.0238 | 0.0238 |
| 41 | 0.5199 | 0.4965 | 0.4965 | 0.0071 | 0.0233 | 0.0233 |
| 42 | 0.5356 | 0.5127 | 0.5127 | 0.0072 | 0.0229 | 0.0229 |
| 43 | 0.5512 | 0.5284 | 0.5284 | 0.0073 | 0.0228 | 0.0228 |
| 44 | 0.5659 | 0.5435 | 0.5436 | 0.0076 | 0.0224 | 0.0223 |
| 45 | 0.5801 | 0.5582 | 0.5582 | 0.0077 | 0.0219 | 0.0219 |
| 46 | 0.6075 | 0.5862 | 0.5862 | 0.0061 | 0.0213 | 0.0213 |
| 47 | 0.6330 | 0.6123 | 0.6124 | 0.0048 | 0.0206 | 0.0206 |
| 48 | 0.6557 | 0.6369 | 0.6369 | 0.0039 | 0.0189 | 0.0188 |
| 49 | 0.6761 | 0.6598 | 0.6599 | 0.0041 | 0.0163 | 0.0162 |
| 50 | 0.6957 | 0.6814 | 0.6814 | 0.0052 | 0.0143 | 0.0143 |
| 51 | 0.7148 | 0.7015 | 0.7016 | 0.0058 | 0.0133 | 0.0132 |
| 52 | 0.7328 | 0.7204 | 0.7205 | 0.0056 | 0.0124 | 0.0123 |
| 53 | 0.7495 | 0.7381 | 0.7382 | 0.0053 | 0.0114 | 0.0114 |
| 54 | 0.7655 | 0.7547 | 0.7548 | 0.0051 | 0.0109 | 0.0108 |
| 55 | 0.7797 | 0.7702 | 0.7703 | 0.0047 | 0.0095 | 0.0094 |
| 56 | 0.7929 | 0.7847 | 0.7848 | 0.0051 | 0.0081 | 0.0080 |
| 57 | 0.8059 | 0.7983 | 0.7985 | 0.0055 | 0.0076 | 0.0075 |
| 58 | 0.8183 | 0.8111 | 0.8112 | 0.0052 | 0.0072 | 0.0071 |
| 59 | 0.8293 | 0.8231 | 0.8232 | 0.0047 | 0.0063 | 0.0062 |
| 60 | 0.8391 | 0.8342 | 0.8344 | 0.0049 | 0.0048 | 0.0047 |
| 61 | 0.8485 | 0.8447 | 0.8449 | 0.0056 | 0.0038 | 0.0037 |
| 62 | 0.8576 | 0.8546 | 0.8547 | 0.0060 | 0.0031 | 0.0029 |
| 63 | 0.8662 | 0.8638 | 0.8639 | 0.0061 | 0.0024 | 0.0023 |
| 64 | 0.8740 | 0.8724 | 0.8725 | 0.0062 | 0.0017 | 0.0015 |
| 65 | 0.8813 | 0.8804 | 0.8806 | 0.0064 | 0.0009 | 0.0008 |
| 66 | 0.8878 | 0.8880 | 0.8882 | 0.0067 | 0.0002 | 0.0004 |
| 67 | 0.8923 | 0.8951 | 0.8952 | 0.0073 | 0.0028 | 0.0029 |
| 68 | 0.8966 | 0.9017 | 0.9019 | 0.0094 | 0.0051 | 0.0053 |
| 69 | 0.9017 | 0.9080 | 0.9081 | 0.0113 | 0.0062 | 0.0064 |
| 70 | 0.9065 | 0.9138 | 0.9139 | 0.0120 | 0.0073 | 0.0075 |

TABLA VI-10-A

| Número | Re2A1S1R2 | | | A01 | A02 | DIF-A |
|---------|-----------|---------|----------|--------|--------|--------|
| | F0 | F0 Teor | F0 teor2 | | | |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0060 | 0.0108 | 0.0108 | 0.0108 | 0.0048 | 0.0048 |
| 2 | 0.0177 | 0.0215 | 0.0215 | 0.0155 | 0.0039 | 0.0039 |
| 3 | 0.0289 | 0.0321 | 0.0321 | 0.0145 | 0.0032 | 0.0032 |
| 4 | 0.0402 | 0.0426 | 0.0426 | 0.0137 | 0.0025 | 0.0025 |
| 5 | 0.0515 | 0.0530 | 0.0530 | 0.0128 | 0.0015 | 0.0015 |
| 6 | 0.0626 | 0.0633 | 0.0633 | 0.0118 | 0.0007 | 0.0007 |
| 7 | 0.0735 | 0.0734 | 0.0734 | 0.0108 | 0.0001 | 0.0001 |
| 8 | 0.0843 | 0.0835 | 0.0835 | 0.0100 | 0.0008 | 0.0008 |
| 9 | 0.0947 | 0.0934 | 0.0934 | 0.0091 | 0.0014 | 0.0014 |
| 10 | 0.1053 | 0.1032 | 0.1032 | 0.0085 | 0.0021 | 0.0021 |
| 11 | 0.1160 | 0.1129 | 0.1129 | 0.0077 | 0.0031 | 0.0031 |
| 12 | 0.1264 | 0.1225 | 0.1225 | 0.0065 | 0.0039 | 0.0039 |
| 13 | 0.1367 | 0.1320 | 0.1320 | 0.0056 | 0.0047 | 0.0047 |
| 14 | 0.1471 | 0.1414 | 0.1414 | 0.0047 | 0.0056 | 0.0056 |
| 15 | 0.1575 | 0.1507 | 0.1507 | 0.0037 | 0.0067 | 0.0067 |
| 16 | 0.1677 | 0.1599 | 0.1599 | 0.0025 | 0.0078 | 0.0078 |
| 17 | 0.1777 | 0.1690 | 0.1690 | 0.0013 | 0.0086 | 0.0086 |
| 18 | 0.1876 | 0.1780 | 0.1780 | 0.0004 | 0.0095 | 0.0095 |
| 19 | 0.1975 | 0.1869 | 0.1869 | 0.0006 | 0.0106 | 0.0106 |
| 20 | 0.2074 | 0.1958 | 0.1958 | 0.0018 | 0.0116 | 0.0116 |
| 21 | 0.2171 | 0.2045 | 0.2045 | 0.0029 | 0.0126 | 0.0126 |
| 22 | 0.2267 | 0.2131 | 0.2131 | 0.0040 | 0.0136 | 0.0136 |
| 23 | 0.2363 | 0.2216 | 0.2216 | 0.0050 | 0.0147 | 0.0147 |
| 24 | 0.2458 | 0.2300 | 0.2300 | 0.0062 | 0.0157 | 0.0157 |
| 25 | 0.2552 | 0.2384 | 0.2384 | 0.0074 | 0.0168 | 0.0168 |
| 26 | 0.2642 | 0.2466 | 0.2466 | 0.0086 | 0.0176 | 0.0176 |
| 27 | 0.2730 | 0.2548 | 0.2548 | 0.0094 | 0.0182 | 0.0182 |
| 28 | 0.2819 | 0.2629 | 0.2629 | 0.0101 | 0.0190 | 0.0190 |
| 29 | 0.2906 | 0.2709 | 0.2709 | 0.0110 | 0.0198 | 0.0197 |
| 30 | 0.2989 | 0.2788 | 0.2788 | 0.0119 | 0.0201 | 0.0201 |
| 31 | 0.3227 | 0.3019 | 0.3019 | 0.0031 | 0.0208 | 0.0208 |
| 32 | 0.3451 | 0.3244 | 0.3244 | 0.0017 | 0.0207 | 0.0207 |
| 33 | 0.3664 | 0.3461 | 0.3461 | 0.0010 | 0.0203 | 0.0203 |
| 34 | 0.3870 | 0.3671 | 0.3671 | 0.0007 | 0.0199 | 0.0199 |
| 35 | 0.4069 | 0.3875 | 0.3875 | 0.0005 | 0.0195 | 0.0195 |
| 36 | 0.4263 | 0.4072 | 0.4072 | 0.0002 | 0.0192 | 0.0192 |

TABLA VI-10-A
Número

continuación.. Re2A1S1R2
Fe Fe Teor Fe teor2

Ao1 Ao2 DIF-A

| | | | | | | |
|----|--------|--------|--------|--------|--------|--------|
| 37 | 0.4444 | 0.4262 | 0.4262 | 0.0001 | 0.0182 | 0.0182 |
| 38 | 0.4616 | 0.4447 | 0.4447 | 0.0002 | 0.0169 | 0.0169 |
| 39 | 0.4784 | 0.4625 | 0.4625 | 0.0010 | 0.0158 | 0.0158 |
| 40 | 0.4947 | 0.4798 | 0.4798 | 0.0014 | 0.0149 | 0.0149 |
| 41 | 0.5110 | 0.4965 | 0.4965 | 0.0018 | 0.0144 | 0.0144 |
| 42 | 0.5265 | 0.5127 | 0.5127 | 0.0018 | 0.0138 | 0.0138 |
| 43 | 0.5416 | 0.5284 | 0.5284 | 0.0018 | 0.0132 | 0.0132 |
| 44 | 0.5563 | 0.5435 | 0.5436 | 0.0020 | 0.0128 | 0.0127 |
| 45 | 0.5703 | 0.5582 | 0.5582 | 0.0019 | 0.0121 | 0.0121 |
| 46 | 0.5974 | 0.5862 | 0.5862 | 0.0158 | 0.0112 | 0.0112 |
| 47 | 0.6228 | 0.6123 | 0.6124 | 0.0150 | 0.0105 | 0.0104 |
| 48 | 0.6473 | 0.6369 | 0.6369 | 0.0141 | 0.0105 | 0.0104 |
| 49 | 0.6706 | 0.6598 | 0.6599 | 0.0125 | 0.0107 | 0.0107 |
| 50 | 0.6910 | 0.6814 | 0.6814 | 0.0108 | 0.0097 | 0.0096 |
| 51 | 0.7099 | 0.7015 | 0.7016 | 0.0105 | 0.0084 | 0.0083 |
| 52 | 0.7281 | 0.7204 | 0.7205 | 0.0105 | 0.0077 | 0.0076 |
| 53 | 0.7442 | 0.7381 | 0.7382 | 0.0100 | 0.0061 | 0.0060 |
| 54 | 0.7586 | 0.7547 | 0.7548 | 0.0105 | 0.0039 | 0.0038 |
| 55 | 0.7734 | 0.7702 | 0.7703 | 0.0116 | 0.0032 | 0.0031 |
| 56 | 0.7878 | 0.7847 | 0.7848 | 0.0114 | 0.0031 | 0.0030 |
| 57 | 0.8017 | 0.7983 | 0.7985 | 0.0106 | 0.0033 | 0.0032 |
| 58 | 0.8153 | 0.8111 | 0.8112 | 0.0094 | 0.0042 | 0.0041 |
| 59 | 0.8281 | 0.8231 | 0.8232 | 0.0077 | 0.0051 | 0.0050 |
| 60 | 0.8403 | 0.8342 | 0.8344 | 0.0061 | 0.0060 | 0.0059 |
| 61 | 0.8515 | 0.8447 | 0.8449 | 0.0045 | 0.0068 | 0.0067 |
| 62 | 0.8617 | 0.8546 | 0.8547 | 0.0030 | 0.0071 | 0.0070 |
| 63 | 0.8711 | 0.8638 | 0.8639 | 0.0021 | 0.0074 | 0.0072 |
| 64 | 0.8788 | 0.8724 | 0.8725 | 0.0012 | 0.0065 | 0.0063 |
| 65 | 0.8849 | 0.8804 | 0.8806 | 0.0016 | 0.0044 | 0.0043 |
| 66 | 0.8902 | 0.8880 | 0.8882 | 0.0031 | 0.0022 | 0.0021 |
| 67 | 0.8956 | 0.8951 | 0.8952 | 0.0049 | 0.0005 | 0.0003 |
| 68 | 0.9008 | 0.9017 | 0.9019 | 0.0062 | 0.0009 | 0.0011 |
| 69 | 0.9053 | 0.9080 | 0.9081 | 0.0071 | 0.0026 | 0.0028 |
| 70 | 0.9087 | 0.9138 | 0.9139 | 0.0085 | 0.0050 | 0.0052 |

TABLA VI-11-A

| Número | Re2A1S2R1 | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0059 | 0.0108 | 0.0108 | 0.0108 | 0.0050 | 0.0050 |
| 2 | 0.0175 | 0.0215 | 0.0215 | 0.0157 | 0.0040 | 0.0040 |
| 3 | 0.0290 | 0.0321 | 0.0321 | 0.0146 | 0.0031 | 0.0031 |
| 4 | 0.0405 | 0.0426 | 0.0426 | 0.0136 | 0.0021 | 0.0021 |
| 5 | 0.0520 | 0.0530 | 0.0530 | 0.0125 | 0.0010 | 0.0010 |
| 6 | 0.0635 | 0.0633 | 0.0633 | 0.0112 | 0.0002 | 0.0002 |
| 7 | 0.0744 | 0.0734 | 0.0734 | 0.0099 | 0.0010 | 0.0010 |
| 8 | 0.0851 | 0.0835 | 0.0835 | 0.0091 | 0.0017 | 0.0017 |
| 9 | 0.0963 | 0.0934 | 0.0934 | 0.0083 | 0.0030 | 0.0029 |
| 10 | 0.1073 | 0.1032 | 0.1032 | 0.0069 | 0.0041 | 0.0041 |
| 11 | 0.1179 | 0.1129 | 0.1129 | 0.0056 | 0.0050 | 0.0050 |
| 12 | 0.1278 | 0.1225 | 0.1225 | 0.0046 | 0.0053 | 0.0053 |
| 13 | 0.1376 | 0.1320 | 0.1320 | 0.0042 | 0.0056 | 0.0056 |
| 14 | 0.1476 | 0.1414 | 0.1414 | 0.0038 | 0.0062 | 0.0062 |
| 15 | 0.1572 | 0.1507 | 0.1507 | 0.0031 | 0.0065 | 0.0065 |
| 16 | 0.1668 | 0.1599 | 0.1599 | 0.0027 | 0.0069 | 0.0069 |
| 17 | 0.1766 | 0.1690 | 0.1690 | 0.0022 | 0.0076 | 0.0076 |
| 18 | 0.1860 | 0.1780 | 0.1780 | 0.0014 | 0.0080 | 0.0080 |
| 19 | 0.1955 | 0.1869 | 0.1869 | 0.0009 | 0.0086 | 0.0086 |
| 20 | 0.2050 | 0.1958 | 0.1958 | 0.0002 | 0.0093 | 0.0093 |
| 21 | 0.2144 | 0.2045 | 0.2045 | 0.0006 | 0.0099 | 0.0099 |
| 22 | 0.2236 | 0.2131 | 0.2131 | 0.0013 | 0.0105 | 0.0105 |
| 23 | 0.2327 | 0.2216 | 0.2216 | 0.0020 | 0.0110 | 0.0110 |
| 24 | 0.2416 | 0.2300 | 0.2300 | 0.0026 | 0.0116 | 0.0116 |
| 25 | 0.2504 | 0.2384 | 0.2384 | 0.0033 | 0.0121 | 0.0121 |
| 26 | 0.2591 | 0.2466 | 0.2466 | 0.0038 | 0.0124 | 0.0124 |
| 27 | 0.2677 | 0.2548 | 0.2548 | 0.0043 | 0.0129 | 0.0129 |
| 28 | 0.2760 | 0.2629 | 0.2629 | 0.0048 | 0.0132 | 0.0132 |
| 29 | 0.2840 | 0.2709 | 0.2709 | 0.0052 | 0.0132 | 0.0132 |
| 30 | 0.2920 | 0.2788 | 0.2788 | 0.0053 | 0.0132 | 0.0132 |
| 31 | 0.3156 | 0.3019 | 0.3019 | 0.0100 | 0.0137 | 0.0137 |
| 32 | 0.3386 | 0.3244 | 0.3244 | 0.0088 | 0.0142 | 0.0142 |
| 33 | 0.3609 | 0.3461 | 0.3461 | 0.0075 | 0.0148 | 0.0147 |
| 34 | 0.3824 | 0.3671 | 0.3671 | 0.0063 | 0.0153 | 0.0153 |
| 35 | 0.4030 | 0.3875 | 0.3875 | 0.0051 | 0.0155 | 0.0155 |
| 36 | 0.4227 | 0.4072 | 0.4072 | 0.0042 | 0.0155 | 0.0155 |

TABLA VI-11-A
Número

continuación.. Re2AlS2R1
Fe Fe Teor Fe teor2

| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
|----|--------|---------|----------|--------|--------|--------|
| 37 | 0.4417 | 0.4262 | 0.4262 | 0.0036 | 0.0155 | 0.0155 |
| 38 | 0.4604 | 0.4447 | 0.4447 | 0.0030 | 0.0157 | 0.0157 |
| 39 | 0.4781 | 0.4625 | 0.4625 | 0.0021 | 0.0156 | 0.0156 |
| 40 | 0.4953 | 0.4798 | 0.4798 | 0.0017 | 0.0155 | 0.0155 |
| 41 | 0.5123 | 0.4965 | 0.4965 | 0.0012 | 0.0158 | 0.0158 |
| 42 | 0.5285 | 0.5127 | 0.5127 | 0.0004 | 0.0158 | 0.0158 |
| 43 | 0.5437 | 0.5284 | 0.5284 | 0.0002 | 0.0153 | 0.0153 |
| 44 | 0.5583 | 0.5435 | 0.5436 | 0.0002 | 0.0148 | 0.0148 |
| 45 | 0.5721 | 0.5582 | 0.5582 | 0.0001 | 0.0139 | 0.0139 |
| 46 | 0.5977 | 0.5862 | 0.5862 | 0.0141 | 0.0115 | 0.0115 |
| 47 | 0.6226 | 0.6123 | 0.6124 | 0.0147 | 0.0103 | 0.0102 |
| 48 | 0.6462 | 0.6369 | 0.6369 | 0.0143 | 0.0093 | 0.0093 |
| 49 | 0.6686 | 0.6598 | 0.6599 | 0.0136 | 0.0088 | 0.0087 |
| 50 | 0.6895 | 0.6814 | 0.6814 | 0.0128 | 0.0081 | 0.0080 |
| 51 | 0.7084 | 0.7015 | 0.7016 | 0.0120 | 0.0069 | 0.0068 |
| 52 | 0.7261 | 0.7204 | 0.7205 | 0.0120 | 0.0056 | 0.0056 |
| 53 | 0.7430 | 0.7381 | 0.7382 | 0.0120 | 0.0049 | 0.0048 |
| 54 | 0.7589 | 0.7547 | 0.7548 | 0.0116 | 0.0043 | 0.0042 |
| 55 | 0.7725 | 0.7702 | 0.7703 | 0.0112 | 0.0023 | 0.0022 |
| 56 | 0.7850 | 0.7847 | 0.7848 | 0.0122 | 0.0003 | 0.0002 |
| 57 | 0.7975 | 0.7983 | 0.7985 | 0.0133 | 0.0008 | 0.0010 |
| 58 | 0.8102 | 0.8111 | 0.8112 | 0.0136 | 0.0009 | 0.0010 |
| 59 | 0.8229 | 0.8231 | 0.8232 | 0.0129 | 0.0002 | 0.0003 |
| 60 | 0.8346 | 0.8342 | 0.8344 | 0.0114 | 0.0003 | 0.0002 |
| 61 | 0.8461 | 0.8447 | 0.8449 | 0.0101 | 0.0014 | 0.0013 |
| 62 | 0.8570 | 0.8546 | 0.8547 | 0.0084 | 0.0024 | 0.0023 |
| 63 | 0.8661 | 0.8638 | 0.8639 | 0.0068 | 0.0024 | 0.0022 |
| 64 | 0.8736 | 0.8724 | 0.8725 | 0.0062 | 0.0012 | 0.0011 |
| 65 | 0.8808 | 0.8804 | 0.8806 | 0.0068 | 0.0003 | 0.0002 |
| 66 | 0.8878 | 0.8880 | 0.8882 | 0.0073 | 0.0003 | 0.0004 |
| 67 | 0.8941 | 0.8951 | 0.8952 | 0.0073 | 0.0010 | 0.0012 |
| 68 | 0.9005 | 0.9017 | 0.9019 | 0.0077 | 0.0013 | 0.0014 |
| 69 | 0.9069 | 0.9080 | 0.9081 | 0.0075 | 0.0010 | 0.0012 |
| 70 | 0.9121 | 0.9138 | 0.9139 | 0.0068 | 0.0017 | 0.0018 |

TABLA VI-12-A

| Número | Fo | Fo Teor | Re2A1S2R2 Fe teor2 | Ao1 | Ao2 | DIF-A |
|---------|--------|---------|-----------------------|--------|--------|--------|
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0056 | 0.0108 | 0.0108 | 0.0108 | 0.0052 | 0.0052 |
| 2 | 0.0169 | 0.0215 | 0.0215 | 0.0160 | 0.0046 | 0.0046 |
| 3 | 0.0281 | 0.0321 | 0.0321 | 0.0152 | 0.0041 | 0.0041 |
| 4 | 0.0388 | 0.0426 | 0.0426 | 0.0145 | 0.0038 | 0.0038 |
| 5 | 0.0495 | 0.0530 | 0.0530 | 0.0142 | 0.0035 | 0.0035 |
| 6 | 0.0601 | 0.0633 | 0.0633 | 0.0138 | 0.0032 | 0.0032 |
| 7 | 0.0707 | 0.0734 | 0.0734 | 0.0133 | 0.0027 | 0.0027 |
| 8 | 0.0813 | 0.0835 | 0.0835 | 0.0128 | 0.0021 | 0.0021 |
| 9 | 0.0919 | 0.0934 | 0.0934 | 0.0121 | 0.0015 | 0.0015 |
| 10 | 0.1025 | 0.1032 | 0.1032 | 0.0113 | 0.0007 | 0.0007 |
| 11 | 0.1130 | 0.1129 | 0.1129 | 0.0104 | 0.0001 | 0.0001 |
| 12 | 0.1231 | 0.1225 | 0.1225 | 0.0095 | 0.0006 | 0.0006 |
| 13 | 0.1333 | 0.1320 | 0.1320 | 0.0089 | 0.0012 | 0.0012 |
| 14 | 0.1440 | 0.1414 | 0.1414 | 0.0082 | 0.0025 | 0.0025 |
| 15 | 0.1545 | 0.1507 | 0.1507 | 0.0068 | 0.0037 | 0.0037 |
| 16 | 0.1645 | 0.1599 | 0.1599 | 0.0055 | 0.0046 | 0.0046 |
| 17 | 0.1742 | 0.1690 | 0.1690 | 0.0045 | 0.0052 | 0.0052 |
| 18 | 0.1833 | 0.1780 | 0.1780 | 0.0038 | 0.0053 | 0.0053 |
| 19 | 0.1924 | 0.1869 | 0.1869 | 0.0036 | 0.0054 | 0.0054 |
| 20 | 0.2016 | 0.1958 | 0.1958 | 0.0034 | 0.0058 | 0.0058 |
| 21 | 0.2116 | 0.2045 | 0.2045 | 0.0029 | 0.0071 | 0.0071 |
| 22 | 0.2219 | 0.2131 | 0.2131 | 0.0015 | 0.0088 | 0.0088 |
| 23 | 0.2316 | 0.2216 | 0.2216 | 0.0003 | 0.0100 | 0.0100 |
| 24 | 0.2410 | 0.2300 | 0.2300 | 0.0016 | 0.0110 | 0.0109 |
| 25 | 0.2507 | 0.2384 | 0.2384 | 0.0026 | 0.0123 | 0.0123 |
| 26 | 0.2605 | 0.2466 | 0.2466 | 0.0041 | 0.0139 | 0.0139 |
| 27 | 0.2703 | 0.2548 | 0.2548 | 0.0057 | 0.0155 | 0.0155 |
| 28 | 0.2800 | 0.2629 | 0.2629 | 0.0075 | 0.0172 | 0.0172 |
| 29 | 0.2890 | 0.2709 | 0.2709 | 0.0092 | 0.0182 | 0.0182 |
| 30 | 0.2975 | 0.2788 | 0.2788 | 0.0103 | 0.0187 | 0.0187 |
| 31 | 0.3215 | 0.3019 | 0.3019 | 0.0045 | 0.0195 | 0.0195 |
| 32 | 0.3443 | 0.3244 | 0.3244 | 0.0029 | 0.0200 | 0.0200 |
| 33 | 0.3662 | 0.3461 | 0.3461 | 0.0018 | 0.0201 | 0.0201 |
| 34 | 0.3873 | 0.3671 | 0.3671 | 0.0009 | 0.0202 | 0.0201 |
| 35 | 0.4075 | 0.3875 | 0.3875 | 0.0002 | 0.0200 | 0.0200 |
| 36 | 0.4271 | 0.4072 | 0.4072 | 0.0003 | 0.0199 | 0.0199 |

TABLA VI-12-A
Número

continuación..

Re2A1S2R2

| Número | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
|--------|--------|---------|----------|--------|--------|--------|
| 37 | 0.4462 | 0.4262 | 0.4262 | 0.0009 | 0.0200 | 0.0200 |
| 38 | 0.4649 | 0.4447 | 0.4447 | 0.0015 | 0.0202 | 0.0202 |
| 39 | 0.4830 | 0.4625 | 0.4625 | 0.0024 | 0.0204 | 0.0204 |
| 40 | 0.5001 | 0.4798 | 0.4798 | 0.0032 | 0.0203 | 0.0203 |
| 41 | 0.5168 | 0.4965 | 0.4965 | 0.0036 | 0.0203 | 0.0203 |
| 42 | 0.5333 | 0.5127 | 0.5127 | 0.0041 | 0.0206 | 0.0206 |
| 43 | 0.5489 | 0.5284 | 0.5284 | 0.0049 | 0.0205 | 0.0205 |
| 44 | 0.5635 | 0.5435 | 0.5436 | 0.0054 | 0.0200 | 0.0200 |
| 45 | 0.5771 | 0.5582 | 0.5582 | 0.0053 | 0.0189 | 0.0189 |
| 46 | 0.6029 | 0.5862 | 0.5862 | 0.0091 | 0.0168 | 0.0167 |
| 47 | 0.6282 | 0.6123 | 0.6124 | 0.0094 | 0.0158 | 0.0158 |
| 48 | 0.6521 | 0.6369 | 0.6369 | 0.0087 | 0.0152 | 0.0152 |
| 49 | 0.6745 | 0.6598 | 0.6599 | 0.0077 | 0.0147 | 0.0146 |
| 50 | 0.6952 | 0.6814 | 0.6814 | 0.0069 | 0.0138 | 0.0138 |
| 51 | 0.7145 | 0.7015 | 0.7016 | 0.0063 | 0.0129 | 0.0129 |
| 52 | 0.7326 | 0.7204 | 0.7205 | 0.0059 | 0.0122 | 0.0121 |
| 53 | 0.7493 | 0.7381 | 0.7382 | 0.0055 | 0.0112 | 0.0111 |
| 54 | 0.7653 | 0.7547 | 0.7548 | 0.0053 | 0.0107 | 0.0106 |
| 55 | 0.7797 | 0.7702 | 0.7703 | 0.0049 | 0.0095 | 0.0094 |
| 56 | 0.7933 | 0.7847 | 0.7848 | 0.0050 | 0.0085 | 0.0084 |
| 57 | 0.8076 | 0.7983 | 0.7985 | 0.0051 | 0.0092 | 0.0091 |
| 58 | 0.8213 | 0.8111 | 0.8112 | 0.0035 | 0.0102 | 0.0101 |
| 59 | 0.8331 | 0.8231 | 0.8232 | 0.0018 | 0.0100 | 0.0099 |
| 60 | 0.8427 | 0.8342 | 0.8344 | 0.0012 | 0.0085 | 0.0084 |
| 61 | 0.8517 | 0.8447 | 0.8449 | 0.0020 | 0.0070 | 0.0069 |
| 62 | 0.8607 | 0.8546 | 0.8547 | 0.0028 | 0.0062 | 0.0061 |
| 63 | 0.8685 | 0.8638 | 0.8639 | 0.0030 | 0.0048 | 0.0046 |
| 64 | 0.8754 | 0.8724 | 0.8725 | 0.0038 | 0.0030 | 0.0028 |
| 65 | 0.8826 | 0.8804 | 0.8806 | 0.0051 | 0.0021 | 0.0020 |
| 66 | 0.8894 | 0.8880 | 0.8882 | 0.0054 | 0.0014 | 0.0012 |
| 67 | 0.8952 | 0.8951 | 0.8952 | 0.0057 | 0.0001 | 0.0000 |
| 68 | 0.9013 | 0.9017 | 0.9019 | 0.0065 | 0.0005 | 0.0006 |
| 69 | 0.9074 | 0.9080 | 0.9081 | 0.0067 | 0.0006 | 0.0007 |
| 70 | 0.9106 | 0.9138 | 0.9139 | 0.0064 | 0.0032 | 0.0033 |

TABLA VI-13-A

| Número | Re2A2S1R1 | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0061 | 0.0108 | 0.0108 | 0.0108 | 0.0048 | 0.0048 |
| 2 | 0.0181 | 0.0215 | 0.0215 | 0.0155 | 0.0034 | 0.0034 |
| 3 | 0.0301 | 0.0321 | 0.0321 | 0.0140 | 0.0021 | 0.0021 |
| 4 | 0.0420 | 0.0426 | 0.0426 | 0.0125 | 0.0007 | 0.0007 |
| 5 | 0.0538 | 0.0530 | 0.0530 | 0.0110 | 0.0008 | 0.0008 |
| 6 | 0.0654 | 0.0633 | 0.0633 | 0.0095 | 0.0021 | 0.0021 |
| 7 | 0.0768 | 0.0734 | 0.0734 | 0.0080 | 0.0034 | 0.0034 |
| 8 | 0.0881 | 0.0835 | 0.0835 | 0.0067 | 0.0047 | 0.0047 |
| 9 | 0.0995 | 0.0934 | 0.0934 | 0.0052 | 0.0061 | 0.0061 |
| 10 | 0.1107 | 0.1032 | 0.1032 | 0.0038 | 0.0075 | 0.0075 |
| 11 | 0.1218 | 0.1129 | 0.1129 | 0.0023 | 0.0089 | 0.0089 |
| 12 | 0.1327 | 0.1225 | 0.1225 | 0.0008 | 0.0102 | 0.0102 |
| 13 | 0.1436 | 0.1320 | 0.1320 | 0.0007 | 0.0115 | 0.0115 |
| 14 | 0.1542 | 0.1414 | 0.1414 | 0.0021 | 0.0128 | 0.0128 |
| 15 | 0.1648 | 0.1507 | 0.1507 | 0.0035 | 0.0141 | 0.0141 |
| 16 | 0.1754 | 0.1599 | 0.1599 | 0.0049 | 0.0154 | 0.0154 |
| 17 | 0.1860 | 0.1690 | 0.1690 | 0.0063 | 0.0170 | 0.0170 |
| 18 | 0.1968 | 0.1780 | 0.1780 | 0.0080 | 0.0188 | 0.0188 |
| 19 | 0.2076 | 0.1869 | 0.1869 | 0.0099 | 0.0206 | 0.0206 |
| 20 | 0.2182 | 0.1958 | 0.1958 | 0.0118 | 0.0225 | 0.0225 |
| 21 | 0.2288 | 0.2045 | 0.2045 | 0.0138 | 0.0243 | 0.0244 |
| 22 | 0.2393 | 0.2131 | 0.2131 | 0.0157 | 0.0263 | 0.0263 |
| 23 | 0.2498 | 0.2216 | 0.2216 | 0.0177 | 0.0282 | 0.0282 |
| 24 | 0.2602 | 0.2300 | 0.2300 | 0.0197 | 0.0302 | 0.0302 |
| 25 | 0.2705 | 0.2384 | 0.2384 | 0.0218 | 0.0321 | 0.0321 |
| 26 | 0.2806 | 0.2466 | 0.2466 | 0.0239 | 0.0340 | 0.0340 |
| 27 | 0.2906 | 0.2548 | 0.2548 | 0.0258 | 0.0358 | 0.0358 |
| 28 | 0.3004 | 0.2629 | 0.2629 | 0.0277 | 0.0375 | 0.0375 |
| 29 | 0.3100 | 0.2709 | 0.2709 | 0.0295 | 0.0392 | 0.0392 |
| 30 | 0.3196 | 0.2788 | 0.2788 | 0.0313 | 0.0408 | 0.0408 |
| 31 | 0.3277 | 0.3019 | 0.3019 | 0.0176 | 0.0457 | 0.0457 |
| 32 | 0.3748 | 0.3244 | 0.3244 | 0.0233 | 0.0504 | 0.0504 |
| 33 | 0.4004 | 0.3461 | 0.3461 | 0.0287 | 0.0543 | 0.0543 |
| 34 | 0.4250 | 0.3671 | 0.3671 | 0.0333 | 0.0579 | 0.0579 |
| 35 | 0.4486 | 0.3875 | 0.3875 | 0.0375 | 0.0611 | 0.0611 |
| 36 | 0.4707 | 0.4072 | 0.4072 | 0.0414 | 0.0636 | 0.0636 |

TABLA VI-13-A
Número

| | continuación.. | | Re2A2S1R1 | Ao1 | Ao2 | DIF-A |
|----|----------------|---------|-----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | | | |
| 37 | 0.4911 | 0.4262 | 0.4262 | 0.0445 | 0.0649 | 0.0649 |
| 38 | 0.5107 | 0.4447 | 0.4447 | 0.0464 | 0.0660 | 0.0660 |
| 39 | 0.5292 | 0.4625 | 0.4625 | 0.0481 | 0.0667 | 0.0667 |
| 40 | 0.5464 | 0.4798 | 0.4798 | 0.0494 | 0.0666 | 0.0666 |
| 41 | 0.5627 | 0.4965 | 0.4965 | 0.0499 | 0.0661 | 0.0661 |
| 42 | 0.5781 | 0.5127 | 0.5127 | 0.0499 | 0.0654 | 0.0654 |
| 43 | 0.5930 | 0.5284 | 0.5284 | 0.0497 | 0.0646 | 0.0647 |
| 44 | 0.6075 | 0.5435 | 0.5436 | 0.0495 | 0.0639 | 0.0639 |
| 45 | 0.6217 | 0.5582 | 0.5582 | 0.0492 | 0.0635 | 0.0635 |
| 46 | 0.6499 | 0.5862 | 0.5862 | 0.0355 | 0.0637 | 0.0637 |
| 47 | 0.6760 | 0.6123 | 0.6124 | 0.0375 | 0.0636 | 0.0636 |
| 48 | 0.7001 | 0.6369 | 0.6369 | 0.0391 | 0.0632 | 0.0632 |
| 49 | 0.7215 | 0.6598 | 0.6599 | 0.0402 | 0.0616 | 0.0617 |
| 50 | 0.7405 | 0.6814 | 0.6814 | 0.0401 | 0.0591 | 0.0592 |
| 51 | 0.7585 | 0.7015 | 0.7016 | 0.0389 | 0.0569 | 0.0570 |
| 52 | 0.7747 | 0.7204 | 0.7205 | 0.0380 | 0.0542 | 0.0543 |
| 53 | 0.7888 | 0.7381 | 0.7382 | 0.0365 | 0.0507 | 0.0508 |
| 54 | 0.8021 | 0.7547 | 0.7548 | 0.0341 | 0.0473 | 0.0474 |
| 55 | 0.8145 | 0.7702 | 0.7703 | 0.0318 | 0.0442 | 0.0443 |
| 56 | 0.8253 | 0.7847 | 0.7848 | 0.0296 | 0.0405 | 0.0406 |
| 57 | 0.8351 | 0.7983 | 0.7985 | 0.0268 | 0.0366 | 0.0367 |
| 58 | 0.8446 | 0.8111 | 0.8112 | 0.0239 | 0.0334 | 0.0335 |
| 59 | 0.8532 | 0.8231 | 0.8232 | 0.0214 | 0.0300 | 0.0302 |
| 60 | 0.8608 | 0.8342 | 0.8344 | 0.0188 | 0.0264 | 0.0265 |
| 61 | 0.8676 | 0.8447 | 0.8449 | 0.0159 | 0.0228 | 0.0229 |
| 62 | 0.8740 | 0.8546 | 0.8547 | 0.0129 | 0.0193 | 0.0195 |
| 63 | 0.8801 | 0.8638 | 0.8639 | 0.0101 | 0.0162 | 0.0163 |
| 64 | 0.8854 | 0.8724 | 0.8725 | 0.0076 | 0.0129 | 0.0131 |
| 65 | 0.8903 | 0.8804 | 0.8806 | 0.0048 | 0.0097 | 0.0099 |
| 66 | 0.8951 | 0.8880 | 0.8882 | 0.0022 | 0.0069 | 0.0071 |
| 67 | 0.8993 | 0.8951 | 0.8952 | 0.0002 | 0.0040 | 0.0042 |
| 68 | 0.9028 | 0.9017 | 0.9019 | 0.0026 | 0.0009 | 0.0011 |
| 69 | 0.9060 | 0.9080 | 0.9081 | 0.0053 | 0.0021 | 0.0020 |
| 70 | 0.9082 | 0.9138 | 0.9139 | 0.0080 | 0.0057 | 0.0056 |

TABLA VI-14-A

| Número | Re2A2S1R1 | | | | | |
|---------|-----------|---------|----------|--------|--------|--------|
| | Fe | Fe Teor | Fe Teor2 | Ao1 | Ao2 | DIF-A |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0060 | 0.0108 | 0.0108 | 0.0108 | 0.0049 | 0.0049 |
| 2 | 0.0180 | 0.0215 | 0.0215 | 0.0156 | 0.0036 | 0.0036 |
| 3 | 0.0296 | 0.0321 | 0.0321 | 0.0142 | 0.0025 | 0.0025 |
| 4 | 0.0411 | 0.0426 | 0.0426 | 0.0130 | 0.0015 | 0.0015 |
| 5 | 0.0526 | 0.0530 | 0.0530 | 0.0119 | 0.0004 | 0.0004 |
| 6 | 0.0639 | 0.0633 | 0.0633 | 0.0107 | 0.0007 | 0.0007 |
| 7 | 0.0753 | 0.0734 | 0.0734 | 0.0095 | 0.0019 | 0.0019 |
| 8 | 0.0865 | 0.0835 | 0.0835 | 0.0081 | 0.0030 | 0.0030 |
| 9 | 0.0974 | 0.0934 | 0.0934 | 0.0069 | 0.0040 | 0.0040 |
| 10 | 0.1083 | 0.1032 | 0.1032 | 0.0058 | 0.0051 | 0.0051 |
| 11 | 0.1194 | 0.1129 | 0.1129 | 0.0046 | 0.0065 | 0.0065 |
| 12 | 0.1304 | 0.1225 | 0.1225 | 0.0031 | 0.0079 | 0.0079 |
| 13 | 0.1414 | 0.1320 | 0.1320 | 0.0016 | 0.0094 | 0.0094 |
| 14 | 0.1524 | 0.1414 | 0.1414 | 0.0000 | 0.0110 | 0.0110 |
| 15 | 0.1632 | 0.1507 | 0.1507 | 0.0017 | 0.0125 | 0.0125 |
| 16 | 0.1739 | 0.1599 | 0.1599 | 0.0033 | 0.0140 | 0.0140 |
| 17 | 0.1844 | 0.1690 | 0.1690 | 0.0049 | 0.0154 | 0.0154 |
| 18 | 0.1948 | 0.1780 | 0.1780 | 0.0064 | 0.0168 | 0.0168 |
| 19 | 0.2053 | 0.1869 | 0.1869 | 0.0079 | 0.0183 | 0.0183 |
| 20 | 0.2156 | 0.1958 | 0.1958 | 0.0095 | 0.0199 | 0.0199 |
| 21 | 0.2256 | 0.2045 | 0.2045 | 0.0112 | 0.0211 | 0.0211 |
| 22 | 0.2352 | 0.2131 | 0.2131 | 0.0125 | 0.0221 | 0.0221 |
| 23 | 0.2447 | 0.2216 | 0.2216 | 0.0136 | 0.0231 | 0.0231 |
| 24 | 0.2543 | 0.2300 | 0.2300 | 0.0147 | 0.0243 | 0.0243 |
| 25 | 0.2638 | 0.2384 | 0.2384 | 0.0159 | 0.0254 | 0.0254 |
| 26 | 0.2730 | 0.2466 | 0.2466 | 0.0172 | 0.0264 | 0.0264 |
| 27 | 0.2821 | 0.2548 | 0.2548 | 0.0182 | 0.0273 | 0.0273 |
| 28 | 0.2915 | 0.2629 | 0.2629 | 0.0192 | 0.0286 | 0.0286 |
| 29 | 0.3012 | 0.2709 | 0.2709 | 0.0206 | 0.0303 | 0.0303 |
| 30 | 0.3106 | 0.2788 | 0.2788 | 0.0224 | 0.0318 | 0.0318 |
| 31 | 0.3376 | 0.3019 | 0.3019 | 0.0086 | 0.0357 | 0.0357 |
| 32 | 0.3635 | 0.3244 | 0.3244 | 0.0133 | 0.0391 | 0.0391 |
| 33 | 0.3885 | 0.3461 | 0.3461 | 0.0174 | 0.0424 | 0.0424 |
| 34 | 0.4126 | 0.3671 | 0.3671 | 0.0214 | 0.0455 | 0.0455 |
| 35 | 0.4360 | 0.3875 | 0.3875 | 0.0251 | 0.0485 | 0.0485 |
| 36 | 0.4583 | 0.4072 | 0.4072 | 0.0288 | 0.0511 | 0.0511 |

TABLA VI-14-A
Número

| | continuación.. | | Re2A2S1R2 | | | |
|----|----------------|---------|-----------|--------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ac1 | Ac2 | DIF-A |
| 37 | 0.4787 | 0.4262 | 0.4262 | 0.0320 | 0.0524 | 0.0524 |
| 38 | 0.4983 | 0.4447 | 0.4447 | 0.0340 | 0.0536 | 0.0536 |
| 39 | 0.5178 | 0.4625 | 0.4625 | 0.0358 | 0.0553 | 0.0553 |
| 40 | 0.5372 | 0.4798 | 0.4798 | 0.0380 | 0.0574 | 0.0574 |
| 41 | 0.5556 | 0.4965 | 0.4965 | 0.0407 | 0.0590 | 0.0590 |
| 42 | 0.5727 | 0.5127 | 0.5127 | 0.0428 | 0.0600 | 0.0600 |
| 43 | 0.5896 | 0.5284 | 0.5284 | 0.0443 | 0.0612 | 0.0612 |
| 44 | 0.6057 | 0.5435 | 0.5436 | 0.0461 | 0.0622 | 0.0622 |
| 45 | 0.6202 | 0.5582 | 0.5582 | 0.0475 | 0.0620 | 0.0619 |
| 46 | 0.6465 | 0.5862 | 0.5862 | 0.0340 | 0.0603 | 0.0603 |
| 47 | 0.6718 | 0.6123 | 0.6124 | 0.0342 | 0.0595 | 0.0594 |
| 48 | 0.6952 | 0.6369 | 0.6369 | 0.0349 | 0.0583 | 0.0583 |
| 49 | 0.7173 | 0.6598 | 0.6599 | 0.0354 | 0.0574 | 0.0574 |
| 50 | 0.7378 | 0.6814 | 0.6814 | 0.0359 | 0.0564 | 0.0563 |
| 51 | 0.7559 | 0.7015 | 0.7016 | 0.0362 | 0.0544 | 0.0543 |
| 52 | 0.7733 | 0.7204 | 0.7205 | 0.0355 | 0.0529 | 0.0528 |
| 53 | 0.7888 | 0.7381 | 0.7382 | 0.0352 | 0.0507 | 0.0506 |
| 54 | 0.8026 | 0.7547 | 0.7548 | 0.0342 | 0.0479 | 0.0478 |
| 55 | 0.8153 | 0.7702 | 0.7703 | 0.0324 | 0.0451 | 0.0450 |
| 56 | 0.8262 | 0.7847 | 0.7848 | 0.0306 | 0.0414 | 0.0413 |
| 57 | 0.8354 | 0.7983 | 0.7985 | 0.0278 | 0.0371 | 0.0370 |
| 58 | 0.8440 | 0.8111 | 0.8112 | 0.0243 | 0.0329 | 0.0328 |
| 59 | 0.8520 | 0.8231 | 0.8232 | 0.0209 | 0.0290 | 0.0288 |
| 60 | 0.8594 | 0.8342 | 0.8344 | 0.0178 | 0.0252 | 0.0250 |
| 61 | 0.8666 | 0.8447 | 0.8449 | 0.0147 | 0.0219 | 0.0218 |
| 62 | 0.8735 | 0.8546 | 0.8547 | 0.0121 | 0.0190 | 0.0188 |
| 63 | 0.8799 | 0.8638 | 0.8639 | 0.0098 | 0.0162 | 0.0160 |
| 64 | 0.8861 | 0.8724 | 0.8725 | 0.0076 | 0.0137 | 0.0136 |
| 65 | 0.8915 | 0.8804 | 0.8806 | 0.0056 | 0.0111 | 0.0110 |
| 66 | 0.8964 | 0.8880 | 0.8882 | 0.0035 | 0.0084 | 0.0082 |
| 67 | 0.9007 | 0.8951 | 0.8952 | 0.0013 | 0.0056 | 0.0055 |
| 68 | 0.9044 | 0.9017 | 0.9019 | 0.0010 | 0.0027 | 0.0025 |
| 69 | 0.9077 | 0.9080 | 0.9081 | 0.0036 | 0.0003 | 0.0004 |
| 70 | 0.9100 | 0.9138 | 0.9139 | 0.0061 | 0.0037 | 0.0039 |

TABLA VI-15-A
Número

| | Fe | Fe Teor | Re2A2S2R1 Fe teor2 | As1 | As2 | DIF-A |
|---------|--------|---------|-----------------------|--------|--------|--------|
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0057 | 0.0108 | 0.0108 | 0.0108 | 0.0051 | 0.0051 |
| 2 | 0.0172 | 0.0215 | 0.0215 | 0.0159 | 0.0044 | 0.0044 |
| 3 | 0.0288 | 0.0321 | 0.0321 | 0.0150 | 0.0033 | 0.0033 |
| 4 | 0.0406 | 0.0426 | 0.0426 | 0.0138 | 0.0020 | 0.0020 |
| 5 | 0.0523 | 0.0530 | 0.0530 | 0.0124 | 0.0007 | 0.0007 |
| 6 | 0.0639 | 0.0633 | 0.0633 | 0.0109 | 0.0006 | 0.0006 |
| 7 | 0.0753 | 0.0734 | 0.0734 | 0.0095 | 0.0018 | 0.0018 |
| 8 | 0.0864 | 0.0835 | 0.0835 | 0.0082 | 0.0029 | 0.0029 |
| 9 | 0.0976 | 0.0934 | 0.0934 | 0.0070 | 0.0042 | 0.0042 |
| 10 | 0.1088 | 0.1032 | 0.1032 | 0.0056 | 0.0056 | 0.0056 |
| 11 | 0.1195 | 0.1129 | 0.1129 | 0.0041 | 0.0066 | 0.0066 |
| 12 | 0.1301 | 0.1225 | 0.1225 | 0.0030 | 0.0076 | 0.0076 |
| 13 | 0.1404 | 0.1320 | 0.1320 | 0.0019 | 0.0083 | 0.0083 |
| 14 | 0.1504 | 0.1414 | 0.1414 | 0.0011 | 0.0090 | 0.0090 |
| 15 | 0.1605 | 0.1507 | 0.1507 | 0.0003 | 0.0097 | 0.0097 |
| 16 | 0.1703 | 0.1599 | 0.1599 | 0.0005 | 0.0104 | 0.0104 |
| 17 | 0.1800 | 0.1690 | 0.1690 | 0.0013 | 0.0110 | 0.0110 |
| 18 | 0.1896 | 0.1780 | 0.1780 | 0.0020 | 0.0116 | 0.0116 |
| 19 | 0.1993 | 0.1869 | 0.1869 | 0.0027 | 0.0123 | 0.0123 |
| 20 | 0.2089 | 0.1958 | 0.1958 | 0.0035 | 0.0131 | 0.0131 |
| 21 | 0.2183 | 0.2045 | 0.2045 | 0.0044 | 0.0139 | 0.0139 |
| 22 | 0.2277 | 0.2131 | 0.2131 | 0.0053 | 0.0146 | 0.0146 |
| 23 | 0.2370 | 0.2216 | 0.2216 | 0.0061 | 0.0154 | 0.0154 |
| 24 | 0.2464 | 0.2300 | 0.2300 | 0.0070 | 0.0164 | 0.0164 |
| 25 | 0.2559 | 0.2384 | 0.2384 | 0.0080 | 0.0175 | 0.0175 |
| 26 | 0.2653 | 0.2466 | 0.2466 | 0.0093 | 0.0186 | 0.0186 |
| 27 | 0.2744 | 0.2548 | 0.2548 | 0.0105 | 0.0196 | 0.0196 |
| 28 | 0.2835 | 0.2629 | 0.2629 | 0.0115 | 0.0207 | 0.0206 |
| 29 | 0.2923 | 0.2709 | 0.2709 | 0.0127 | 0.0215 | 0.0215 |
| 30 | 0.3009 | 0.2788 | 0.2788 | 0.0136 | 0.0222 | 0.0222 |
| 31 | 0.3267 | 0.3019 | 0.3019 | 0.0010 | 0.0247 | 0.0247 |
| 32 | 0.3517 | 0.3244 | 0.3244 | 0.0023 | 0.0273 | 0.0273 |
| 33 | 0.3756 | 0.3461 | 0.3461 | 0.0056 | 0.0295 | 0.0295 |
| 34 | 0.3982 | 0.3671 | 0.3671 | 0.0084 | 0.0311 | 0.0311 |
| 35 | 0.4205 | 0.3875 | 0.3875 | 0.0107 | 0.0331 | 0.0331 |
| 36 | 0.4421 | 0.4072 | 0.4072 | 0.0134 | 0.0349 | 0.0349 |

TABLA VI-15-A
Número

continuación.. Re2A2S2R1
Fe Fe Teor Fe teor2

| | | | | Ao1 | Ao2 | DIF-A |
|----|--------|--------|--------|--------|--------|--------|
| 37 | 0.4619 | 0.4262 | 0.4262 | 0.0159 | 0.0357 | 0.0356 |
| 38 | 0.4800 | 0.4447 | 0.4447 | 0.0172 | 0.0354 | 0.0354 |
| 39 | 0.4976 | 0.4625 | 0.4625 | 0.0175 | 0.0351 | 0.0351 |
| 40 | 0.5150 | 0.4798 | 0.4798 | 0.0178 | 0.0352 | 0.0352 |
| 41 | 0.5320 | 0.4965 | 0.4965 | 0.0185 | 0.0354 | 0.0354 |
| 42 | 0.5477 | 0.5127 | 0.5127 | 0.0192 | 0.0350 | 0.0350 |
| 43 | 0.5627 | 0.5284 | 0.5284 | 0.0194 | 0.0343 | 0.0343 |
| 44 | 0.5777 | 0.5435 | 0.5436 | 0.0192 | 0.0342 | 0.0342 |
| 45 | 0.5923 | 0.5582 | 0.5582 | 0.0195 | 0.0341 | 0.0341 |
| 46 | 0.6194 | 0.5862 | 0.5862 | 0.0061 | 0.0332 | 0.0332 |
| 47 | 0.6447 | 0.6123 | 0.6124 | 0.0070 | 0.0324 | 0.0324 |
| 48 | 0.6688 | 0.6369 | 0.6369 | 0.0079 | 0.0319 | 0.0319 |
| 49 | 0.6914 | 0.6598 | 0.6599 | 0.0089 | 0.0315 | 0.0315 |
| 50 | 0.7115 | 0.6814 | 0.6814 | 0.0100 | 0.0302 | 0.0301 |
| 51 | 0.7301 | 0.7015 | 0.7016 | 0.0100 | 0.0286 | 0.0285 |
| 52 | 0.7476 | 0.7204 | 0.7205 | 0.0097 | 0.0272 | 0.0271 |
| 53 | 0.7641 | 0.7381 | 0.7382 | 0.0095 | 0.0260 | 0.0259 |
| 54 | 0.7798 | 0.7547 | 0.7548 | 0.0095 | 0.0251 | 0.0250 |
| 55 | 0.7940 | 0.7702 | 0.7703 | 0.0096 | 0.0238 | 0.0237 |
| 56 | 0.8075 | 0.7847 | 0.7848 | 0.0092 | 0.0228 | 0.0227 |
| 57 | 0.8207 | 0.7983 | 0.7985 | 0.0092 | 0.0224 | 0.0223 |
| 58 | 0.8326 | 0.8111 | 0.8112 | 0.0096 | 0.0215 | 0.0214 |
| 59 | 0.8434 | 0.8231 | 0.8232 | 0.0095 | 0.0203 | 0.0202 |
| 60 | 0.8532 | 0.8342 | 0.8344 | 0.0091 | 0.0190 | 0.0189 |
| 61 | 0.8622 | 0.8447 | 0.8449 | 0.0085 | 0.0175 | 0.0174 |
| 62 | 0.8704 | 0.8546 | 0.8547 | 0.0077 | 0.0159 | 0.0157 |
| 63 | 0.8779 | 0.8638 | 0.8639 | 0.0066 | 0.0142 | 0.0140 |
| 64 | 0.8844 | 0.8724 | 0.8725 | 0.0056 | 0.0120 | 0.0119 |
| 65 | 0.8895 | 0.8804 | 0.8806 | 0.0039 | 0.0091 | 0.0089 |
| 66 | 0.8935 | 0.8880 | 0.8882 | 0.0015 | 0.0055 | 0.0054 |
| 67 | 0.8967 | 0.8951 | 0.8952 | 0.0016 | 0.0016 | 0.0015 |
| 68 | 0.8995 | 0.9017 | 0.9019 | 0.0050 | 0.0022 | 0.0024 |
| 69 | 0.9017 | 0.9080 | 0.9081 | 0.0084 | 0.0062 | 0.0064 |
| 70 | 0.9035 | 0.9138 | 0.9139 | 0.0121 | 0.0103 | 0.0104 |

TABLA VI-16-A

| Número | Re2A2S2R2 | | | | | |
|---------|----------------|---------------------|----------------------|-----------------|-----------------|--------|
| | F ₀ | F _a Teor | F _e teor2 | A ₀₁ | A ₀₂ | DIF-A |
| initial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0060 | 0.0108 | 0.0108 | 0.0108 | 0.0048 | 0.0048 |
| 2 | 0.0177 | 0.0215 | 0.0215 | 0.0155 | 0.0039 | 0.0039 |
| 3 | 0.0291 | 0.0321 | 0.0321 | 0.0145 | 0.0031 | 0.0031 |
| 4 | 0.0406 | 0.0426 | 0.0426 | 0.0136 | 0.0021 | 0.0021 |
| 5 | 0.0517 | 0.0530 | 0.0530 | 0.0124 | 0.0013 | 0.0013 |
| 6 | 0.0627 | 0.0633 | 0.0633 | 0.0115 | 0.0006 | 0.0006 |
| 7 | 0.0737 | 0.0734 | 0.0734 | 0.0107 | 0.0003 | 0.0003 |
| 8 | 0.0850 | 0.0835 | 0.0835 | 0.0097 | 0.0015 | 0.0015 |
| 9 | 0.0962 | 0.0934 | 0.0934 | 0.0084 | 0.0029 | 0.0029 |
| 10 | 0.1070 | 0.1032 | 0.1032 | 0.0070 | 0.0038 | 0.0038 |
| 11 | 0.1173 | 0.1129 | 0.1129 | 0.0060 | 0.0044 | 0.0044 |
| 12 | 0.1277 | 0.1225 | 0.1225 | 0.0052 | 0.0051 | 0.0051 |
| 13 | 0.1379 | 0.1320 | 0.1320 | 0.0044 | 0.0059 | 0.0059 |
| 14 | 0.1482 | 0.1414 | 0.1414 | 0.0035 | 0.0068 | 0.0067 |
| 15 | 0.1584 | 0.1507 | 0.1507 | 0.0026 | 0.0077 | 0.0077 |
| 16 | 0.1683 | 0.1599 | 0.1599 | 0.0015 | 0.0084 | 0.0084 |
| 17 | 0.1780 | 0.1690 | 0.1690 | 0.0007 | 0.0090 | 0.0090 |
| 18 | 0.1876 | 0.1780 | 0.1780 | 0.0000 | 0.0096 | 0.0096 |
| 19 | 0.1972 | 0.1869 | 0.1869 | 0.0007 | 0.0103 | 0.0102 |
| 20 | 0.2064 | 0.1958 | 0.1958 | 0.0014 | 0.0107 | 0.0107 |
| 21 | 0.2155 | 0.2045 | 0.2045 | 0.0020 | 0.0110 | 0.0110 |
| 22 | 0.2243 | 0.2131 | 0.2131 | 0.0024 | 0.0112 | 0.0112 |
| 23 | 0.2332 | 0.2216 | 0.2216 | 0.0027 | 0.0116 | 0.0116 |
| 24 | 0.2421 | 0.2300 | 0.2300 | 0.0032 | 0.0121 | 0.0121 |
| 25 | 0.2510 | 0.2384 | 0.2384 | 0.0037 | 0.0126 | 0.0126 |
| 26 | 0.2600 | 0.2466 | 0.2466 | 0.0043 | 0.0134 | 0.0134 |
| 27 | 0.2690 | 0.2548 | 0.2548 | 0.0052 | 0.0142 | 0.0142 |
| 28 | 0.2778 | 0.2629 | 0.2629 | 0.0061 | 0.0149 | 0.0149 |
| 29 | 0.2865 | 0.2709 | 0.2709 | 0.0069 | 0.0157 | 0.0157 |
| 30 | 0.2953 | 0.2788 | 0.2788 | 0.0078 | 0.0165 | 0.0165 |
| 31 | 0.3207 | 0.3019 | 0.3019 | 0.0067 | 0.0187 | 0.0187 |
| 32 | 0.3455 | 0.3244 | 0.3244 | 0.0037 | 0.0211 | 0.0211 |
| 33 | 0.3693 | 0.3461 | 0.3461 | 0.0007 | 0.0232 | 0.0232 |
| 34 | 0.3914 | 0.3671 | 0.3671 | 0.0022 | 0.0243 | 0.0243 |
| 35 | 0.4118 | 0.3875 | 0.3875 | 0.0039 | 0.0244 | 0.0243 |
| 36 | 0.4309 | 0.4072 | 0.4072 | 0.0047 | 0.0238 | 0.0238 |

TABLA VI-16-A

| Número | continuación.. | | | Re2A252R2 | | DIF-A |
|--------|----------------|---------|----------|-----------|--------|--------|
| | Fe | Fe Teor | Fe teor2 | Ao1 | Ao2 | |
| 37 | 0.4490 | 0.4262 | 0.4262 | 0.0047 | 0.0228 | 0.0228 |
| 38 | 0.4668 | 0.4447 | 0.4447 | 0.0043 | 0.0222 | 0.0221 |
| 39 | 0.4847 | 0.4625 | 0.4625 | 0.0043 | 0.0222 | 0.0222 |
| 40 | 0.5023 | 0.4798 | 0.4798 | 0.0049 | 0.0225 | 0.0224 |
| 41 | 0.5192 | 0.4965 | 0.4965 | 0.0057 | 0.0226 | 0.0226 |
| 42 | 0.5350 | 0.5127 | 0.5127 | 0.0065 | 0.0223 | 0.0222 |
| 43 | 0.5502 | 0.5284 | 0.5284 | 0.0066 | 0.0218 | 0.0217 |
| 44 | 0.5648 | 0.5435 | 0.5436 | 0.0066 | 0.0212 | 0.0212 |
| 45 | 0.5785 | 0.5582 | 0.5582 | 0.0066 | 0.0203 | 0.0202 |
| 46 | 0.6043 | 0.5862 | 0.5862 | 0.0077 | 0.0182 | 0.0181 |
| 47 | 0.6288 | 0.6123 | 0.6124 | 0.0080 | 0.0165 | 0.0164 |
| 48 | 0.6525 | 0.6369 | 0.6369 | 0.0080 | 0.0157 | 0.0156 |
| 49 | 0.6754 | 0.6598 | 0.6599 | 0.0073 | 0.0156 | 0.0155 |
| 50 | 0.6961 | 0.6814 | 0.6814 | 0.0059 | 0.0148 | 0.0147 |
| 51 | 0.7142 | 0.7015 | 0.7016 | 0.0054 | 0.0127 | 0.0126 |
| 52 | 0.7307 | 0.7204 | 0.7205 | 0.0062 | 0.0103 | 0.0102 |
| 53 | 0.7471 | 0.7381 | 0.7382 | 0.0074 | 0.0090 | 0.0089 |
| 54 | 0.7632 | 0.7547 | 0.7548 | 0.0076 | 0.0086 | 0.0085 |
| 55 | 0.7784 | 0.7702 | 0.7703 | 0.0070 | 0.0082 | 0.0081 |
| 56 | 0.7925 | 0.7847 | 0.7848 | 0.0064 | 0.0078 | 0.0077 |
| 57 | 0.8055 | 0.7983 | 0.7985 | 0.0058 | 0.0071 | 0.0070 |
| 58 | 0.8170 | 0.8111 | 0.8112 | 0.0056 | 0.0059 | 0.0057 |
| 59 | 0.8275 | 0.8231 | 0.8232 | 0.0061 | 0.0045 | 0.0044 |
| 60 | 0.8374 | 0.8342 | 0.8344 | 0.0067 | 0.0031 | 0.0030 |
| 61 | 0.8469 | 0.8447 | 0.8449 | 0.0073 | 0.0022 | 0.0021 |
| 62 | 0.8557 | 0.8546 | 0.8547 | 0.0076 | 0.0012 | 0.0010 |
| 63 | 0.8635 | 0.8638 | 0.8639 | 0.0080 | 0.0003 | 0.0004 |
| 64 | 0.8710 | 0.8724 | 0.8725 | 0.0089 | 0.0014 | 0.0015 |
| 65 | 0.8778 | 0.8804 | 0.8806 | 0.0095 | 0.0027 | 0.0028 |
| 66 | 0.8834 | 0.8880 | 0.8882 | 0.0103 | 0.0045 | 0.0046 |
| 67 | 0.8884 | 0.8951 | 0.8952 | 0.0115 | 0.0067 | 0.0069 |
| 68 | 0.8922 | 0.9017 | 0.9019 | 0.0134 | 0.0095 | 0.0097 |
| 69 | 0.8955 | 0.9080 | 0.9081 | 0.0158 | 0.0125 | 0.0126 |
| 70 | 0.8978 | 0.9138 | 0.9139 | 0.0183 | 0.0160 | 0.0161 |

La segunda serie de tablas nos muestra el tratamiento estadístico entre la prueba y su réplica con el objeto de saber si ambas siguen la misma distribución.

A continuación se define la nomenclatura de cada una de las columnas de estas tablas:

Número = Número de frecuencias acumuladas.

F_{eR1} = Frecuencias acumuladas de la prueba.

F_{eR2} = Frecuencias acumuladas de la réplica.

$F_{eR1}-F_{eR2}$ = Desviación para la prueba estadística

$$DIF(R1-R2) = |F_{eR1}-F_{eR2}|.$$

TABLA VI-1-B

| Número | | ReIAISI | | Número | | ReIAISI | |
|---------|--------|---------|-----------|--------|--------|---------|-----------|
| | FeR1 | FeR2 | FeR1-FeR2 | | FeR1 | FeR2 | FeR1-FeR2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.4170 | 0.4105 | 0.0065 |
| 1 | 0.0052 | 0.0053 | 0.0001 | 38 | 0.4366 | 0.4275 | 0.0091 |
| 2 | 0.0157 | 0.0158 | 0.0001 | 39 | 0.4552 | 0.4453 | 0.0099 |
| 3 | 0.0261 | 0.0263 | 0.0002 | 40 | 0.4728 | 0.4632 | 0.0096 |
| 4 | 0.0366 | 0.0366 | 0.0000 | 41 | 0.4898 | 0.4796 | 0.0102 |
| 5 | 0.0469 | 0.0467 | 0.0002 | 42 | 0.5066 | 0.4957 | 0.0109 |
| 6 | 0.0568 | 0.0576 | 0.0008 | 43 | 0.5227 | 0.5115 | 0.0112 |
| 7 | 0.0667 | 0.0665 | 0.0002 | 44 | 0.5384 | 0.5268 | 0.0116 |
| 8 | 0.0766 | 0.0762 | 0.0004 | 45 | 0.5540 | 0.5416 | 0.0124 |
| 9 | 0.0864 | 0.0858 | 0.0006 | 46 | 0.5685 | 0.5697 | 0.0138 |
| 10 | 0.0960 | 0.0954 | 0.0006 | 47 | 0.6098 | 0.5957 | 0.0141 |
| 11 | 0.1053 | 0.1048 | 0.0005 | 48 | 0.6339 | 0.6200 | 0.0139 |
| 12 | 0.1146 | 0.1142 | 0.0004 | 49 | 0.6564 | 0.6437 | 0.0127 |
| 13 | 0.1240 | 0.1236 | 0.0004 | 50 | 0.6769 | 0.6661 | 0.0108 |
| 14 | 0.1335 | 0.1333 | 0.0002 | 51 | 0.6960 | 0.6872 | 0.0088 |
| 15 | 0.1430 | 0.1428 | 0.0002 | 52 | 0.7141 | 0.7072 | 0.0069 |
| 16 | 0.1523 | 0.1521 | 0.0002 | 53 | 0.7316 | 0.7262 | 0.0054 |
| 17 | 0.1614 | 0.1611 | 0.0003 | 54 | 0.7483 | 0.7442 | 0.0041 |
| 18 | 0.1705 | 0.1695 | 0.0010 | 55 | 0.7638 | 0.7601 | 0.0037 |
| 19 | 0.1794 | 0.1777 | 0.0017 | 56 | 0.7780 | 0.7741 | 0.0039 |
| 20 | 0.1881 | 0.1859 | 0.0022 | 57 | 0.7913 | 0.7856 | 0.0057 |
| 21 | 0.1964 | 0.1942 | 0.0022 | 58 | 0.8040 | 0.7968 | 0.0072 |
| 22 | 0.2045 | 0.2027 | 0.0018 | 59 | 0.8155 | 0.8093 | 0.0062 |
| 23 | 0.2127 | 0.2112 | 0.0015 | 60 | 0.8265 | 0.8210 | 0.0055 |
| 24 | 0.2210 | 0.2195 | 0.0015 | 61 | 0.8372 | 0.8319 | 0.0053 |
| 25 | 0.2292 | 0.2279 | 0.0013 | 62 | 0.8475 | 0.8427 | 0.0048 |
| 26 | 0.2372 | 0.2364 | 0.0008 | 63 | 0.8572 | 0.8530 | 0.0042 |
| 27 | 0.2451 | 0.2449 | 0.0002 | 64 | 0.8662 | 0.8622 | 0.0040 |
| 28 | 0.2527 | 0.2526 | 0.0001 | 65 | 0.8753 | 0.8712 | 0.0041 |
| 29 | 0.2603 | 0.2601 | 0.0002 | 66 | 0.8846 | 0.8803 | 0.0043 |
| 30 | 0.2676 | 0.2670 | 0.0006 | 67 | 0.8920 | 0.8890 | 0.0030 |
| 31 | 0.2892 | 0.2902 | 0.0010 | 68 | 0.8977 | 0.8972 | 0.0005 |
| 32 | 0.3115 | 0.3114 | 0.0001 | 69 | 0.9039 | 0.9046 | 0.0007 |
| 33 | 0.3340 | 0.3325 | 0.0015 | 70 | 0.9073 | 0.9085 | 0.0012 |
| 34 | 0.3588 | 0.3541 | 0.0047 | | | | |
| 35 | 0.3759 | 0.3746 | 0.0013 | | | | |
| 36 | 0.3965 | 0.3931 | 0.0034 | | | | |

TABLA VI-2-B

| Número | ReIAIS2 | | | Número | FeR1 | FeR2 | FeR1-FeR2 |
|---------|---------|--------|-----------|--------|--------|--------|-----------|
| | FeR1 | FeR2 | FeR1-FeR2 | | | | |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.3927 | 0.3959 | 0.0032 |
| 1 | 0.0049 | 0.0051 | 0.0002 | 38 | 0.4100 | 0.4139 | 0.0039 |
| 2 | 0.0144 | 0.0155 | 0.0011 | 39 | 0.4274 | 0.4315 | 0.0041 |
| 3 | 0.0237 | 0.0259 | 0.0022 | 40 | 0.4441 | 0.4487 | 0.0046 |
| 4 | 0.0332 | 0.0360 | 0.0028 | 41 | 0.4599 | 0.4652 | 0.0053 |
| 5 | 0.0431 | 0.0458 | 0.0027 | 42 | 0.4751 | 0.4809 | 0.0058 |
| 6 | 0.0525 | 0.0557 | 0.0032 | 43 | 0.4900 | 0.4963 | 0.0063 |
| 7 | 0.0619 | 0.0649 | 0.0030 | 44 | 0.5044 | 0.5112 | 0.0068 |
| 8 | 0.0715 | 0.0733 | 0.0018 | 45 | 0.5185 | 0.5256 | 0.0071 |
| 9 | 0.0803 | 0.0817 | 0.0014 | 46 | 0.5462 | 0.5529 | 0.0067 |
| 10 | 0.0890 | 0.0904 | 0.0014 | 47 | 0.5715 | 0.5784 | 0.0069 |
| 11 | 0.0981 | 0.0994 | 0.0013 | 48 | 0.5950 | 0.6021 | 0.0071 |
| 12 | 0.1072 | 0.1084 | 0.0012 | 49 | 0.6185 | 0.6239 | 0.0054 |
| 13 | 0.1160 | 0.1172 | 0.0012 | 50 | 0.6411 | 0.6447 | 0.0036 |
| 14 | 0.1245 | 0.1259 | 0.0014 | 51 | 0.6614 | 0.6652 | 0.0038 |
| 15 | 0.1327 | 0.1343 | 0.0016 | 52 | 0.6816 | 0.6850 | 0.0034 |
| 16 | 0.1412 | 0.1426 | 0.0014 | 53 | 0.7012 | 0.7040 | 0.0028 |
| 17 | 0.1498 | 0.1511 | 0.0013 | 54 | 0.7195 | 0.7217 | 0.0022 |
| 18 | 0.1580 | 0.1596 | 0.0016 | 55 | 0.7373 | 0.7388 | 0.0015 |
| 19 | 0.1661 | 0.1678 | 0.0017 | 56 | 0.7541 | 0.7564 | 0.0023 |
| 20 | 0.1742 | 0.1759 | 0.0017 | 57 | 0.7693 | 0.7731 | 0.0038 |
| 21 | 0.1821 | 0.1840 | 0.0019 | 58 | 0.7838 | 0.7884 | 0.0046 |
| 22 | 0.1898 | 0.1921 | 0.0023 | 59 | 0.7972 | 0.8028 | 0.0056 |
| 23 | 0.1975 | 0.2001 | 0.0026 | 60 | 0.8099 | 0.8160 | 0.0061 |
| 24 | 0.2052 | 0.2078 | 0.0026 | 61 | 0.8221 | 0.8281 | 0.0060 |
| 25 | 0.2132 | 0.2155 | 0.0023 | 62 | 0.8334 | 0.8397 | 0.0063 |
| 26 | 0.2212 | 0.2233 | 0.0021 | 63 | 0.8445 | 0.8507 | 0.0062 |
| 27 | 0.2286 | 0.2311 | 0.0025 | 64 | 0.8552 | 0.8612 | 0.0060 |
| 28 | 0.2362 | 0.2389 | 0.0027 | 65 | 0.8651 | 0.8716 | 0.0065 |
| 29 | 0.2441 | 0.2465 | 0.0024 | 66 | 0.8744 | 0.8816 | 0.0072 |
| 30 | 0.2520 | 0.2539 | 0.0019 | 67 | 0.8833 | 0.8905 | 0.0072 |
| 31 | 0.2741 | 0.2752 | 0.0011 | 68 | 0.8918 | 0.8984 | 0.0066 |
| 32 | 0.2954 | 0.2963 | 0.0009 | 69 | 0.9000 | 0.9057 | 0.0057 |
| 33 | 0.3160 | 0.3172 | 0.0012 | 70 | 0.9045 | 0.9115 | 0.0070 |
| 34 | 0.3359 | 0.3377 | 0.0018 | | | | |
| 35 | 0.3553 | 0.3580 | 0.0027 | | | | |
| 36 | 0.3745 | 0.3774 | 0.0029 | | | | |

TABLA VI-3-B

| | | | | Fe1A251 | | | |
|---------|--------|--------|-----------|---------|--------|--------|-----------|
| Número | FeR1 | FeR2 | FeR1-FeR2 | Número | FeR1 | FeR2 | FeR1-FeR2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.4190 | 0.4019 | 0.0171 |
| 1 | 0.0052 | 0.0055 | 0.0003 | 38 | 0.4370 | 0.4194 | 0.0176 |
| 2 | 0.0154 | 0.0164 | 0.0010 | 39 | 0.4545 | 0.4367 | 0.0178 |
| 3 | 0.0259 | 0.0271 | 0.0012 | 40 | 0.4717 | 0.4534 | 0.0183 |
| 4 | 0.0367 | 0.0376 | 0.0009 | 41 | 0.4880 | 0.4697 | 0.0183 |
| 5 | 0.0471 | 0.0476 | 0.0005 | 42 | 0.5038 | 0.4858 | 0.0180 |
| 6 | 0.0574 | 0.0574 | 0.0000 | 43 | 0.5194 | 0.5012 | 0.0182 |
| 7 | 0.0677 | 0.0668 | 0.0009 | 44 | 0.5346 | 0.5162 | 0.0184 |
| 8 | 0.0775 | 0.0763 | 0.0012 | 45 | 0.5496 | 0.5309 | 0.0187 |
| 9 | 0.0873 | 0.0859 | 0.0014 | 46 | 0.5782 | 0.5583 | 0.0199 |
| 10 | 0.0969 | 0.0953 | 0.0016 | 47 | 0.6040 | 0.5855 | 0.0185 |
| 11 | 0.1064 | 0.1042 | 0.0022 | 48 | 0.6264 | 0.6113 | 0.0151 |
| 12 | 0.1159 | 0.1128 | 0.0031 | 49 | 0.6474 | 0.6352 | 0.0122 |
| 13 | 0.1249 | 0.1212 | 0.0037 | 50 | 0.6691 | 0.6575 | 0.0116 |
| 14 | 0.1341 | 0.1299 | 0.0042 | 51 | 0.6890 | 0.6782 | 0.0108 |
| 15 | 0.1437 | 0.1380 | 0.0049 | 52 | 0.7073 | 0.6979 | 0.0094 |
| 16 | 0.1531 | 0.1476 | 0.0055 | 53 | 0.7262 | 0.7164 | 0.0098 |
| 17 | 0.1619 | 0.1560 | 0.0059 | 54 | 0.7427 | 0.7334 | 0.0093 |
| 18 | 0.1706 | 0.1643 | 0.0063 | 55 | 0.7575 | 0.7489 | 0.0086 |
| 19 | 0.1792 | 0.1726 | 0.0066 | 56 | 0.7721 | 0.7628 | 0.0093 |
| 20 | 0.1879 | 0.1810 | 0.0069 | 57 | 0.7856 | 0.7757 | 0.0099 |
| 21 | 0.1967 | 0.1895 | 0.0072 | 58 | 0.7986 | 0.7878 | 0.0108 |
| 22 | 0.2054 | 0.1978 | 0.0076 | 59 | 0.8095 | 0.7989 | 0.0106 |
| 23 | 0.2141 | 0.2060 | 0.0081 | 60 | 0.8185 | 0.8091 | 0.0094 |
| 24 | 0.2226 | 0.2142 | 0.0084 | 61 | 0.8282 | 0.8188 | 0.0094 |
| 25 | 0.2307 | 0.2225 | 0.0084 | 62 | 0.8380 | 0.8278 | 0.0102 |
| 26 | 0.2389 | 0.2305 | 0.0084 | 63 | 0.8469 | 0.8359 | 0.0110 |
| 27 | 0.2470 | 0.2384 | 0.0086 | 64 | 0.8552 | 0.8435 | 0.0117 |
| 28 | 0.2551 | 0.2463 | 0.0088 | 65 | 0.8625 | 0.8511 | 0.0114 |
| 29 | 0.2630 | 0.2541 | 0.0089 | 66 | 0.8691 | 0.8589 | 0.0102 |
| 30 | 0.2708 | 0.2616 | 0.0092 | 67 | 0.8751 | 0.8660 | 0.0091 |
| 31 | 0.2791 | 0.2688 | 0.0103 | 68 | 0.8807 | 0.8730 | 0.0077 |
| 32 | 0.3164 | 0.3051 | 0.0113 | 69 | 0.8861 | 0.8798 | 0.0063 |
| 33 | 0.3381 | 0.3257 | 0.0124 | 70 | 0.8902 | 0.8857 | 0.0045 |
| 34 | 0.3598 | 0.3461 | 0.0137 | | | | |
| 35 | 0.3801 | 0.3657 | 0.0144 | | | | |
| 36 | 0.3997 | 0.3843 | 0.0154 | | | | |

TABLA VI-4-B

| | | | | RelA252 | | | |
|---------|--------|--------|-----------|---------|--------|--------|-----------|
| Número | FeR1 | FeR2 | FeR1-FeR2 | Número | FeR1 | FeR2 | FeR1-FeR2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.3872 | 0.3782 | 0.0090 |
| 1 | 0.0047 | 0.0045 | 0.0002 | 38 | 0.4049 | 0.3962 | 0.0087 |
| 2 | 0.0145 | 0.0134 | 0.0011 | 39 | 0.4218 | 0.4148 | 0.0070 |
| 3 | 0.0244 | 0.0225 | 0.0019 | 40 | 0.4383 | 0.4327 | 0.0056 |
| 4 | 0.0343 | 0.0317 | 0.0026 | 41 | 0.4550 | 0.4486 | 0.0064 |
| 5 | 0.0436 | 0.0407 | 0.0029 | 42 | 0.4715 | 0.4636 | 0.0079 |
| 6 | 0.0527 | 0.0498 | 0.0029 | 43 | 0.4871 | 0.4783 | 0.0088 |
| 7 | 0.0619 | 0.0589 | 0.0030 | 44 | 0.5015 | 0.4934 | 0.0081 |
| 8 | 0.0713 | 0.0675 | 0.0038 | 45 | 0.5156 | 0.5084 | 0.0072 |
| 9 | 0.0807 | 0.0760 | 0.0047 | 46 | 0.5433 | 0.5372 | 0.0061 |
| 10 | 0.0896 | 0.0849 | 0.0047 | 47 | 0.5689 | 0.5644 | 0.0045 |
| 11 | 0.0986 | 0.0936 | 0.0050 | 48 | 0.5930 | 0.5900 | 0.0030 |
| 12 | 0.1073 | 0.1021 | 0.0052 | 49 | 0.6167 | 0.6145 | 0.0022 |
| 13 | 0.1153 | 0.1102 | 0.0051 | 50 | 0.6387 | 0.6370 | 0.0017 |
| 14 | 0.1234 | 0.1184 | 0.0050 | 51 | 0.6590 | 0.6576 | 0.0014 |
| 15 | 0.1316 | 0.1267 | 0.0049 | 52 | 0.6790 | 0.6770 | 0.0020 |
| 16 | 0.1397 | 0.1350 | 0.0047 | 53 | 0.6976 | 0.6952 | 0.0024 |
| 17 | 0.1477 | 0.1434 | 0.0043 | 54 | 0.7145 | 0.7123 | 0.0022 |
| 18 | 0.1554 | 0.1516 | 0.0038 | 55 | 0.7307 | 0.7277 | 0.0030 |
| 19 | 0.1633 | 0.1596 | 0.0037 | 56 | 0.7460 | 0.7426 | 0.0034 |
| 20 | 0.1713 | 0.1675 | 0.0038 | 57 | 0.7610 | 0.7572 | 0.0038 |
| 21 | 0.1790 | 0.1752 | 0.0038 | 58 | 0.7756 | 0.7708 | 0.0048 |
| 22 | 0.1866 | 0.1827 | 0.0039 | 59 | 0.7889 | 0.7836 | 0.0053 |
| 23 | 0.1944 | 0.1906 | 0.0038 | 60 | 0.8015 | 0.7959 | 0.0056 |
| 24 | 0.2022 | 0.1983 | 0.0039 | 61 | 0.8140 | 0.8074 | 0.0066 |
| 25 | 0.2099 | 0.2061 | 0.0038 | 62 | 0.8257 | 0.8178 | 0.0079 |
| 26 | 0.2175 | 0.2139 | 0.0036 | 63 | 0.8362 | 0.8282 | 0.0080 |
| 27 | 0.2250 | 0.2215 | 0.0035 | 64 | 0.8459 | 0.8380 | 0.0079 |
| 28 | 0.2322 | 0.2291 | 0.0031 | 65 | 0.8553 | 0.8461 | 0.0092 |
| 29 | 0.2395 | 0.2361 | 0.0034 | 66 | 0.8640 | 0.8538 | 0.0102 |
| 30 | 0.2471 | 0.2430 | 0.0041 | 67 | 0.8724 | 0.8617 | 0.0107 |
| 31 | 0.2695 | 0.2635 | 0.0060 | 68 | 0.8807 | 0.8692 | 0.0115 |
| 32 | 0.2905 | 0.2836 | 0.0069 | 69 | 0.8886 | 0.8766 | 0.0120 |
| 33 | 0.3103 | 0.3035 | 0.0068 | 70 | 0.8950 | 0.8819 | 0.0131 |
| 34 | 0.3296 | 0.3228 | 0.0068 | | | | |
| 35 | 0.3503 | 0.3418 | 0.0085 | | | | |
| 36 | 0.3696 | 0.3601 | 0.0095 | | | | |

TABLA VI-5-B

| Número | Re2A1S1 | | | Número | FeR1 | FeR2 | FeR1-FeR2 |
|---------|---------|--------|-----------|--------|--------|--------|-----------|
| | FeR1 | FeR2 | FeR1-FeR2 | | | | |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.4513 | 0.4444 | 0.0069 |
| 1 | 0.0120 | 0.0060 | 0.0060 | 38 | 0.4691 | 0.4616 | 0.0075 |
| 2 | 0.0237 | 0.0177 | 0.0060 | 39 | 0.4865 | 0.4784 | 0.0081 |
| 3 | 0.0349 | 0.0289 | 0.0060 | 40 | 0.5036 | 0.4947 | 0.0089 |
| 4 | 0.0462 | 0.0402 | 0.0060 | 41 | 0.5199 | 0.5110 | 0.0089 |
| 5 | 0.0575 | 0.0515 | 0.0060 | 42 | 0.5356 | 0.5265 | 0.0091 |
| 6 | 0.0686 | 0.0626 | 0.0060 | 43 | 0.5512 | 0.5416 | 0.0096 |
| 7 | 0.0795 | 0.0735 | 0.0060 | 44 | 0.5659 | 0.5563 | 0.0096 |
| 8 | 0.0903 | 0.0843 | 0.0060 | 45 | 0.5801 | 0.5703 | 0.0098 |
| 9 | 0.1008 | 0.0947 | 0.0061 | 46 | 0.6075 | 0.5974 | 0.0101 |
| 10 | 0.1113 | 0.1053 | 0.0060 | 47 | 0.6330 | 0.6228 | 0.0102 |
| 11 | 0.1220 | 0.1160 | 0.0060 | 48 | 0.6557 | 0.6473 | 0.0084 |
| 12 | 0.1326 | 0.1264 | 0.0062 | 49 | 0.6761 | 0.6706 | 0.0055 |
| 13 | 0.1431 | 0.1367 | 0.0064 | 50 | 0.6957 | 0.6910 | 0.0047 |
| 14 | 0.1536 | 0.1471 | 0.0065 | 51 | 0.7148 | 0.7099 | 0.0049 |
| 15 | 0.1639 | 0.1575 | 0.0064 | 52 | 0.7328 | 0.7281 | 0.0047 |
| 16 | 0.1740 | 0.1677 | 0.0063 | 53 | 0.7495 | 0.7442 | 0.0053 |
| 17 | 0.1840 | 0.1777 | 0.0063 | 54 | 0.7655 | 0.7586 | 0.0069 |
| 18 | 0.1939 | 0.1876 | 0.0063 | 55 | 0.7797 | 0.7734 | 0.0063 |
| 19 | 0.2038 | 0.1975 | 0.0063 | 56 | 0.7929 | 0.7878 | 0.0051 |
| 20 | 0.2137 | 0.2074 | 0.0063 | 57 | 0.8059 | 0.8017 | 0.0042 |
| 21 | 0.2234 | 0.2171 | 0.0063 | 58 | 0.8183 | 0.8153 | 0.0030 |
| 22 | 0.2329 | 0.2267 | 0.0062 | 59 | 0.8293 | 0.8281 | 0.0012 |
| 23 | 0.2426 | 0.2363 | 0.0063 | 60 | 0.8391 | 0.8403 | 0.0012 |
| 24 | 0.2521 | 0.2458 | 0.0063 | 61 | 0.8485 | 0.8515 | 0.0030 |
| 25 | 0.2615 | 0.2552 | 0.0063 | 62 | 0.8576 | 0.8617 | 0.0041 |
| 26 | 0.2705 | 0.2642 | 0.0063 | 63 | 0.8662 | 0.8711 | 0.0049 |
| 27 | 0.2790 | 0.2730 | 0.0060 | 64 | 0.8740 | 0.8788 | 0.0048 |
| 28 | 0.2875 | 0.2819 | 0.0056 | 65 | 0.8813 | 0.8849 | 0.0036 |
| 29 | 0.2957 | 0.2906 | 0.0051 | 66 | 0.8878 | 0.8902 | 0.0024 |
| 30 | 0.3035 | 0.2989 | 0.0046 | 67 | 0.8923 | 0.8956 | 0.0033 |
| 31 | 0.3264 | 0.3227 | 0.0037 | 68 | 0.8966 | 0.9008 | 0.0042 |
| 32 | 0.3489 | 0.3451 | 0.0038 | 69 | 0.9017 | 0.9053 | 0.0036 |
| 33 | 0.3710 | 0.3664 | 0.0046 | 70 | 0.9065 | 0.9087 | 0.0022 |
| 34 | 0.3926 | 0.3870 | 0.0056 | | | | |
| 35 | 0.4132 | 0.4069 | 0.0063 | | | | |
| 36 | 0.4326 | 0.4263 | 0.0063 | | | | |

TABLA VI-6-B

| | | | | Re2AlS2 | | | |
|---------|--------|--------|-----------|---------|--------|--------|-----------|
| Número | FaR1 | FaR2 | FaR1-FaR2 | Número | FaR1 | FaR2 | FaR1-FaR2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.4417 | 0.4462 | 0.0045 |
| 1 | 0.0059 | 0.0056 | 0.0003 | 38 | 0.4604 | 0.4649 | 0.0045 |
| 2 | 0.0175 | 0.0169 | 0.0006 | 39 | 0.4781 | 0.4830 | 0.0049 |
| 3 | 0.0290 | 0.0281 | 0.0009 | 40 | 0.4953 | 0.5001 | 0.0048 |
| 4 | 0.0405 | 0.0388 | 0.0017 | 41 | 0.5123 | 0.5168 | 0.0045 |
| 5 | 0.0520 | 0.0495 | 0.0025 | 42 | 0.5285 | 0.5333 | 0.0048 |
| 6 | 0.0635 | 0.0601 | 0.0034 | 43 | 0.5437 | 0.5489 | 0.0052 |
| 7 | 0.0744 | 0.0707 | 0.0037 | 44 | 0.5583 | 0.5635 | 0.0052 |
| 8 | 0.0851 | 0.0813 | 0.0038 | 45 | 0.5721 | 0.5771 | 0.0050 |
| 9 | 0.0963 | 0.0919 | 0.0044 | 46 | 0.5977 | 0.6029 | 0.0052 |
| 10 | 0.1073 | 0.1025 | 0.0048 | 47 | 0.6226 | 0.6282 | 0.0056 |
| 11 | 0.1179 | 0.1130 | 0.0049 | 48 | 0.6462 | 0.6521 | 0.0059 |
| 12 | 0.1278 | 0.1231 | 0.0047 | 49 | 0.6686 | 0.6745 | 0.0059 |
| 13 | 0.1376 | 0.1333 | 0.0043 | 50 | 0.6895 | 0.6952 | 0.0057 |
| 14 | 0.1475 | 0.1440 | 0.0036 | 51 | 0.7084 | 0.7145 | 0.0061 |
| 15 | 0.1572 | 0.1545 | 0.0027 | 52 | 0.7261 | 0.7326 | 0.0065 |
| 16 | 0.1668 | 0.1645 | 0.0023 | 53 | 0.7430 | 0.7493 | 0.0063 |
| 17 | 0.1766 | 0.1742 | 0.0024 | 54 | 0.7589 | 0.7653 | 0.0064 |
| 18 | 0.1860 | 0.1833 | 0.0027 | 55 | 0.7725 | 0.7797 | 0.0072 |
| 19 | 0.1955 | 0.1924 | 0.0031 | 56 | 0.7850 | 0.7933 | 0.0083 |
| 20 | 0.2050 | 0.2016 | 0.0034 | 57 | 0.7975 | 0.8076 | 0.0101 |
| 21 | 0.2144 | 0.2116 | 0.0028 | 58 | 0.8102 | 0.8213 | 0.0111 |
| 22 | 0.2236 | 0.2219 | 0.0017 | 59 | 0.8229 | 0.8331 | 0.0102 |
| 23 | 0.2327 | 0.2316 | 0.0011 | 60 | 0.8346 | 0.8427 | 0.0081 |
| 24 | 0.2416 | 0.2410 | 0.0006 | 61 | 0.8461 | 0.8517 | 0.0056 |
| 25 | 0.2504 | 0.2507 | 0.0003 | 62 | 0.8570 | 0.8607 | 0.0037 |
| 26 | 0.2591 | 0.2605 | 0.0014 | 63 | 0.8661 | 0.8685 | 0.0024 |
| 27 | 0.2677 | 0.2703 | 0.0026 | 64 | 0.8736 | 0.8754 | 0.0018 |
| 28 | 0.2760 | 0.2800 | 0.0040 | 65 | 0.8808 | 0.8826 | 0.0018 |
| 29 | 0.2840 | 0.2890 | 0.0050 | 66 | 0.8878 | 0.8894 | 0.0016 |
| 30 | 0.2920 | 0.2975 | 0.0055 | 67 | 0.8941 | 0.8952 | 0.0011 |
| 31 | 0.3156 | 0.3215 | 0.0059 | 68 | 0.9005 | 0.9013 | 0.0008 |
| 32 | 0.3386 | 0.3443 | 0.0057 | 69 | 0.9069 | 0.9074 | 0.0005 |
| 33 | 0.3609 | 0.3662 | 0.0053 | 70 | 0.9121 | 0.9106 | 0.0015 |
| 34 | 0.3824 | 0.3873 | 0.0049 | | | | |
| 35 | 0.4030 | 0.4075 | 0.0045 | | | | |
| 36 | 0.4227 | 0.4271 | 0.0044 | | | | |

TABLA VI-7-B

| Número | | Re2h2S1 | | Número | | Re2h2S1 | |
|---------|--------|---------|-----------|--------|--------|---------|-----------|
| | FeR1 | FeR2 | FeR1-FeR2 | | FeR1 | FeR2 | FeR1-FeR2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.4911 | 0.4787 | 0.0124 |
| 1 | 0.0061 | 0.0060 | 0.0001 | 38 | 0.5107 | 0.4983 | 0.0124 |
| 2 | 0.0181 | 0.0180 | 0.0001 | 39 | 0.5292 | 0.5178 | 0.0114 |
| 3 | 0.0301 | 0.0296 | 0.0005 | 40 | 0.5464 | 0.5372 | 0.0092 |
| 4 | 0.0420 | 0.0411 | 0.0009 | 41 | 0.5627 | 0.5556 | 0.0071 |
| 5 | 0.0538 | 0.0526 | 0.0012 | 42 | 0.5781 | 0.5727 | 0.0054 |
| 6 | 0.0654 | 0.0639 | 0.0015 | 43 | 0.5930 | 0.5896 | 0.0034 |
| 7 | 0.0769 | 0.0753 | 0.0015 | 44 | 0.6075 | 0.6057 | 0.0018 |
| 8 | 0.0881 | 0.0865 | 0.0016 | 45 | 0.6217 | 0.6202 | 0.0015 |
| 9 | 0.0995 | 0.0974 | 0.0021 | 46 | 0.6499 | 0.6465 | 0.0034 |
| 10 | 0.1107 | 0.1083 | 0.0024 | 47 | 0.6760 | 0.6718 | 0.0042 |
| 11 | 0.1218 | 0.1194 | 0.0024 | 48 | 0.7001 | 0.6952 | 0.0049 |
| 12 | 0.1327 | 0.1304 | 0.0023 | 49 | 0.7215 | 0.7173 | 0.0042 |
| 13 | 0.1436 | 0.1414 | 0.0022 | 50 | 0.7405 | 0.7378 | 0.0027 |
| 14 | 0.1542 | 0.1524 | 0.0018 | 51 | 0.7585 | 0.7559 | 0.0026 |
| 15 | 0.1648 | 0.1632 | 0.0016 | 52 | 0.7747 | 0.7733 | 0.0014 |
| 16 | 0.1754 | 0.1739 | 0.0015 | 53 | 0.7888 | 0.7888 | 0.0000 |
| 17 | 0.1860 | 0.1844 | 0.0016 | 54 | 0.8021 | 0.8026 | 0.0005 |
| 18 | 0.1968 | 0.1948 | 0.0020 | 55 | 0.8145 | 0.8153 | 0.0008 |
| 19 | 0.2076 | 0.2052 | 0.0023 | 56 | 0.8253 | 0.8262 | 0.0009 |
| 20 | 0.2182 | 0.2156 | 0.0026 | 57 | 0.8351 | 0.8354 | 0.0003 |
| 21 | 0.2288 | 0.2256 | 0.0032 | 58 | 0.8446 | 0.8440 | 0.0006 |
| 22 | 0.2393 | 0.2352 | 0.0041 | 59 | 0.8532 | 0.8520 | 0.0012 |
| 23 | 0.2498 | 0.2447 | 0.0051 | 60 | 0.8608 | 0.8594 | 0.0014 |
| 24 | 0.2602 | 0.2543 | 0.0059 | 61 | 0.8676 | 0.8666 | 0.0010 |
| 25 | 0.2705 | 0.2638 | 0.0067 | 62 | 0.8740 | 0.8735 | 0.0005 |
| 26 | 0.2806 | 0.2730 | 0.0076 | 63 | 0.8801 | 0.8799 | 0.0002 |
| 27 | 0.2905 | 0.2821 | 0.0085 | 64 | 0.8854 | 0.8861 | 0.0007 |
| 28 | 0.3004 | 0.2915 | 0.0089 | 65 | 0.8903 | 0.8915 | 0.0012 |
| 29 | 0.3100 | 0.3012 | 0.0088 | 66 | 0.8951 | 0.8964 | 0.0013 |
| 30 | 0.3196 | 0.3106 | 0.0090 | 67 | 0.8993 | 0.9007 | 0.0014 |
| 31 | 0.3277 | 0.3276 | 0.0101 | 68 | 0.9028 | 0.9044 | 0.0016 |
| 32 | 0.3748 | 0.3635 | 0.0113 | 69 | 0.9060 | 0.9077 | 0.0017 |
| 33 | 0.4004 | 0.3885 | 0.0119 | 70 | 0.9082 | 0.9100 | 0.0018 |
| 34 | 0.4250 | 0.4126 | 0.0124 | | | | |
| 35 | 0.4486 | 0.4360 | 0.0126 | | | | |
| 36 | 0.4707 | 0.4583 | 0.0124 | | | | |

TABLA VI-B-B

| TABLA VI-B-B | | Re2A2S2 | | | | | |
|--------------|--------|---------|-----------|--------|--------|--------|-----------|
| Número | FeR1 | FeR2 | FeR1-FeR2 | Número | FeR1 | FeR2 | FeR1-FeR2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 37 | 0.4619 | 0.4490 | 0.0129 |
| 1 | 0.0057 | 0.0060 | 0.0003 | 38 | 0.4800 | 0.4668 | 0.0132 |
| 2 | 0.0172 | 0.0177 | 0.0005 | 39 | 0.4976 | 0.4847 | 0.0129 |
| 3 | 0.0288 | 0.0291 | 0.0003 | 40 | 0.5150 | 0.5023 | 0.0127 |
| 4 | 0.0406 | 0.0406 | 0.0000 | 41 | 0.5320 | 0.5192 | 0.0128 |
| 5 | 0.0523 | 0.0517 | 0.0006 | 42 | 0.5477 | 0.5350 | 0.0127 |
| 6 | 0.0639 | 0.0627 | 0.0012 | 43 | 0.5627 | 0.5502 | 0.0125 |
| 7 | 0.0753 | 0.0737 | 0.0016 | 44 | 0.5777 | 0.5648 | 0.0129 |
| 8 | 0.0864 | 0.0850 | 0.0014 | 45 | 0.5923 | 0.5785 | 0.0138 |
| 9 | 0.0976 | 0.0962 | 0.0014 | 46 | 0.6194 | 0.6043 | 0.0151 |
| 10 | 0.1088 | 0.1070 | 0.0018 | 47 | 0.6447 | 0.6288 | 0.0159 |
| 11 | 0.1195 | 0.1173 | 0.0022 | 48 | 0.6688 | 0.6525 | 0.0163 |
| 12 | 0.1301 | 0.1277 | 0.0024 | 49 | 0.6914 | 0.6754 | 0.0160 |
| 13 | 0.1404 | 0.1379 | 0.0025 | 50 | 0.7115 | 0.6961 | 0.0154 |
| 14 | 0.1504 | 0.1482 | 0.0022 | 51 | 0.7301 | 0.7142 | 0.0159 |
| 15 | 0.1605 | 0.1584 | 0.0021 | 52 | 0.7476 | 0.7307 | 0.0169 |
| 16 | 0.1703 | 0.1683 | 0.0020 | 53 | 0.7641 | 0.7471 | 0.0170 |
| 17 | 0.1800 | 0.1780 | 0.0020 | 54 | 0.7798 | 0.7632 | 0.0166 |
| 18 | 0.1896 | 0.1876 | 0.0020 | 55 | 0.7940 | 0.7784 | 0.0156 |
| 19 | 0.1993 | 0.1972 | 0.0021 | 56 | 0.8075 | 0.7925 | 0.0150 |
| 20 | 0.2089 | 0.2064 | 0.0025 | 57 | 0.8207 | 0.8055 | 0.0152 |
| 21 | 0.2183 | 0.2155 | 0.0028 | 58 | 0.8326 | 0.8170 | 0.0156 |
| 22 | 0.2277 | 0.2243 | 0.0034 | 59 | 0.8434 | 0.8275 | 0.0159 |
| 23 | 0.2370 | 0.2332 | 0.0038 | 60 | 0.8532 | 0.8374 | 0.0158 |
| 24 | 0.2464 | 0.2421 | 0.0043 | 61 | 0.8622 | 0.8469 | 0.0153 |
| 25 | 0.2559 | 0.2510 | 0.0049 | 62 | 0.8704 | 0.8557 | 0.0147 |
| 26 | 0.2653 | 0.2600 | 0.0053 | 63 | 0.8779 | 0.8635 | 0.0144 |
| 27 | 0.2744 | 0.2690 | 0.0054 | 64 | 0.8844 | 0.8710 | 0.0134 |
| 28 | 0.2835 | 0.2778 | 0.0057 | 65 | 0.8895 | 0.8778 | 0.0117 |
| 29 | 0.2923 | 0.2865 | 0.0058 | 66 | 0.8935 | 0.8834 | 0.0099 |
| 30 | 0.3009 | 0.2953 | 0.0056 | 67 | 0.8967 | 0.8884 | 0.0083 |
| 31 | 0.3267 | 0.3207 | 0.0060 | 68 | 0.8995 | 0.8922 | 0.0073 |
| 32 | 0.3517 | 0.3455 | 0.0062 | 69 | 0.9017 | 0.8955 | 0.0062 |
| 33 | 0.3756 | 0.3693 | 0.0063 | 70 | 0.9035 | 0.8978 | 0.0057 |
| 34 | 0.3982 | 0.3914 | 0.0068 | | | | |
| 35 | 0.4205 | 0.4118 | 0.0087 | | | | |
| 36 | 0.4421 | 0.4309 | 0.0112 | | | | |

La tercera serie de tablas corresponde al análisis estadístico aplicado al promedio de las frecuencias acumuladas de la prueba y su réplica (FoPROM) para ser comparado con los valores de la curva teórica.

A continuación se explica la nomenclatura de las columnas de esta serie de tablas:

Número = Número de frecuencias acumuladas.

F_e teor1 = Frecuencia teórica acumulada, calculada a partir de valores continuos (ec. IV-A7).

F_e teor2 = Frecuencia teórica acumulada, calculada a partir de valores discretos (ec. IV-A8).

F_ePROM = Promedio entre las frecuencias acumuladas de la prueba y su réplica.

DIF-A = Desviación para la prueba estadística
 $|F_{e \text{ teor2}} - F_{e \text{ PROM}}(a)|$.

A°1 = Desviación para la prueba estadística
 $|F_{e \text{ teor1}} - F_{e \text{ PROM}}(a-1)|$.

A°2 = Desviación para la prueba estadística
 $|F_{e \text{ teor1}} - F_{e \text{ PROM}}(a)|$.

TABLA VI-1-C

| Número | FePR0M | Fe teor1 | Re1A1S1R1R2 Fe teor2 | DIF A | Ao1 | Ao2 |
|---------|--------|----------|-------------------------|--------|--------|--------|
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0053 | 0.0108 | 0.0108 | 0.0056 | 0.0108 | 0.0056 |
| 2 | 0.0157 | 0.0215 | 0.0215 | 0.0058 | 0.0163 | 0.0058 |
| 3 | 0.0262 | 0.0321 | 0.0321 | 0.0060 | 0.0164 | 0.0060 |
| 4 | 0.0366 | 0.0426 | 0.0426 | 0.0060 | 0.0165 | 0.0060 |
| 5 | 0.0468 | 0.0530 | 0.0530 | 0.0062 | 0.0164 | 0.0062 |
| 6 | 0.0572 | 0.0633 | 0.0633 | 0.0061 | 0.0165 | 0.0061 |
| 7 | 0.0666 | 0.0734 | 0.0734 | 0.0068 | 0.0162 | 0.0068 |
| 8 | 0.0764 | 0.0835 | 0.0835 | 0.0071 | 0.0169 | 0.0071 |
| 9 | 0.0861 | 0.0934 | 0.0934 | 0.0073 | 0.0170 | 0.0073 |
| 10 | 0.0957 | 0.1032 | 0.1032 | 0.0075 | 0.0171 | 0.0075 |
| 11 | 0.1051 | 0.1129 | 0.1129 | 0.0078 | 0.0172 | 0.0078 |
| 12 | 0.1144 | 0.1225 | 0.1225 | 0.0081 | 0.0175 | 0.0081 |
| 13 | 0.1238 | 0.1320 | 0.1320 | 0.0082 | 0.0176 | 0.0082 |
| 14 | 0.1334 | 0.1414 | 0.1414 | 0.0081 | 0.0176 | 0.0081 |
| 15 | 0.1429 | 0.1507 | 0.1507 | 0.0079 | 0.0174 | 0.0079 |
| 16 | 0.1522 | 0.1599 | 0.1599 | 0.0077 | 0.0171 | 0.0077 |
| 17 | 0.1613 | 0.1690 | 0.1690 | 0.0078 | 0.0168 | 0.0078 |
| 18 | 0.1700 | 0.1780 | 0.1780 | 0.0081 | 0.0168 | 0.0081 |
| 19 | 0.1786 | 0.1869 | 0.1869 | 0.0084 | 0.0170 | 0.0084 |
| 20 | 0.1870 | 0.1958 | 0.1958 | 0.0088 | 0.0172 | 0.0088 |
| 21 | 0.1953 | 0.2045 | 0.2045 | 0.0092 | 0.0175 | 0.0092 |
| 22 | 0.2036 | 0.2131 | 0.2131 | 0.0095 | 0.0178 | 0.0095 |
| 23 | 0.2120 | 0.2216 | 0.2216 | 0.0097 | 0.0180 | 0.0097 |
| 24 | 0.2203 | 0.2300 | 0.2300 | 0.0098 | 0.0181 | 0.0098 |
| 25 | 0.2286 | 0.2384 | 0.2384 | 0.0098 | 0.0181 | 0.0098 |
| 26 | 0.2368 | 0.2466 | 0.2466 | 0.0098 | 0.0181 | 0.0098 |
| 27 | 0.2450 | 0.2548 | 0.2548 | 0.0098 | 0.0180 | 0.0098 |
| 28 | 0.2527 | 0.2629 | 0.2629 | 0.0102 | 0.0179 | 0.0102 |
| 29 | 0.2602 | 0.2709 | 0.2709 | 0.0107 | 0.0182 | 0.0107 |
| 30 | 0.2677 | 0.2788 | 0.2788 | 0.0110 | 0.0186 | 0.0110 |
| 31 | 0.2897 | 0.3019 | 0.3019 | 0.0123 | 0.0342 | 0.0122 |
| 32 | 0.3114 | 0.3244 | 0.3244 | 0.0129 | 0.0347 | 0.0129 |
| 33 | 0.3333 | 0.3461 | 0.3461 | 0.0128 | 0.0347 | 0.0128 |
| 34 | 0.3548 | 0.3671 | 0.3671 | 0.0124 | 0.0339 | 0.0123 |
| 35 | 0.3752 | 0.3875 | 0.3875 | 0.0122 | 0.0327 | 0.0122 |
| 36 | 0.3948 | 0.4072 | 0.4072 | 0.0124 | 0.0319 | 0.0123 |

TABLA VI-1-C
Número

| | continuación.. | | ReIAISIR1R2 | | Ao1 | Ao2 |
|----|----------------|----------|-------------|--------|--------|--------|
| | FeFROM | Fe teor1 | Fe teor2 | DIF-A | | |
| 37 | 0.4138 | 0.4262 | 0.4262 | 0.0125 | 0.0314 | 0.0125 |
| 38 | 0.4321 | 0.4447 | 0.4447 | 0.0126 | 0.0309 | 0.0126 |
| 39 | 0.4502 | 0.4625 | 0.4625 | 0.0123 | 0.0305 | 0.0123 |
| 40 | 0.4680 | 0.4798 | 0.4798 | 0.0118 | 0.0296 | 0.0118 |
| 41 | 0.4847 | 0.4965 | 0.4965 | 0.0118 | 0.0285 | 0.0118 |
| 42 | 0.5011 | 0.5127 | 0.5127 | 0.0116 | 0.0280 | 0.0116 |
| 43 | 0.5171 | 0.5284 | 0.5284 | 0.0113 | 0.0272 | 0.0113 |
| 44 | 0.5326 | 0.5435 | 0.5436 | 0.0109 | 0.0264 | 0.0109 |
| 45 | 0.5478 | 0.5582 | 0.5582 | 0.0104 | 0.0256 | 0.0104 |
| 46 | 0.5766 | 0.5862 | 0.5862 | 0.0096 | 0.0383 | 0.0096 |
| 47 | 0.6027 | 0.6123 | 0.6124 | 0.0097 | 0.0358 | 0.0096 |
| 48 | 0.6270 | 0.6369 | 0.6369 | 0.0100 | 0.0341 | 0.0099 |
| 49 | 0.6500 | 0.6598 | 0.6599 | 0.0099 | 0.0329 | 0.0098 |
| 50 | 0.6715 | 0.6814 | 0.6814 | 0.0099 | 0.0313 | 0.0099 |
| 51 | 0.6916 | 0.7015 | 0.7016 | 0.0100 | 0.0300 | 0.0099 |
| 52 | 0.7107 | 0.7204 | 0.7205 | 0.0098 | 0.0288 | 0.0098 |
| 53 | 0.7289 | 0.7381 | 0.7382 | 0.0093 | 0.0274 | 0.0092 |
| 54 | 0.7462 | 0.7547 | 0.7548 | 0.0085 | 0.0257 | 0.0084 |
| 55 | 0.7619 | 0.7702 | 0.7703 | 0.0083 | 0.0239 | 0.0082 |
| 56 | 0.7760 | 0.7847 | 0.7848 | 0.0088 | 0.0228 | 0.0087 |
| 57 | 0.7884 | 0.7983 | 0.7985 | 0.0100 | 0.0223 | 0.0099 |
| 58 | 0.8004 | 0.8111 | 0.8112 | 0.0108 | 0.0227 | 0.0107 |
| 59 | 0.8124 | 0.8231 | 0.8232 | 0.0108 | 0.0227 | 0.0106 |
| 60 | 0.8237 | 0.8342 | 0.8344 | 0.0106 | 0.0218 | 0.0105 |
| 61 | 0.8346 | 0.8447 | 0.8449 | 0.0103 | 0.0210 | 0.0102 |
| 62 | 0.8451 | 0.8546 | 0.8547 | 0.0096 | 0.0200 | 0.0094 |
| 63 | 0.8551 | 0.8638 | 0.8639 | 0.0088 | 0.0186 | 0.0087 |
| 64 | 0.8642 | 0.8724 | 0.8725 | 0.0083 | 0.0173 | 0.0082 |
| 65 | 0.8733 | 0.8804 | 0.8806 | 0.0073 | 0.0163 | 0.0072 |
| 66 | 0.8825 | 0.8880 | 0.8882 | 0.0057 | 0.0148 | 0.0056 |
| 67 | 0.8905 | 0.8951 | 0.8952 | 0.0047 | 0.0126 | 0.0046 |
| 68 | 0.8975 | 0.9017 | 0.9019 | 0.0044 | 0.0112 | 0.0043 |
| 69 | 0.9042 | 0.9080 | 0.9081 | 0.0039 | 0.0105 | 0.0037 |
| 70 | 0.9079 | 0.9138 | 0.9139 | 0.0060 | 0.0095 | 0.0059 |

TABLA VI-2-C

| Número | RelAIS2RIR2 | | | | | |
|---------|-------------|----------|----------|--------|--------|--------|
| | FaFROM | Fa teor1 | Fa teor2 | DIF-A | Ao1 | Ao2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0050 | 0.0108 | 0.0108 | 0.0058 | 0.0108 | 0.0058 |
| 2 | 0.0150 | 0.0215 | 0.0215 | 0.0066 | 0.0166 | 0.0066 |
| 3 | 0.0248 | 0.0321 | 0.0321 | 0.0074 | 0.0172 | 0.0074 |
| 4 | 0.0346 | 0.0426 | 0.0426 | 0.0080 | 0.0178 | 0.0080 |
| 5 | 0.0444 | 0.0530 | 0.0530 | 0.0086 | 0.0184 | 0.0086 |
| 6 | 0.0541 | 0.0633 | 0.0633 | 0.0092 | 0.0188 | 0.0092 |
| 7 | 0.0634 | 0.0734 | 0.0734 | 0.0100 | 0.0193 | 0.0100 |
| 8 | 0.0724 | 0.0835 | 0.0835 | 0.0111 | 0.0200 | 0.0111 |
| 9 | 0.0810 | 0.0934 | 0.0934 | 0.0124 | 0.0210 | 0.0124 |
| 10 | 0.0897 | 0.1032 | 0.1032 | 0.0135 | 0.0222 | 0.0135 |
| 11 | 0.0987 | 0.1129 | 0.1129 | 0.0142 | 0.0232 | 0.0142 |
| 12 | 0.1078 | 0.1225 | 0.1225 | 0.0147 | 0.0238 | 0.0147 |
| 13 | 0.1166 | 0.1320 | 0.1320 | 0.0154 | 0.0242 | 0.0154 |
| 14 | 0.1252 | 0.1414 | 0.1414 | 0.0162 | 0.0248 | 0.0162 |
| 15 | 0.1335 | 0.1507 | 0.1507 | 0.0172 | 0.0255 | 0.0172 |
| 16 | 0.1419 | 0.1599 | 0.1599 | 0.0180 | 0.0264 | 0.0180 |
| 17 | 0.1505 | 0.1690 | 0.1690 | 0.0186 | 0.0271 | 0.0186 |
| 18 | 0.1588 | 0.1780 | 0.1780 | 0.0193 | 0.0276 | 0.0193 |
| 19 | 0.1669 | 0.1869 | 0.1869 | 0.0200 | 0.0282 | 0.0200 |
| 20 | 0.1751 | 0.1958 | 0.1958 | 0.0207 | 0.0288 | 0.0207 |
| 21 | 0.1831 | 0.2045 | 0.2045 | 0.0214 | 0.0294 | 0.0214 |
| 22 | 0.1909 | 0.2131 | 0.2131 | 0.0221 | 0.0300 | 0.0221 |
| 23 | 0.1988 | 0.2216 | 0.2216 | 0.0228 | 0.0307 | 0.0228 |
| 24 | 0.2065 | 0.2300 | 0.2300 | 0.0235 | 0.0312 | 0.0235 |
| 25 | 0.2143 | 0.2384 | 0.2384 | 0.0240 | 0.0319 | 0.0240 |
| 26 | 0.2222 | 0.2466 | 0.2466 | 0.0244 | 0.0323 | 0.0244 |
| 27 | 0.2299 | 0.2548 | 0.2548 | 0.0249 | 0.0326 | 0.0249 |
| 28 | 0.2375 | 0.2629 | 0.2629 | 0.0253 | 0.0330 | 0.0253 |
| 29 | 0.2453 | 0.2709 | 0.2709 | 0.0256 | 0.0333 | 0.0256 |
| 30 | 0.2529 | 0.2788 | 0.2788 | 0.0258 | 0.0335 | 0.0258 |
| 31 | 0.2747 | 0.3019 | 0.3019 | 0.0273 | 0.0490 | 0.0273 |
| 32 | 0.2959 | 0.3244 | 0.3244 | 0.0285 | 0.0497 | 0.0285 |
| 33 | 0.3166 | 0.3461 | 0.3461 | 0.0295 | 0.0502 | 0.0295 |
| 34 | 0.3368 | 0.3671 | 0.3671 | 0.0304 | 0.0505 | 0.0303 |
| 35 | 0.3566 | 0.3875 | 0.3875 | 0.0308 | 0.0507 | 0.0308 |
| 36 | 0.3759 | 0.4072 | 0.4072 | 0.0312 | 0.0505 | 0.0312 |

TABLA VI-2-C
Número

| | continuación.. | | Re1A192R1R2 | | | Ao1 | Ao2 |
|----|----------------|----------|-------------|--------|--|--------|--------|
| | FaFROM | Fa teor1 | Fa teor2 | DIF-A | | | |
| 37 | 0.3943 | 0.4262 | 0.4262 | 0.0319 | | 0.0503 | 0.0319 |
| 38 | 0.4119 | 0.4447 | 0.4447 | 0.0328 | | 0.0504 | 0.0327 |
| 39 | 0.4294 | 0.4625 | 0.4625 | 0.0331 | | 0.0506 | 0.0331 |
| 40 | 0.4464 | 0.4798 | 0.4798 | 0.0334 | | 0.0504 | 0.0334 |
| 41 | 0.4626 | 0.4965 | 0.4965 | 0.0340 | | 0.0501 | 0.0340 |
| 42 | 0.4780 | 0.5127 | 0.5127 | 0.0347 | | 0.0501 | 0.0347 |
| 43 | 0.4931 | 0.5284 | 0.5284 | 0.0353 | | 0.0504 | 0.0352 |
| 44 | 0.5078 | 0.5435 | 0.5436 | 0.0358 | | 0.0504 | 0.0357 |
| 45 | 0.5221 | 0.5582 | 0.5582 | 0.0362 | | 0.0504 | 0.0362 |
| 46 | 0.5495 | 0.5862 | 0.5862 | 0.0367 | | 0.0641 | 0.0366 |
| 47 | 0.5749 | 0.6123 | 0.6124 | 0.0374 | | 0.0628 | 0.0374 |
| 48 | 0.5985 | 0.6369 | 0.6369 | 0.0384 | | 0.0619 | 0.0383 |
| 49 | 0.6212 | 0.6598 | 0.6599 | 0.0387 | | 0.0613 | 0.0386 |
| 50 | 0.6429 | 0.6814 | 0.6814 | 0.0385 | | 0.0601 | 0.0385 |
| 51 | 0.6633 | 0.7015 | 0.7016 | 0.0383 | | 0.0586 | 0.0382 |
| 52 | 0.6833 | 0.7204 | 0.7205 | 0.0372 | | 0.0571 | 0.0371 |
| 53 | 0.7026 | 0.7381 | 0.7382 | 0.0356 | | 0.0548 | 0.0355 |
| 54 | 0.7206 | 0.7547 | 0.7548 | 0.0342 | | 0.0521 | 0.0341 |
| 55 | 0.7381 | 0.7702 | 0.7703 | 0.0322 | | 0.0496 | 0.0321 |
| 56 | 0.7553 | 0.7847 | 0.7848 | 0.0296 | | 0.0467 | 0.0295 |
| 57 | 0.7712 | 0.7983 | 0.7985 | 0.0273 | | 0.0431 | 0.0271 |
| 58 | 0.7861 | 0.8111 | 0.8112 | 0.0251 | | 0.0399 | 0.0250 |
| 59 | 0.8000 | 0.8231 | 0.8232 | 0.0232 | | 0.0370 | 0.0230 |
| 60 | 0.8129 | 0.8342 | 0.8344 | 0.0214 | | 0.0342 | 0.0213 |
| 61 | 0.8251 | 0.8447 | 0.8449 | 0.0198 | | 0.0318 | 0.0196 |
| 62 | 0.8366 | 0.8546 | 0.8547 | 0.0181 | | 0.0295 | 0.0180 |
| 63 | 0.8476 | 0.8638 | 0.8639 | 0.0163 | | 0.0272 | 0.0161 |
| 64 | 0.8582 | 0.8724 | 0.8725 | 0.0143 | | 0.0248 | 0.0142 |
| 65 | 0.8683 | 0.8804 | 0.8806 | 0.0123 | | 0.0223 | 0.0121 |
| 66 | 0.8780 | 0.8880 | 0.8882 | 0.0102 | | 0.0197 | 0.0100 |
| 67 | 0.8869 | 0.8951 | 0.8952 | 0.0084 | | 0.0171 | 0.0082 |
| 68 | 0.8951 | 0.9017 | 0.9019 | 0.0068 | | 0.0149 | 0.0067 |
| 69 | 0.9029 | 0.9080 | 0.9081 | 0.0053 | | 0.0129 | 0.0051 |
| 70 | 0.9080 | 0.9138 | 0.9139 | 0.0059 | | 0.0109 | 0.0058 |

TABLA VI-3-C

| Número | RelA2SIR1R2 | | | | Ao1 | Ao2 |
|---------|-------------|----------|----------|--------|--------|--------|
| | FaFRON | Fa teor1 | Fa teor2 | DIF-A | | |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0053 | 0.0108 | 0.0108 | 0.0055 | 0.0108 | 0.0055 |
| 2 | 0.0159 | 0.0215 | 0.0215 | 0.0056 | 0.0162 | 0.0056 |
| 3 | 0.0265 | 0.0321 | 0.0321 | 0.0057 | 0.0162 | 0.0057 |
| 4 | 0.0371 | 0.0426 | 0.0426 | 0.0055 | 0.0161 | 0.0055 |
| 5 | 0.0474 | 0.0530 | 0.0530 | 0.0056 | 0.0159 | 0.0056 |
| 6 | 0.0574 | 0.0633 | 0.0633 | 0.0059 | 0.0159 | 0.0059 |
| 7 | 0.0673 | 0.0734 | 0.0734 | 0.0061 | 0.0160 | 0.0061 |
| 8 | 0.0769 | 0.0835 | 0.0835 | 0.0065 | 0.0162 | 0.0065 |
| 9 | 0.0866 | 0.0934 | 0.0934 | 0.0068 | 0.0165 | 0.0068 |
| 10 | 0.0961 | 0.1032 | 0.1032 | 0.0071 | 0.0166 | 0.0071 |
| 11 | 0.1053 | 0.1129 | 0.1129 | 0.0076 | 0.0168 | 0.0076 |
| 12 | 0.1144 | 0.1225 | 0.1225 | 0.0082 | 0.0172 | 0.0082 |
| 13 | 0.1230 | 0.1320 | 0.1320 | 0.0090 | 0.0177 | 0.0090 |
| 14 | 0.1320 | 0.1414 | 0.1414 | 0.0095 | 0.0184 | 0.0095 |
| 15 | 0.1413 | 0.1507 | 0.1507 | 0.0095 | 0.0188 | 0.0095 |
| 16 | 0.1503 | 0.1599 | 0.1599 | 0.0096 | 0.0187 | 0.0096 |
| 17 | 0.1590 | 0.1690 | 0.1690 | 0.0101 | 0.0187 | 0.0101 |
| 18 | 0.1674 | 0.1780 | 0.1780 | 0.0106 | 0.0191 | 0.0106 |
| 19 | 0.1759 | 0.1869 | 0.1869 | 0.0110 | 0.0195 | 0.0110 |
| 20 | 0.1844 | 0.1958 | 0.1958 | 0.0113 | 0.0199 | 0.0113 |
| 21 | 0.1931 | 0.2045 | 0.2045 | 0.0114 | 0.0200 | 0.0114 |
| 22 | 0.2016 | 0.2131 | 0.2131 | 0.0115 | 0.0200 | 0.0115 |
| 23 | 0.2101 | 0.2216 | 0.2216 | 0.0116 | 0.0200 | 0.0116 |
| 24 | 0.2184 | 0.2300 | 0.2300 | 0.0116 | 0.0200 | 0.0116 |
| 25 | 0.2267 | 0.2384 | 0.2384 | 0.0117 | 0.0200 | 0.0117 |
| 26 | 0.2347 | 0.2466 | 0.2466 | 0.0119 | 0.0200 | 0.0119 |
| 27 | 0.2427 | 0.2548 | 0.2548 | 0.0121 | 0.0201 | 0.0121 |
| 28 | 0.2507 | 0.2629 | 0.2629 | 0.0122 | 0.0202 | 0.0122 |
| 29 | 0.2585 | 0.2709 | 0.2709 | 0.0123 | 0.0202 | 0.0123 |
| 30 | 0.2662 | 0.2788 | 0.2788 | 0.0126 | 0.0202 | 0.0126 |
| 31 | 0.2890 | 0.3019 | 0.3019 | 0.0130 | 0.0358 | 0.0130 |
| 32 | 0.3107 | 0.3244 | 0.3244 | 0.0136 | 0.0354 | 0.0136 |
| 33 | 0.3319 | 0.3461 | 0.3461 | 0.0142 | 0.0354 | 0.0142 |
| 34 | 0.3530 | 0.3671 | 0.3671 | 0.0142 | 0.0352 | 0.0142 |
| 35 | 0.3729 | 0.3875 | 0.3875 | 0.0146 | 0.0345 | 0.0146 |
| 36 | 0.3920 | 0.4072 | 0.4072 | 0.0152 | 0.0342 | 0.0152 |

TABLA VI-3-C
 Número

| | continuación.. | | Re1A2S1R1R2 | | | | |
|----|----------------|----------|-------------|--------|--------|--------|--|
| | FePRON | Fe teor1 | Fe teor2 | DIF-A | Ao1 | Ao2 | |
| 37 | 0.4104 | 0.4262 | 0.4262 | 0.0158 | 0.0342 | 0.0158 | |
| 38 | 0.4282 | 0.4447 | 0.4447 | 0.0165 | 0.0342 | 0.0165 | |
| 39 | 0.4456 | 0.4625 | 0.4625 | 0.0169 | 0.0343 | 0.0169 | |
| 40 | 0.4626 | 0.4798 | 0.4798 | 0.0173 | 0.0342 | 0.0172 | |
| 41 | 0.4788 | 0.4965 | 0.4965 | 0.0177 | 0.0340 | 0.0177 | |
| 42 | 0.4948 | 0.5127 | 0.5127 | 0.0179 | 0.0339 | 0.0179 | |
| 43 | 0.5103 | 0.5284 | 0.5284 | 0.0181 | 0.0336 | 0.0181 | |
| 44 | 0.5254 | 0.5435 | 0.5436 | 0.0182 | 0.0332 | 0.0181 | |
| 45 | 0.5402 | 0.5582 | 0.5582 | 0.0180 | 0.0326 | 0.0180 | |
| 46 | 0.5682 | 0.5862 | 0.5862 | 0.0180 | 0.0459 | 0.0179 | |
| 47 | 0.5947 | 0.6123 | 0.6124 | 0.0177 | 0.0441 | 0.0176 | |
| 48 | 0.6188 | 0.6369 | 0.6369 | 0.0181 | 0.0421 | 0.0180 | |
| 49 | 0.6413 | 0.6598 | 0.6599 | 0.0186 | 0.0410 | 0.0185 | |
| 50 | 0.6633 | 0.6814 | 0.6814 | 0.0181 | 0.0401 | 0.0181 | |
| 51 | 0.6836 | 0.7015 | 0.7016 | 0.0180 | 0.0382 | 0.0179 | |
| 52 | 0.7026 | 0.7204 | 0.7205 | 0.0179 | 0.0368 | 0.0178 | |
| 53 | 0.7213 | 0.7381 | 0.7382 | 0.0169 | 0.0355 | 0.0168 | |
| 54 | 0.7381 | 0.7547 | 0.7548 | 0.0167 | 0.0334 | 0.0166 | |
| 55 | 0.7532 | 0.7702 | 0.7703 | 0.0171 | 0.0321 | 0.0170 | |
| 56 | 0.7675 | 0.7847 | 0.7848 | 0.0174 | 0.0315 | 0.0173 | |
| 57 | 0.7807 | 0.7983 | 0.7985 | 0.0178 | 0.0309 | 0.0177 | |
| 58 | 0.7932 | 0.8111 | 0.8112 | 0.0180 | 0.0304 | 0.0179 | |
| 59 | 0.8042 | 0.8231 | 0.8232 | 0.0190 | 0.0299 | 0.0188 | |
| 60 | 0.8138 | 0.8342 | 0.8344 | 0.0206 | 0.0300 | 0.0204 | |
| 61 | 0.8235 | 0.8447 | 0.8449 | 0.0214 | 0.0309 | 0.0212 | |
| 62 | 0.8329 | 0.8546 | 0.8547 | 0.0218 | 0.0311 | 0.0217 | |
| 63 | 0.8414 | 0.8638 | 0.8639 | 0.0225 | 0.0309 | 0.0223 | |
| 64 | 0.8494 | 0.8724 | 0.8725 | 0.0232 | 0.0310 | 0.0230 | |
| 65 | 0.8568 | 0.8804 | 0.8806 | 0.0238 | 0.0311 | 0.0236 | |
| 66 | 0.8640 | 0.8880 | 0.8882 | 0.0242 | 0.0312 | 0.0240 | |
| 67 | 0.8705 | 0.8951 | 0.8952 | 0.0247 | 0.0311 | 0.0245 | |
| 68 | 0.8769 | 0.9017 | 0.9019 | 0.0250 | 0.0312 | 0.0249 | |
| 69 | 0.8829 | 0.9080 | 0.9081 | 0.0252 | 0.0311 | 0.0250 | |
| 70 | 0.8880 | 0.9138 | 0.9139 | 0.0260 | 0.0308 | 0.0258 | |

TABLA VI-4-C

| Número | RelA2S2R1R2 | | | | | |
|---------|-------------|----------|----------|--------|--------|--------|
| | FeFROM | Fe Leor1 | Fe Leor2 | DIF-A | Aa1 | Aa2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0046 | 0.0108 | 0.0108 | 0.0062 | 0.0108 | 0.0062 |
| 2 | 0.0139 | 0.0215 | 0.0215 | 0.0076 | 0.0169 | 0.0076 |
| 3 | 0.0235 | 0.0321 | 0.0321 | 0.0087 | 0.0182 | 0.0087 |
| 4 | 0.0330 | 0.0426 | 0.0426 | 0.0096 | 0.0192 | 0.0096 |
| 5 | 0.0422 | 0.0530 | 0.0530 | 0.0109 | 0.0200 | 0.0109 |
| 6 | 0.0512 | 0.0633 | 0.0633 | 0.0120 | 0.0211 | 0.0120 |
| 7 | 0.0604 | 0.0734 | 0.0734 | 0.0130 | 0.0222 | 0.0130 |
| 8 | 0.0694 | 0.0835 | 0.0835 | 0.0140 | 0.0230 | 0.0140 |
| 9 | 0.0784 | 0.0934 | 0.0934 | 0.0150 | 0.0240 | 0.0150 |
| 10 | 0.0873 | 0.1032 | 0.1032 | 0.0159 | 0.0248 | 0.0159 |
| 11 | 0.0961 | 0.1129 | 0.1129 | 0.0168 | 0.0257 | 0.0168 |
| 12 | 0.1047 | 0.1225 | 0.1225 | 0.0178 | 0.0264 | 0.0178 |
| 13 | 0.1128 | 0.1320 | 0.1320 | 0.0193 | 0.0273 | 0.0193 |
| 14 | 0.1209 | 0.1414 | 0.1414 | 0.0205 | 0.0287 | 0.0205 |
| 15 | 0.1291 | 0.1507 | 0.1507 | 0.0216 | 0.0298 | 0.0216 |
| 16 | 0.1373 | 0.1599 | 0.1599 | 0.0226 | 0.0308 | 0.0226 |
| 17 | 0.1455 | 0.1690 | 0.1690 | 0.0235 | 0.0317 | 0.0235 |
| 18 | 0.1535 | 0.1780 | 0.1780 | 0.0245 | 0.0325 | 0.0245 |
| 19 | 0.1614 | 0.1869 | 0.1869 | 0.0255 | 0.0334 | 0.0255 |
| 20 | 0.1694 | 0.1958 | 0.1958 | 0.0263 | 0.0343 | 0.0263 |
| 21 | 0.1771 | 0.2045 | 0.2045 | 0.0274 | 0.0351 | 0.0274 |
| 22 | 0.1847 | 0.2131 | 0.2131 | 0.0284 | 0.0360 | 0.0284 |
| 23 | 0.1925 | 0.2216 | 0.2216 | 0.0291 | 0.0369 | 0.0291 |
| 24 | 0.2002 | 0.2300 | 0.2300 | 0.0298 | 0.0375 | 0.0298 |
| 25 | 0.2080 | 0.2384 | 0.2384 | 0.0304 | 0.0382 | 0.0304 |
| 26 | 0.2157 | 0.2466 | 0.2466 | 0.0309 | 0.0387 | 0.0309 |
| 27 | 0.2233 | 0.2548 | 0.2548 | 0.0315 | 0.0391 | 0.0315 |
| 28 | 0.2307 | 0.2629 | 0.2629 | 0.0322 | 0.0396 | 0.0322 |
| 29 | 0.2378 | 0.2709 | 0.2709 | 0.0331 | 0.0402 | 0.0331 |
| 30 | 0.2451 | 0.2788 | 0.2788 | 0.0337 | 0.0410 | 0.0337 |
| 31 | 0.2665 | 0.3019 | 0.3019 | 0.0355 | 0.0569 | 0.0355 |
| 32 | 0.2870 | 0.3244 | 0.3244 | 0.0374 | 0.0579 | 0.0373 |
| 33 | 0.3069 | 0.3461 | 0.3461 | 0.0392 | 0.0591 | 0.0392 |
| 34 | 0.3262 | 0.3671 | 0.3671 | 0.0409 | 0.0602 | 0.0409 |
| 35 | 0.3461 | 0.3875 | 0.3875 | 0.0414 | 0.0613 | 0.0414 |
| 36 | 0.3649 | 0.4072 | 0.4072 | 0.0423 | 0.0611 | 0.0423 |

TABLA VI-4-C
Número

| | continuación.. | | ReJA2S2R1R2 | | Ao1 | Ao2 |
|----|----------------|----------|-------------|--------|--------|--------|
| | FePRON | Fe teor1 | Fe teor2 | DIF-A | | |
| 37 | 0.3827 | 0.4262 | 0.4262 | 0.0436 | 0.0614 | 0.0435 |
| 38 | 0.4005 | 0.4447 | 0.4447 | 0.0442 | 0.0620 | 0.0441 |
| 39 | 0.4183 | 0.4625 | 0.4625 | 0.0442 | 0.0620 | 0.0442 |
| 40 | 0.4355 | 0.4798 | 0.4798 | 0.0443 | 0.0615 | 0.0443 |
| 41 | 0.4518 | 0.4965 | 0.4965 | 0.0447 | 0.0610 | 0.0447 |
| 42 | 0.4675 | 0.5127 | 0.5127 | 0.0452 | 0.0609 | 0.0452 |
| 43 | 0.4827 | 0.5284 | 0.5284 | 0.0457 | 0.0609 | 0.0457 |
| 44 | 0.4975 | 0.5435 | 0.5436 | 0.0461 | 0.0609 | 0.0461 |
| 45 | 0.5120 | 0.5582 | 0.5582 | 0.0462 | 0.0607 | 0.0462 |
| 46 | 0.5403 | 0.5862 | 0.5862 | 0.0459 | 0.0742 | 0.0459 |
| 47 | 0.5667 | 0.6123 | 0.6124 | 0.0457 | 0.0721 | 0.0457 |
| 48 | 0.5915 | 0.6369 | 0.6369 | 0.0454 | 0.0702 | 0.0454 |
| 49 | 0.6156 | 0.6598 | 0.6599 | 0.0443 | 0.0683 | 0.0442 |
| 50 | 0.6379 | 0.6814 | 0.6814 | 0.0436 | 0.0658 | 0.0435 |
| 51 | 0.6583 | 0.7015 | 0.7016 | 0.0433 | 0.0637 | 0.0432 |
| 52 | 0.6780 | 0.7204 | 0.7205 | 0.0425 | 0.0621 | 0.0424 |
| 53 | 0.6964 | 0.7381 | 0.7382 | 0.0418 | 0.0601 | 0.0417 |
| 54 | 0.7134 | 0.7547 | 0.7548 | 0.0414 | 0.0582 | 0.0413 |
| 55 | 0.7292 | 0.7702 | 0.7703 | 0.0411 | 0.0568 | 0.0410 |
| 56 | 0.7443 | 0.7847 | 0.7848 | 0.0405 | 0.0555 | 0.0404 |
| 57 | 0.7591 | 0.7983 | 0.7985 | 0.0394 | 0.0540 | 0.0393 |
| 58 | 0.7732 | 0.8111 | 0.8112 | 0.0380 | 0.0520 | 0.0379 |
| 59 | 0.7862 | 0.8231 | 0.8232 | 0.0369 | 0.0498 | 0.0368 |
| 60 | 0.7987 | 0.8342 | 0.8344 | 0.0357 | 0.0480 | 0.0355 |
| 61 | 0.8107 | 0.8447 | 0.8449 | 0.0341 | 0.0460 | 0.0340 |
| 62 | 0.8217 | 0.8546 | 0.8547 | 0.0330 | 0.0438 | 0.0328 |
| 63 | 0.8322 | 0.8638 | 0.8639 | 0.0317 | 0.0420 | 0.0315 |
| 64 | 0.8420 | 0.8724 | 0.8725 | 0.0306 | 0.0402 | 0.0304 |
| 65 | 0.8507 | 0.8804 | 0.8806 | 0.0299 | 0.0385 | 0.0297 |
| 66 | 0.8589 | 0.8880 | 0.8882 | 0.0292 | 0.0373 | 0.0291 |
| 67 | 0.8671 | 0.8951 | 0.8952 | 0.0282 | 0.0362 | 0.0280 |
| 68 | 0.8750 | 0.9017 | 0.9019 | 0.0269 | 0.0347 | 0.0268 |
| 69 | 0.8826 | 0.9080 | 0.9081 | 0.0255 | 0.0330 | 0.0254 |
| 70 | 0.8885 | 0.9138 | 0.9139 | 0.0255 | 0.0312 | 0.0253 |

TABLA VI-5-C
Número

| | Re2A1S1R1R2 | | | | | |
|---------|-------------|----------|----------|--------|--------|--------|
| Número | FePRON | Fe teor1 | Fe teor2 | DIF-A | Ao1 | Ao2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0090 | 0.0108 | 0.0108 | 0.0018 | 0.0108 | 0.0018 |
| 2 | 0.0207 | 0.0215 | 0.0215 | 0.0009 | 0.0125 | 0.0009 |
| 3 | 0.0319 | 0.0321 | 0.0321 | 0.0002 | 0.0115 | 0.0002 |
| 4 | 0.0432 | 0.0426 | 0.0426 | 0.0006 | 0.0107 | 0.0006 |
| 5 | 0.0545 | 0.0530 | 0.0530 | 0.0015 | 0.0098 | 0.0015 |
| 6 | 0.0656 | 0.0633 | 0.0633 | 0.0023 | 0.0088 | 0.0023 |
| 7 | 0.0765 | 0.0734 | 0.0734 | 0.0031 | 0.0078 | 0.0031 |
| 8 | 0.0873 | 0.0835 | 0.0835 | 0.0038 | 0.0070 | 0.0038 |
| 9 | 0.0977 | 0.0934 | 0.0934 | 0.0043 | 0.0061 | 0.0043 |
| 10 | 0.1083 | 0.1032 | 0.1032 | 0.0051 | 0.0055 | 0.0051 |
| 11 | 0.1190 | 0.1129 | 0.1129 | 0.0061 | 0.0046 | 0.0061 |
| 12 | 0.1295 | 0.1225 | 0.1225 | 0.0070 | 0.0035 | 0.0070 |
| 13 | 0.1399 | 0.1320 | 0.1320 | 0.0079 | 0.0025 | 0.0079 |
| 14 | 0.1503 | 0.1414 | 0.1414 | 0.0089 | 0.0015 | 0.0089 |
| 15 | 0.1607 | 0.1507 | 0.1507 | 0.0099 | 0.0004 | 0.0099 |
| 16 | 0.1708 | 0.1599 | 0.1599 | 0.0109 | 0.0007 | 0.0109 |
| 17 | 0.1808 | 0.1690 | 0.1690 | 0.0118 | 0.0018 | 0.0118 |
| 18 | 0.1907 | 0.1780 | 0.1780 | 0.0127 | 0.0028 | 0.0127 |
| 19 | 0.2007 | 0.1869 | 0.1869 | 0.0137 | 0.0038 | 0.0137 |
| 20 | 0.2105 | 0.1958 | 0.1958 | 0.0148 | 0.0049 | 0.0148 |
| 21 | 0.2202 | 0.2045 | 0.2045 | 0.0158 | 0.0061 | 0.0158 |
| 22 | 0.2298 | 0.2131 | 0.2131 | 0.0167 | 0.0071 | 0.0167 |
| 23 | 0.2394 | 0.2216 | 0.2216 | 0.0178 | 0.0082 | 0.0178 |
| 24 | 0.2489 | 0.2300 | 0.2300 | 0.0189 | 0.0094 | 0.0189 |
| 25 | 0.2583 | 0.2384 | 0.2384 | 0.0200 | 0.0106 | 0.0200 |
| 26 | 0.2673 | 0.2466 | 0.2466 | 0.0207 | 0.0117 | 0.0207 |
| 27 | 0.2760 | 0.2548 | 0.2548 | 0.0212 | 0.0126 | 0.0212 |
| 28 | 0.2847 | 0.2629 | 0.2629 | 0.0218 | 0.0132 | 0.0218 |
| 29 | 0.2931 | 0.2709 | 0.2709 | 0.0223 | 0.0138 | 0.0223 |
| 30 | 0.3012 | 0.2788 | 0.2788 | 0.0224 | 0.0144 | 0.0225 |
| 31 | 0.3246 | 0.3019 | 0.3019 | 0.0226 | 0.0007 | 0.0226 |
| 32 | 0.3470 | 0.3244 | 0.3244 | 0.0226 | 0.0002 | 0.0226 |
| 33 | 0.3687 | 0.3461 | 0.3461 | 0.0226 | 0.0009 | 0.0226 |
| 34 | 0.3898 | 0.3671 | 0.3671 | 0.0227 | 0.0016 | 0.0227 |
| 35 | 0.4100 | 0.3875 | 0.3875 | 0.0226 | 0.0023 | 0.0226 |
| 36 | 0.4294 | 0.4072 | 0.4072 | 0.0223 | 0.0029 | 0.0223 |

TABLA VI-5-C
Número

| | continuación.. | | Re2A1S1R1R2 | | | |
|----|----------------|----------|-------------|--------|--------|--------|
| | FePR0M | Fe teor1 | Fe teor2 | DIF-A | Ao1 | Ao2 |
| 37 | 0.4479 | 0.4262 | 0.4262 | 0.0216 | 0.0032 | 0.0217 |
| 38 | 0.4654 | 0.4447 | 0.4447 | 0.0207 | 0.0032 | 0.0207 |
| 39 | 0.4824 | 0.4625 | 0.4625 | 0.0199 | 0.0029 | 0.0199 |
| 40 | 0.4991 | 0.4798 | 0.4798 | 0.0193 | 0.0026 | 0.0193 |
| 41 | 0.5154 | 0.4965 | 0.4965 | 0.0189 | 0.0026 | 0.0189 |
| 42 | 0.5311 | 0.5127 | 0.5127 | 0.0183 | 0.0027 | 0.0184 |
| 43 | 0.5464 | 0.5284 | 0.5284 | 0.0180 | 0.0027 | 0.0180 |
| 44 | 0.5611 | 0.5435 | 0.5436 | 0.0175 | 0.0028 | 0.0176 |
| 45 | 0.5752 | 0.5582 | 0.5582 | 0.0170 | 0.0029 | 0.0170 |
| 46 | 0.6025 | 0.5862 | 0.5862 | 0.0163 | 0.0110 | 0.0163 |
| 47 | 0.6279 | 0.6123 | 0.6124 | 0.0155 | 0.0099 | 0.0155 |
| 48 | 0.6515 | 0.6369 | 0.6369 | 0.0146 | 0.0090 | 0.0146 |
| 49 | 0.6734 | 0.6598 | 0.6599 | 0.0135 | 0.0083 | 0.0135 |
| 50 | 0.6923 | 0.6814 | 0.6814 | 0.0119 | 0.0080 | 0.0120 |
| 51 | 0.7123 | 0.7015 | 0.7016 | 0.0107 | 0.0082 | 0.0108 |
| 52 | 0.7304 | 0.7204 | 0.7205 | 0.0099 | 0.0081 | 0.0100 |
| 53 | 0.7469 | 0.7381 | 0.7382 | 0.0087 | 0.0077 | 0.0088 |
| 54 | 0.7621 | 0.7547 | 0.7548 | 0.0073 | 0.0078 | 0.0074 |
| 55 | 0.7765 | 0.7702 | 0.7703 | 0.0062 | 0.0081 | 0.0063 |
| 56 | 0.7903 | 0.7847 | 0.7848 | 0.0055 | 0.0082 | 0.0056 |
| 57 | 0.8038 | 0.7983 | 0.7985 | 0.0054 | 0.0080 | 0.0055 |
| 58 | 0.8168 | 0.8111 | 0.8112 | 0.0056 | 0.0073 | 0.0057 |
| 59 | 0.8287 | 0.8231 | 0.8232 | 0.0055 | 0.0062 | 0.0057 |
| 60 | 0.8397 | 0.8342 | 0.8344 | 0.0053 | 0.0055 | 0.0055 |
| 61 | 0.8500 | 0.8447 | 0.8449 | 0.0052 | 0.0050 | 0.0053 |
| 62 | 0.8597 | 0.8546 | 0.8547 | 0.0050 | 0.0045 | 0.0051 |
| 63 | 0.8686 | 0.8630 | 0.8639 | 0.0047 | 0.0041 | 0.0049 |
| 64 | 0.8764 | 0.8724 | 0.8725 | 0.0039 | 0.0037 | 0.0040 |
| 65 | 0.8831 | 0.8804 | 0.8806 | 0.0025 | 0.0040 | 0.0027 |
| 66 | 0.8890 | 0.8880 | 0.8882 | 0.0008 | 0.0049 | 0.0010 |
| 67 | 0.8940 | 0.8951 | 0.8952 | 0.0013 | 0.0061 | 0.0011 |
| 68 | 0.8987 | 0.9017 | 0.9019 | 0.0032 | 0.0078 | 0.0030 |
| 69 | 0.9035 | 0.9080 | 0.9081 | 0.0046 | 0.0092 | 0.0044 |
| 70 | 0.9076 | 0.9138 | 0.9139 | 0.0064 | 0.0103 | 0.0062 |

TABLA VI-6-C

| Número | Re2A1S2R1R2 | | | | Ao1 | Ao2 |
|---------|-------------|----------|----------|--------|--------|--------|
| | FePRDM | Fe teor1 | Fe teor2 | DIF-A | | |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0057 | 0.0108 | 0.0108 | 0.0051 | 0.0108 | 0.0051 |
| 2 | 0.0172 | 0.0215 | 0.0215 | 0.0043 | 0.0158 | 0.0043 |
| 3 | 0.0286 | 0.0321 | 0.0321 | 0.0036 | 0.0149 | 0.0036 |
| 4 | 0.0396 | 0.0426 | 0.0426 | 0.0030 | 0.0141 | 0.0030 |
| 5 | 0.0508 | 0.0530 | 0.0530 | 0.0022 | 0.0134 | 0.0022 |
| 6 | 0.0618 | 0.0633 | 0.0633 | 0.0015 | 0.0125 | 0.0015 |
| 7 | 0.0725 | 0.0734 | 0.0734 | 0.0009 | 0.0116 | 0.0009 |
| 8 | 0.0832 | 0.0835 | 0.0835 | 0.0002 | 0.0109 | 0.0002 |
| 9 | 0.0941 | 0.0934 | 0.0934 | 0.0007 | 0.0102 | 0.0007 |
| 10 | 0.1049 | 0.1032 | 0.1032 | 0.0017 | 0.0091 | 0.0017 |
| 11 | 0.1154 | 0.1129 | 0.1129 | 0.0025 | 0.0080 | 0.0025 |
| 12 | 0.1255 | 0.1225 | 0.1225 | 0.0029 | 0.0071 | 0.0029 |
| 13 | 0.1354 | 0.1320 | 0.1320 | 0.0034 | 0.0066 | 0.0034 |
| 14 | 0.1458 | 0.1414 | 0.1414 | 0.0044 | 0.0060 | 0.0044 |
| 15 | 0.1559 | 0.1507 | 0.1507 | 0.0051 | 0.0049 | 0.0051 |
| 16 | 0.1656 | 0.1599 | 0.1599 | 0.0057 | 0.0041 | 0.0057 |
| 17 | 0.1754 | 0.1690 | 0.1690 | 0.0064 | 0.0034 | 0.0064 |
| 18 | 0.1847 | 0.1780 | 0.1780 | 0.0066 | 0.0026 | 0.0066 |
| 19 | 0.1940 | 0.1869 | 0.1869 | 0.0070 | 0.0023 | 0.0070 |
| 20 | 0.2033 | 0.1958 | 0.1958 | 0.0076 | 0.0018 | 0.0076 |
| 21 | 0.2130 | 0.2045 | 0.2045 | 0.0085 | 0.0011 | 0.0085 |
| 22 | 0.2227 | 0.2131 | 0.2131 | 0.0097 | 0.0001 | 0.0097 |
| 23 | 0.2321 | 0.2216 | 0.2216 | 0.0105 | 0.0011 | 0.0105 |
| 24 | 0.2413 | 0.2300 | 0.2300 | 0.0113 | 0.0021 | 0.0113 |
| 25 | 0.2506 | 0.2384 | 0.2384 | 0.0122 | 0.0029 | 0.0122 |
| 26 | 0.2598 | 0.2466 | 0.2466 | 0.0131 | 0.0039 | 0.0131 |
| 27 | 0.2690 | 0.2548 | 0.2548 | 0.0142 | 0.0050 | 0.0142 |
| 28 | 0.2780 | 0.2629 | 0.2629 | 0.0151 | 0.0061 | 0.0152 |
| 29 | 0.2865 | 0.2709 | 0.2709 | 0.0157 | 0.0072 | 0.0157 |
| 30 | 0.2947 | 0.2788 | 0.2788 | 0.0160 | 0.0078 | 0.0160 |
| 31 | 0.3186 | 0.3019 | 0.3019 | 0.0166 | 0.0072 | 0.0166 |
| 32 | 0.3414 | 0.3244 | 0.3244 | 0.0171 | 0.0058 | 0.0171 |
| 33 | 0.3635 | 0.3461 | 0.3461 | 0.0174 | 0.0047 | 0.0174 |
| 34 | 0.3848 | 0.3671 | 0.3671 | 0.0177 | 0.0036 | 0.0177 |
| 35 | 0.4052 | 0.3875 | 0.3875 | 0.0177 | 0.0026 | 0.0178 |
| 36 | 0.4249 | 0.4072 | 0.4072 | 0.0177 | 0.0019 | 0.0177 |

TABLA VI-6-C
Número

| | continuación.. | | Re2A1S2R1R2 | | | Ao1 | Ao2 |
|----|----------------|----------|-------------|--------|--|--------|--------|
| | FeFROM | Fe teor1 | Fe teor2 | DIF-A | | | |
| 37 | 0.4440 | 0.4262 | 0.4262 | 0.0177 | | 0.0013 | 0.0177 |
| 38 | 0.4626 | 0.4447 | 0.4447 | 0.0180 | | 0.0007 | 0.0180 |
| 39 | 0.4806 | 0.4625 | 0.4625 | 0.0180 | | 0.0001 | 0.0181 |
| 40 | 0.4977 | 0.4798 | 0.4798 | 0.0179 | | 0.0008 | 0.0179 |
| 41 | 0.5146 | 0.4965 | 0.4965 | 0.0180 | | 0.0012 | 0.0180 |
| 42 | 0.5309 | 0.5127 | 0.5127 | 0.0182 | | 0.0018 | 0.0182 |
| 43 | 0.5463 | 0.5284 | 0.5284 | 0.0179 | | 0.0025 | 0.0179 |
| 44 | 0.5609 | 0.5435 | 0.5436 | 0.0173 | | 0.0028 | 0.0174 |
| 45 | 0.5746 | 0.5582 | 0.5582 | 0.0164 | | 0.0027 | 0.0164 |
| 46 | 0.6003 | 0.5862 | 0.5862 | 0.0141 | | 0.0116 | 0.0141 |
| 47 | 0.6254 | 0.6123 | 0.6124 | 0.0130 | | 0.0121 | 0.0131 |
| 48 | 0.6491 | 0.6369 | 0.6369 | 0.0122 | | 0.0115 | 0.0123 |
| 49 | 0.6715 | 0.6598 | 0.6599 | 0.0116 | | 0.0107 | 0.0117 |
| 50 | 0.6923 | 0.6814 | 0.6814 | 0.0109 | | 0.0098 | 0.0110 |
| 51 | 0.7114 | 0.7015 | 0.7016 | 0.0098 | | 0.0092 | 0.0099 |
| 52 | 0.7293 | 0.7204 | 0.7205 | 0.0088 | | 0.0090 | 0.0089 |
| 53 | 0.7462 | 0.7381 | 0.7382 | 0.0080 | | 0.0088 | 0.0081 |
| 54 | 0.7621 | 0.7547 | 0.7548 | 0.0074 | | 0.0085 | 0.0075 |
| 55 | 0.7761 | 0.7702 | 0.7703 | 0.0058 | | 0.0081 | 0.0059 |
| 56 | 0.7892 | 0.7847 | 0.7848 | 0.0043 | | 0.0086 | 0.0045 |
| 57 | 0.8025 | 0.7983 | 0.7985 | 0.0041 | | 0.0092 | 0.0042 |
| 58 | 0.8157 | 0.8111 | 0.8112 | 0.0045 | | 0.0086 | 0.0046 |
| 59 | 0.8280 | 0.8231 | 0.8232 | 0.0048 | | 0.0073 | 0.0049 |
| 60 | 0.8386 | 0.8342 | 0.8344 | 0.0043 | | 0.0063 | 0.0044 |
| 61 | 0.8489 | 0.8447 | 0.8449 | 0.0040 | | 0.0061 | 0.0042 |
| 62 | 0.8588 | 0.8546 | 0.8547 | 0.0042 | | 0.0056 | 0.0043 |
| 63 | 0.8673 | 0.8638 | 0.8639 | 0.0034 | | 0.0049 | 0.0036 |
| 64 | 0.8745 | 0.8724 | 0.8725 | 0.0020 | | 0.0051 | 0.0021 |
| 65 | 0.8817 | 0.8804 | 0.8806 | 0.0011 | | 0.0059 | 0.0012 |
| 66 | 0.8886 | 0.8880 | 0.8882 | 0.0004 | | 0.0063 | 0.0006 |
| 67 | 0.8946 | 0.8951 | 0.8952 | 0.0006 | | 0.0065 | 0.0005 |
| 68 | 0.9009 | 0.9017 | 0.9019 | 0.0010 | | 0.0071 | 0.0009 |
| 69 | 0.9072 | 0.9080 | 0.9081 | 0.0009 | | 0.0071 | 0.0008 |
| 70 | 0.9114 | 0.9138 | 0.9139 | 0.0026 | | 0.0066 | 0.0024 |

TABLA VI-7-C
Número

| | Re2A2S1R1R2 | | | | | |
|---------|-------------|----------|----------|--------|--------|--------|
| | FePRM | Fe teor1 | Fe teor2 | DIF-A | Ao1 | Ao2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0060 | 0.0108 | 0.0108 | 0.0048 | 0.0108 | 0.0048 |
| 2 | 0.0181 | 0.0215 | 0.0215 | 0.0035 | 0.0155 | 0.0035 |
| 3 | 0.0298 | 0.0321 | 0.0321 | 0.0023 | 0.0141 | 0.0023 |
| 4 | 0.0415 | 0.0426 | 0.0426 | 0.0011 | 0.0128 | 0.0011 |
| 5 | 0.0532 | 0.0530 | 0.0530 | 0.0002 | 0.0115 | 0.0002 |
| 6 | 0.0646 | 0.0633 | 0.0633 | 0.0014 | 0.0101 | 0.0014 |
| 7 | 0.0760 | 0.0734 | 0.0734 | 0.0026 | 0.0088 | 0.0026 |
| 8 | 0.0873 | 0.0835 | 0.0835 | 0.0039 | 0.0074 | 0.0039 |
| 9 | 0.0984 | 0.0934 | 0.0934 | 0.0050 | 0.0061 | 0.0050 |
| 10 | 0.1095 | 0.1032 | 0.1032 | 0.0063 | 0.0048 | 0.0063 |
| 11 | 0.1206 | 0.1129 | 0.1129 | 0.0077 | 0.0034 | 0.0077 |
| 12 | 0.1316 | 0.1225 | 0.1225 | 0.0090 | 0.0019 | 0.0090 |
| 13 | 0.1425 | 0.1320 | 0.1320 | 0.0104 | 0.0005 | 0.0104 |
| 14 | 0.1533 | 0.1414 | 0.1414 | 0.0119 | 0.0010 | 0.0119 |
| 15 | 0.1640 | 0.1507 | 0.1507 | 0.0133 | 0.0026 | 0.0133 |
| 16 | 0.1746 | 0.1599 | 0.1599 | 0.0147 | 0.0041 | 0.0147 |
| 17 | 0.1852 | 0.1690 | 0.1690 | 0.0162 | 0.0056 | 0.0162 |
| 18 | 0.1958 | 0.1780 | 0.1780 | 0.0178 | 0.0072 | 0.0178 |
| 19 | 0.2064 | 0.1869 | 0.1869 | 0.0195 | 0.0089 | 0.0195 |
| 20 | 0.2169 | 0.1958 | 0.1958 | 0.0212 | 0.0107 | 0.0212 |
| 21 | 0.2272 | 0.2045 | 0.2045 | 0.0227 | 0.0124 | 0.0227 |
| 22 | 0.2373 | 0.2131 | 0.2131 | 0.0242 | 0.0141 | 0.0242 |
| 23 | 0.2472 | 0.2216 | 0.2216 | 0.0256 | 0.0157 | 0.0256 |
| 24 | 0.2572 | 0.2300 | 0.2300 | 0.0272 | 0.0172 | 0.0272 |
| 25 | 0.2672 | 0.2384 | 0.2384 | 0.0288 | 0.0189 | 0.0288 |
| 26 | 0.2768 | 0.2466 | 0.2466 | 0.0302 | 0.0205 | 0.0302 |
| 27 | 0.2863 | 0.2548 | 0.2548 | 0.0315 | 0.0220 | 0.0315 |
| 28 | 0.2959 | 0.2629 | 0.2629 | 0.0331 | 0.0235 | 0.0331 |
| 29 | 0.3056 | 0.2709 | 0.2709 | 0.0348 | 0.0251 | 0.0348 |
| 30 | 0.3151 | 0.2788 | 0.2788 | 0.0363 | 0.0269 | 0.0363 |
| 31 | 0.3246 | 0.3019 | 0.3019 | 0.0407 | 0.0131 | 0.0407 |
| 32 | 0.3692 | 0.3244 | 0.3244 | 0.0448 | 0.0183 | 0.0448 |
| 33 | 0.3945 | 0.3461 | 0.3461 | 0.0484 | 0.0231 | 0.0484 |
| 34 | 0.4188 | 0.3671 | 0.3671 | 0.0517 | 0.0274 | 0.0517 |
| 35 | 0.4423 | 0.3875 | 0.3875 | 0.0548 | 0.0313 | 0.0548 |
| 36 | 0.4645 | 0.4072 | 0.4072 | 0.0573 | 0.0351 | 0.0574 |

TABLA VI-7-C

| Número | continuacion.. | | Re2A2S1R1R2 | | DIF-A | Ao1 | Ao2 |
|--------|----------------|----------|-------------|--------|--------|--------|-----|
| | FeFRON | Fe teor1 | Fe teor2 | | | | |
| 37 | 0.4849 | 0.4262 | 0.4262 | 0.0587 | 0.0383 | 0.0587 | |
| 38 | 0.5045 | 0.4447 | 0.4447 | 0.0598 | 0.0402 | 0.0598 | |
| 39 | 0.5235 | 0.4625 | 0.4625 | 0.0610 | 0.0420 | 0.0610 | |
| 40 | 0.5418 | 0.4798 | 0.4798 | 0.0620 | 0.0437 | 0.0620 | |
| 41 | 0.5591 | 0.4965 | 0.4965 | 0.0626 | 0.0453 | 0.0626 | |
| 42 | 0.5754 | 0.5127 | 0.5127 | 0.0627 | 0.0464 | 0.0627 | |
| 43 | 0.5913 | 0.5284 | 0.5284 | 0.0629 | 0.0470 | 0.0629 | |
| 44 | 0.6066 | 0.5435 | 0.5436 | 0.0630 | 0.0478 | 0.0630 | |
| 45 | 0.6210 | 0.5582 | 0.5582 | 0.0627 | 0.0484 | 0.0628 | |
| 46 | 0.6482 | 0.5862 | 0.5862 | 0.0620 | 0.0348 | 0.0620 | |
| 47 | 0.6739 | 0.6123 | 0.6124 | 0.0615 | 0.0359 | 0.0616 | |
| 48 | 0.6976 | 0.6369 | 0.6369 | 0.0607 | 0.0370 | 0.0608 | |
| 49 | 0.7194 | 0.6598 | 0.6599 | 0.0595 | 0.0378 | 0.0596 | |
| 50 | 0.7392 | 0.6814 | 0.6814 | 0.0577 | 0.0381 | 0.0578 | |
| 51 | 0.7572 | 0.7015 | 0.7016 | 0.0556 | 0.0376 | 0.0557 | |
| 52 | 0.7740 | 0.7204 | 0.7205 | 0.0535 | 0.0368 | 0.0536 | |
| 53 | 0.7888 | 0.7381 | 0.7382 | 0.0506 | 0.0359 | 0.0507 | |
| 54 | 0.8023 | 0.7547 | 0.7548 | 0.0476 | 0.0342 | 0.0477 | |
| 55 | 0.8149 | 0.7702 | 0.7703 | 0.0446 | 0.0322 | 0.0447 | |
| 56 | 0.8257 | 0.7847 | 0.7848 | 0.0409 | 0.0302 | 0.0410 | |
| 57 | 0.8352 | 0.7983 | 0.7983 | 0.0368 | 0.0274 | 0.0369 | |
| 58 | 0.8443 | 0.8111 | 0.8112 | 0.0331 | 0.0241 | 0.0332 | |
| 59 | 0.8526 | 0.8231 | 0.8232 | 0.0294 | 0.0212 | 0.0296 | |
| 60 | 0.8601 | 0.8342 | 0.8344 | 0.0257 | 0.0184 | 0.0258 | |
| 61 | 0.8671 | 0.8447 | 0.8449 | 0.0223 | 0.0154 | 0.0224 | |
| 62 | 0.8730 | 0.8546 | 0.8547 | 0.0191 | 0.0126 | 0.0192 | |
| 63 | 0.8800 | 0.8638 | 0.8639 | 0.0161 | 0.0100 | 0.0162 | |
| 64 | 0.8858 | 0.8724 | 0.8725 | 0.0133 | 0.0076 | 0.0134 | |
| 65 | 0.8909 | 0.8804 | 0.8806 | 0.0103 | 0.0053 | 0.0105 | |
| 66 | 0.8957 | 0.8880 | 0.8882 | 0.0076 | 0.0029 | 0.0077 | |
| 67 | 0.9000 | 0.8951 | 0.8952 | 0.0047 | 0.0006 | 0.0049 | |
| 68 | 0.9036 | 0.9017 | 0.9019 | 0.0017 | 0.0018 | 0.0019 | |
| 69 | 0.9068 | 0.9080 | 0.9081 | 0.0013 | 0.0043 | 0.0011 | |
| 70 | 0.9091 | 0.9138 | 0.9139 | 0.0048 | 0.0069 | 0.0047 | |

TABLA VI-B-C

| Número | Re2A2S2R1K2 | | | | | |
|---------|-------------|----------|----------|--------|--------|--------|
| | FeFROM | Fe teor1 | Fe teor2 | DIF-A | Ao1 | Ao2 |
| inicial | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 1 | 0.0058 | 0.0108 | 0.0108 | 0.0050 | 0.0108 | 0.0050 |
| 2 | 0.0174 | 0.0215 | 0.0215 | 0.0041 | 0.0157 | 0.0041 |
| 3 | 0.0290 | 0.0321 | 0.0321 | 0.0032 | 0.0147 | 0.0032 |
| 4 | 0.0406 | 0.0426 | 0.0426 | 0.0020 | 0.0137 | 0.0020 |
| 5 | 0.0520 | 0.0530 | 0.0530 | 0.0010 | 0.0124 | 0.0010 |
| 6 | 0.0633 | 0.0633 | 0.0633 | 0.0000 | 0.0112 | 0.0000 |
| 7 | 0.0745 | 0.0734 | 0.0734 | 0.0011 | 0.0101 | 0.0011 |
| 8 | 0.0857 | 0.0835 | 0.0835 | 0.0022 | 0.0090 | 0.0022 |
| 9 | 0.0969 | 0.0934 | 0.0934 | 0.0035 | 0.0077 | 0.0035 |
| 10 | 0.1079 | 0.1032 | 0.1032 | 0.0047 | 0.0063 | 0.0047 |
| 11 | 0.1184 | 0.1129 | 0.1129 | 0.0055 | 0.0050 | 0.0055 |
| 12 | 0.1289 | 0.1225 | 0.1225 | 0.0064 | 0.0041 | 0.0064 |
| 13 | 0.1391 | 0.1320 | 0.1320 | 0.0071 | 0.0031 | 0.0071 |
| 14 | 0.1493 | 0.1414 | 0.1414 | 0.0079 | 0.0023 | 0.0079 |
| 15 | 0.1594 | 0.1507 | 0.1507 | 0.0087 | 0.0014 | 0.0087 |
| 16 | 0.1693 | 0.1599 | 0.1599 | 0.0094 | 0.0005 | 0.0094 |
| 17 | 0.1790 | 0.1690 | 0.1690 | 0.0100 | 0.0003 | 0.0100 |
| 18 | 0.1886 | 0.1780 | 0.1780 | 0.0106 | 0.0010 | 0.0106 |
| 19 | 0.1982 | 0.1869 | 0.1869 | 0.0113 | 0.0017 | 0.0113 |
| 20 | 0.2076 | 0.1958 | 0.1958 | 0.0119 | 0.0025 | 0.0119 |
| 21 | 0.2169 | 0.2045 | 0.2045 | 0.0125 | 0.0032 | 0.0125 |
| 22 | 0.2260 | 0.2131 | 0.2131 | 0.0129 | 0.0038 | 0.0129 |
| 23 | 0.2351 | 0.2216 | 0.2216 | 0.0135 | 0.0044 | 0.0135 |
| 24 | 0.2443 | 0.2300 | 0.2300 | 0.0142 | 0.0051 | 0.0142 |
| 25 | 0.2535 | 0.2384 | 0.2384 | 0.0151 | 0.0059 | 0.0151 |
| 26 | 0.2625 | 0.2466 | 0.2466 | 0.0160 | 0.0068 | 0.0160 |
| 27 | 0.2717 | 0.2548 | 0.2548 | 0.0169 | 0.0078 | 0.0169 |
| 28 | 0.2807 | 0.2629 | 0.2629 | 0.0178 | 0.0088 | 0.0178 |
| 29 | 0.2894 | 0.2709 | 0.2709 | 0.0186 | 0.0098 | 0.0186 |
| 30 | 0.2981 | 0.2788 | 0.2788 | 0.0194 | 0.0107 | 0.0194 |
| 31 | 0.3237 | 0.3019 | 0.3019 | 0.0217 | 0.0038 | 0.0217 |
| 32 | 0.3486 | 0.3244 | 0.3244 | 0.0242 | 0.0007 | 0.0242 |
| 33 | 0.3724 | 0.3461 | 0.3461 | 0.0263 | 0.0025 | 0.0263 |
| 34 | 0.3948 | 0.3671 | 0.3671 | 0.0277 | 0.0053 | 0.0277 |
| 35 | 0.4162 | 0.3875 | 0.3875 | 0.0287 | 0.0073 | 0.0287 |
| 36 | 0.4365 | 0.4072 | 0.4072 | 0.0293 | 0.0090 | 0.0293 |

TABLA VI-8-C
Número

| | continuación.. | | Re2A2S2R1R2 | | Ao1 | Ao2 |
|----|----------------|----------|-------------|--------|--------|--------|
| | FePRDM | Fe teor1 | Fe teor2 | DIF-A | | |
| 37 | 0.4554 | 0.4262 | 0.4262 | 0.0292 | 0.0103 | 0.0292 |
| 38 | 0.4734 | 0.4447 | 0.4447 | 0.0287 | 0.0108 | 0.0288 |
| 39 | 0.4911 | 0.4625 | 0.4625 | 0.0286 | 0.0109 | 0.0286 |
| 40 | 0.5087 | 0.4798 | 0.4798 | 0.0288 | 0.0113 | 0.0289 |
| 41 | 0.5256 | 0.4965 | 0.4965 | 0.0290 | 0.0121 | 0.0291 |
| 42 | 0.5414 | 0.5127 | 0.5127 | 0.0286 | 0.0129 | 0.0287 |
| 43 | 0.5564 | 0.5284 | 0.5284 | 0.0280 | 0.0130 | 0.0281 |
| 44 | 0.5713 | 0.5435 | 0.5436 | 0.0277 | 0.0129 | 0.0277 |
| 45 | 0.5854 | 0.5582 | 0.5582 | 0.0272 | 0.0130 | 0.0272 |
| 46 | 0.6118 | 0.5862 | 0.5862 | 0.0256 | 0.0008 | 0.0257 |
| 47 | 0.6368 | 0.6123 | 0.6124 | 0.0244 | 0.0005 | 0.0244 |
| 48 | 0.6606 | 0.6369 | 0.6369 | 0.0237 | 0.0001 | 0.0238 |
| 49 | 0.6834 | 0.6598 | 0.6599 | 0.0235 | 0.0008 | 0.0235 |
| 50 | 0.7038 | 0.6814 | 0.6814 | 0.0224 | 0.0020 | 0.0225 |
| 51 | 0.7221 | 0.7015 | 0.7016 | 0.0205 | 0.0023 | 0.0206 |
| 52 | 0.7392 | 0.7204 | 0.7205 | 0.0187 | 0.0017 | 0.0188 |
| 53 | 0.7556 | 0.7381 | 0.7382 | 0.0174 | 0.0011 | 0.0175 |
| 54 | 0.7715 | 0.7547 | 0.7548 | 0.0167 | 0.0009 | 0.0168 |
| 55 | 0.7862 | 0.7702 | 0.7703 | 0.0159 | 0.0013 | 0.0160 |
| 56 | 0.8000 | 0.7847 | 0.7848 | 0.0152 | 0.0015 | 0.0153 |
| 57 | 0.8131 | 0.7983 | 0.7985 | 0.0147 | 0.0017 | 0.0148 |
| 58 | 0.8248 | 0.8111 | 0.8112 | 0.0136 | 0.0020 | 0.0137 |
| 59 | 0.8354 | 0.8231 | 0.8232 | 0.0123 | 0.0017 | 0.0124 |
| 60 | 0.8453 | 0.8342 | 0.8344 | 0.0110 | 0.0012 | 0.0111 |
| 61 | 0.8546 | 0.8447 | 0.8449 | 0.0097 | 0.0006 | 0.0098 |
| 62 | 0.8631 | 0.8546 | 0.8547 | 0.0084 | 0.0000 | 0.0085 |
| 63 | 0.8707 | 0.8638 | 0.8639 | 0.0068 | 0.0007 | 0.0070 |
| 64 | 0.8777 | 0.8724 | 0.8725 | 0.0052 | 0.0017 | 0.0053 |
| 65 | 0.8827 | 0.8804 | 0.8806 | 0.0031 | 0.0028 | 0.0032 |
| 66 | 0.8886 | 0.8880 | 0.8882 | 0.0004 | 0.0044 | 0.0005 |
| 67 | 0.8926 | 0.8951 | 0.8952 | 0.0027 | 0.0065 | 0.0025 |
| 68 | 0.8959 | 0.9017 | 0.9019 | 0.0060 | 0.0092 | 0.0059 |
| 69 | 0.8986 | 0.9080 | 0.9081 | 0.0095 | 0.0121 | 0.0093 |
| 70 | 0.9007 | 0.9138 | 0.9139 | 0.0133 | 0.0152 | 0.0131 |

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